



First Semester Examination  
2019/2020 Academic Session

December 2019/January 2020

**ESA321 – Aerospace Structure**  
**[Struktur Aeroangkasa]**

Duration : 3 hours  
(Masa : 3 jam)

---

Please check that this examination paper consists of **ELEVEN (11)** pages of printed material, included **TWO (2)** pages appendix and **FIVE (5)** questions before you begin the examination.

*[Sila pastikan bahawa kertas peperiksaan ini mengandungi **SEBELAS (11)** mukasurat yang bercetak termasuk **DUA (2)** mukasurat lampiran dan **LIMA (5)** soalan sebelum anda memulakan peperiksaan ini].*

**Instructions** : Answer **ALL** questions.

**Arahan** : Jawab **SEMUA** soalan].

Student may answer the questions either in **English** or **Bahasa Malaysia**.

*[Pelajar boleh menjawab soalan dalam **Bahasa Inggeris** atau **Bahasa Malaysia**].*

Each questions must begin from a new page.

*[Setiap soalan mestilah dimulakan pada mukasurat yang baru].*

In the event of any discrepancies, the English version shall be used.

*[Sekiranya terdapat sebarang percanggahan pada soalan peperiksaan, versi Bahasa Inggeris hendaklah digunakan]*

1. (a). Describe the general procedure for performing structural analysis using finite element method software.

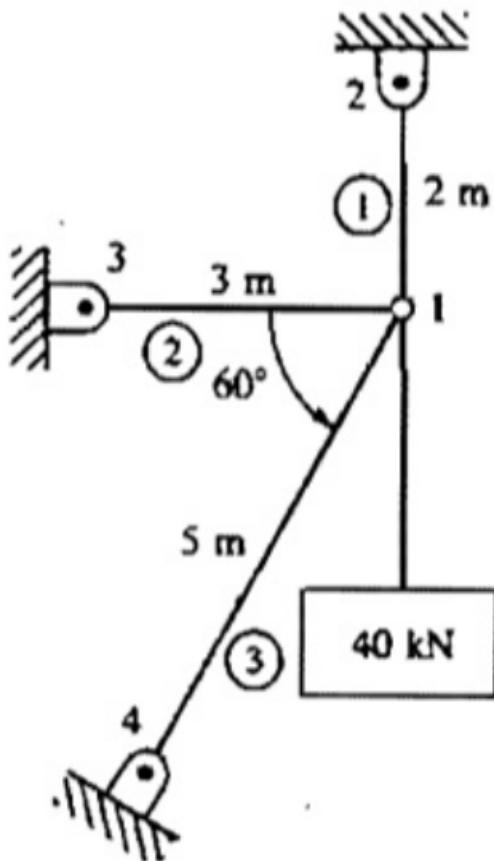
(3 marks)

- (b). List **FIVE** ways that can be employed to confirm the validity of the results obtained using finite element method.

(3 marks)

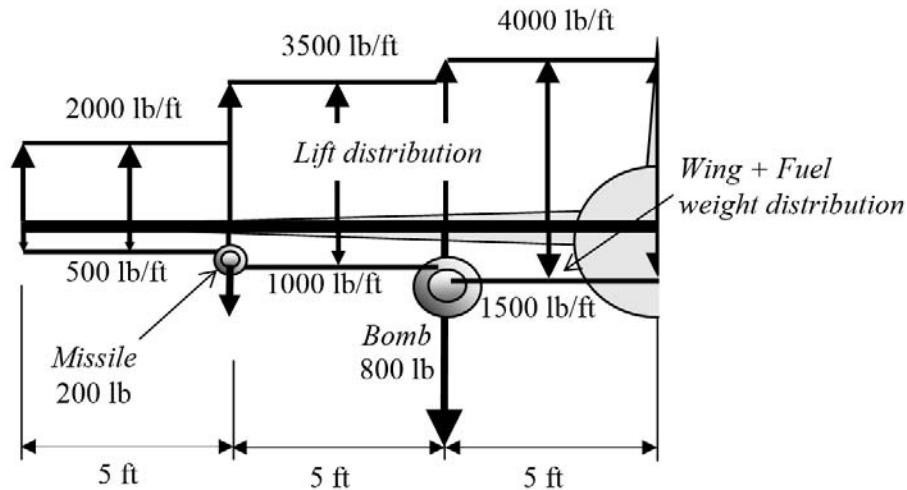
- (c). For the plane trusses shown in **Figure 1**, using finite element method determine the horizontal and vertical displacements of node 1. All elements have  $E = 210 \text{ GPa}$  and  $A = 4.0 \times 10^{-4} \text{ m}^2$ .

