## PARAMETRIC STUDY OF CAVITATION EFFECT ON 3D HYDROKINETIC TURBINE BLADES USING CFD

## NHGANTIRAN A/L NANTHAKUMAR KAWENDAR

# UNIVERSITI SAINS MALAYSIA

2021

## PARAMETRIC STUDY OF CAVITATION EFFECT ON 3D HYDROKINETIC TURBINE BLADES USING CFD

by

## NHGANTIRAN A/L NANTHAKUMAR KAWENDAR

Thesis submitted in fulfilment of the requirements for the Bachelor Degree of Engineering (Honours) (Aerospace Engineering)

June 2021

### ENDORSEMENT

I, Nhgantiran A/L Nanthakumar Kawendar hereby declare that I have checked and revised the whole draft of dissertation as required by my supervisor.

Nhgan

(Signature of Student) Date: 25 June 2021

(Signature of Supervisor) Date: 25 June 2021

(Signature of Examiner) Date: 6 July 2021

### DECLARATION

This whole thesis is the work and investigation of my own, except where it is stated otherwise, this work has not previously been accepted in substances for any degree and is not being concurrently submitted in candidature for any other degree.

Nhgan

(Signature of Student) Date: 25 June 2021

#### ACKNOWLEDGEMENT

I would like to take this opportunity to express my gratitude and appreciation to everyone who has been guiding and helping me throughout this project. Firstly, I would like to thank my supervisor Dr. Chang Wei Shyang who has been continuously guiding and helping me since the initiation of this project until the completion of this project. Dr. Chang Wei Shyang continuously keep track of my progress on this project and always have suggestions and ideas to further increase the performance and reliability of this project. Dr. Chang Wei Shyang always gives advises and technical support on performing the CFD simulation in ANSYS software. He shows a proper way to do a project and produce a reliable result. For instance, he gave example journals which were a great help for me to efficiently search proper journals and experimental data for validation purposes. Next I would like to express my utmost gratitude to Assoc.Prof. Dr. Farzad Ismail, Dr. Mohammad Hafifi Hafiz Bin Ishaik and other fellow friends who attended, corrected my flaws in CFD workflow during weekly FYP presentation. I would also like to express my gratitude to my senior Lim Han Wea who conducted the research on 2D hydrokinetic turbine. They have given suggestions and corrections on the conditions of simulations. I would also like to thank my school for providing me the access to computer with Ansys Software to run simulation in CFD lab. These assistances were really meaningful to me and keep me from deviating to a wrong approach in conducting this research. From my bottom of heart, I express my gratitude to all of the people who supported me in this research project.

# PARAMETRIC STUDY OF CAVITATION EFFECT ON 3D HYDROKINETIC TURBINE BLADES USING CFD ABSTRACT

This project's work discusses about the parametric study of cavitation around the horizontal axis turbine blade. This work mainly focusses on the case study of cavitation and how it affects the performance of the blade in terms of lift, drag and pitching moment. Cavitation is the phenomenon where it damages the surface of turbine blade when the cavities collapse. The objectives of this work are to study the