(14 marks)



**Figure 1**

2. Using **Figure 2** shown below, draw the shear load and bending moment diagrams of the half-wing while the aircraft is in flight.

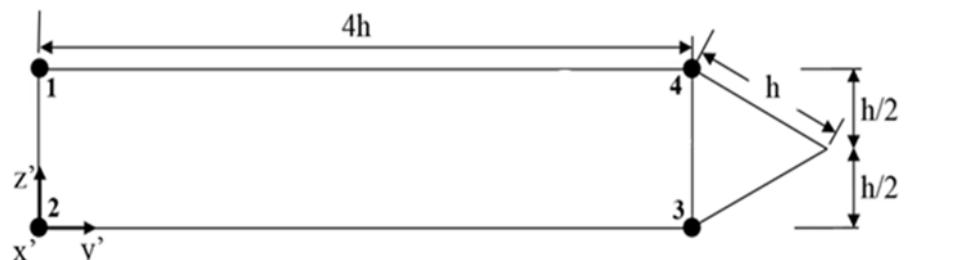


**Figure 2**

**(20 marks)**

3. Bending moments of  $M_y = -50$  Nm and  $M_z = -10$  Nm are applied on the idealized thin-walled 4 booms wing beam section shown in **Figure 3**.

Determine the axial stresses in all booms.



$h = 200 \text{ mm}$

Area of boom 2 = 2000 mm<sup>2</sup>

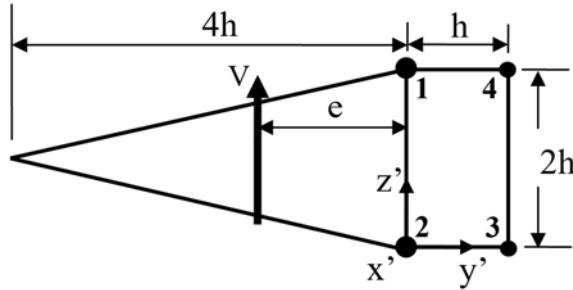
Area of booms 1, 3 & 4 = 3000 mm<sup>2</sup>

**Figure 3**

(20 marks)

4/-

4. Determine  $e$ , the shear center of the idealized thin-walled 4-boom beam section shown in **Figure 4**.



Original thickness of all walls =  $t$

Area of booms 1 & 2 =  $2A$

Area of booms 3 & 4 =  $A$

**Figure 4**

**(20 marks)**

5. **Figure 5** shows a fuselage structure.

- Fuselage skins between the stringers are considered flat
- Structure is made of aluminum:

$$E = 10 \times 10^6 \text{ psi}; \nu = 0.3; \sigma_{\text{yield}} = 63 \text{ ksi}; \sigma_{\text{ult}} = 74 \text{ ksi}$$

- Skin thickness,  $t_{\text{sk}}$  0.05 in
- Stringer thickness,  $t_{\text{st}}$  0.04 in

- (a). Determine whether the skin and stringer can fail in local buckling, if

- Maximum compressive load  $N_x$  1200 lb/in
- Frame/former spacing,  $L$  24 in
- Stringer spacing,  $W$  3 in

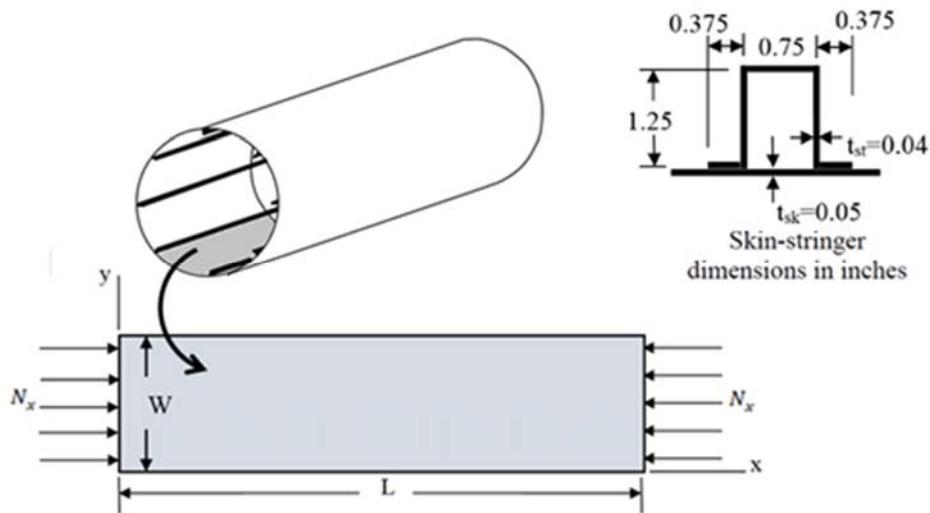
**(5 marks)**

...5/-

- (b). Optimize the skin-stringer (stiffened-panel/panel-strut) structure design by finding the appropriate frame and stringer spacings, L and W such that if buckling failure occurs, the skins, stringers and stiffened-panel structure should fail simultaneously (i.e. local and general/global buckling occurs at the same critical stress).

Design requirements:

- All stringer dimensions are fixed.
- Ratio  $L/W \gg 3$



**Figure 5**

**(15 marks)**

1. (a). Terangkan tatacara am untuk melakukan analisa struktur dengan menggunakan perisian kaedah elemen terhingga.

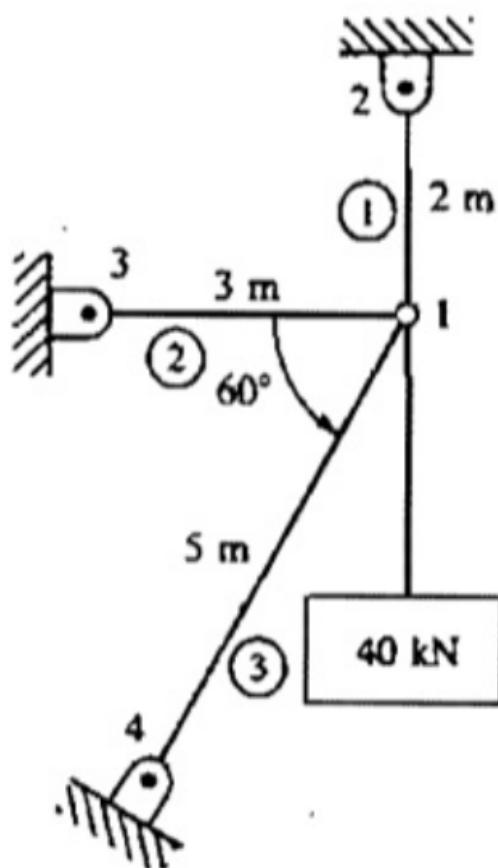
(3 markah)

- (b). Senaraikan **LIMA** cara yang boleh digunakan untuk memastikan kesahihan keputusan yang diperolehi daripada kaedah elemen terhingga.

(3 markah)

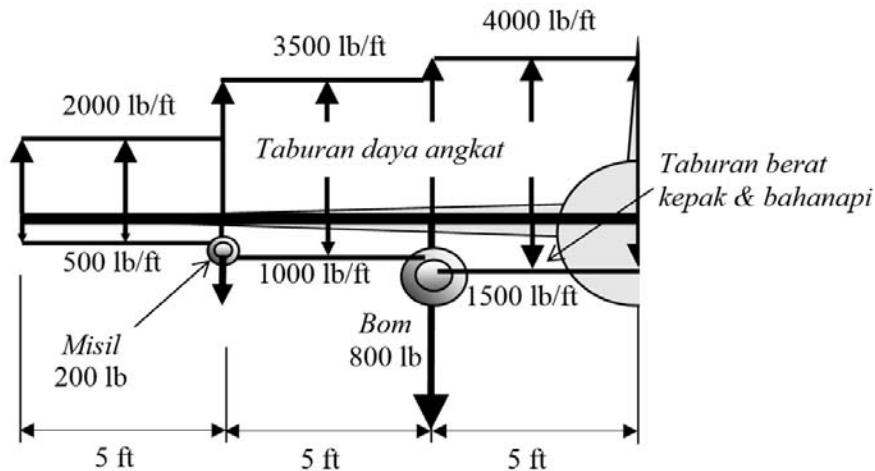
- (c). Untuk palang planar yang ditunjukkan dalam **Rajah 1**, dengan kaedah elemen terhingga cari sesaran melintang dan mengak pada nod 1. Semua elemen mempunyai  $E = 210 \text{ GPa}$  dan  $A = 4.0 \times 10^{-4} \text{ m}^2$ .

(14 markah)



**Rajah 1**

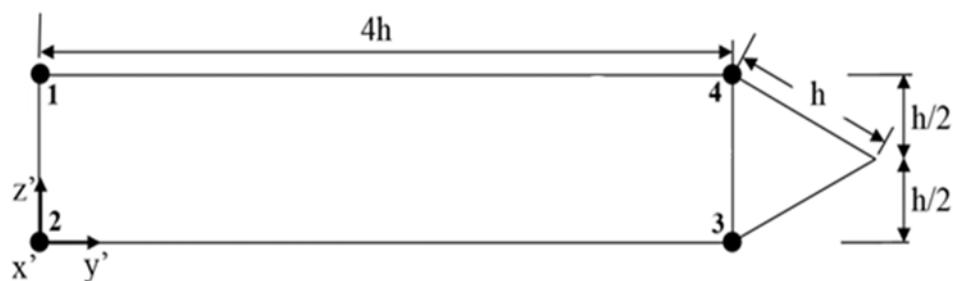
2. Dengan menggunakan **Rajah 2** di bawah, lukiskan rajah beban ricih dan momen lentur kepada sepah semasa pesawat yang sedang dalam penerbangan

**Rajah 2**

(20 markah)

3. Momen lentur  $M_y = -50 \text{ kNm}$  dan  $M_z = 10 \text{ kNm}$  dikenakan ke atas keratan-rentas rasuk dinding-nipis 4 gelegar yang ditunjukkan di **Rajah 3**.

Tentukan tegasan paksi pada setiap gelegar.



$$h = 200 \text{ mm}$$

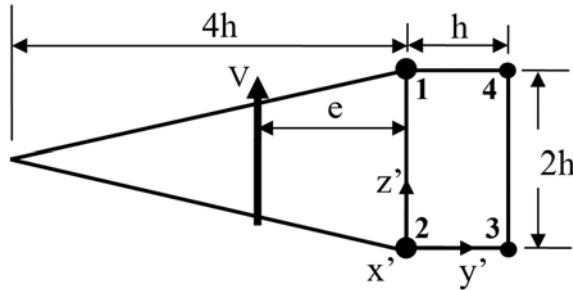
$$\text{Keluasan gelegar } 2 = 2000 \text{ mm}^2$$

$$\text{Keluasan gelegar } 1, 3 \text{ & } 4 = 3000 \text{ mm}^2$$

**Rajah 3**

(20 markah)

4. Tentukan  $e$ , pusat rincih rasuk 4-gelegar ideal yang ditunjukkan di **Rajah 4**.



Tebal asal semua dinding =  $t$

Keluasan gelegar 1 & 2 =  $2A$

Keluasan gelegar 3 & 4 =  $A$

**Rajah 4**

(20 markah)

5. **Rajah 5** menunjukkan struktur fuselaj.

- Kulit fuselaj di antara gelegar dianggap rata.
- Struktur dibuat dari aluminium:

$$E = 10 \times 10^6 \text{ psi}; \nu = 0.3; \sigma_{yield} = 63 \text{ ksi}; \sigma_{ult} = 74 \text{ ksi}$$

- Tebal kulit,  $t_{sk}$                     0.05 in
- Tebal gelegar,  $t_{st}$     0.04 in

- (a). Tentukan jika kulit dan gelegar boleh gagal secara lengkokan (termasuk lengkokan lokal), jika

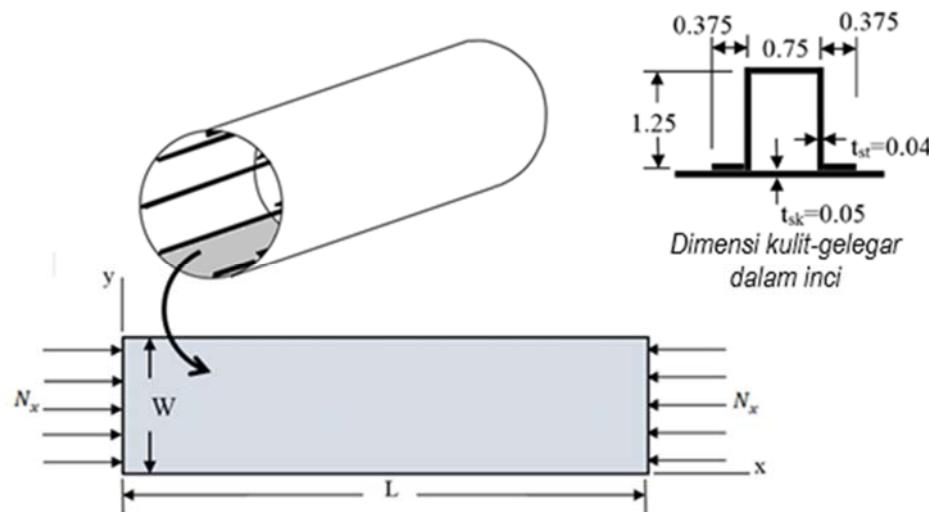
- Beban mampat maksimum,  $N_x$     1200 lb/in
- Jarak antara rusuk/bingkai,  $L$     24 in
- Jarak antara gelegar,  $W$                 3 in

(5 markah)

- (b). Optimumkan rekabentuk struktur kulit-gelegar dengan mencari jarak sesuai,  $L$  (antara rusuk ke rusuk) dan  $W$  (antara gelegar ke gelegar) di mana andai jika berlaku kegagalan secara lengkokan kulit, gelegar dan struktur kulit-gelegar, hendaklah gagal serentak (iaitu kegagalan lokal dan global berlaku pada tegasan kritikal yang sama).

Keperluan rekabentuk :

- Semua dimensi gelegar tidak berubah
- Nisbah  $L/W \gg 3$



**Rajah 5**

**(15 markah)**

**Equation for truss element stiffness in global coordinate system**

$$k = \frac{EA}{L} \begin{bmatrix} l^2 & lm & -l^2 & -lm \\ lm & m^2 & -lm & -m^2 \\ -l^2 & -lm & l^2 & lm \\ -lm & -m^2 & lm & m^2 \end{bmatrix}$$

Where

$$l = \cos\theta = \frac{X_j - X_i}{L}$$

and

$$m = \sin\theta = \frac{Y_j - Y_i}{L}$$

$$\sigma_x = \frac{P}{A} + \frac{- (M_z I_y + M_y I_{yz}) y + (M_y I_z + M_z I_{yz}) z}{I_y I_z - I_{yz}^2}$$

$$\Delta q = - \left[ \frac{(V_y I_y - V_z I_{yz}) Q_z + (V_z I_z - V_y I_{yz}) Q_y}{I_y I_z - I_{yz}^2} \right] \quad \theta = \frac{q}{2AG} \oint \frac{ds}{t}$$

$$P_{cr} = \frac{\pi^2 EI}{L_e^2} \quad \sigma_{cr} = \frac{\pi^2 E}{(L_e / r)^2} \quad \sigma_{cr} = k \frac{\pi^2 E}{12(1-\nu^2)} \left( \frac{t}{b} \right)^2$$

**Buckling Loads**

Buckling Load	$\frac{\pi^2 EI}{L^2}$	$\frac{4\pi^2 EI}{L^2}$	$\frac{2.045\pi^2 EI}{L^2}$	$\frac{\pi^2 EI}{4L^2}$	$\frac{\pi^2 EI}{L^2}$
Effective Length $L_e$	$L$	$0.5L$	$0.699L$	$2L$	$L$

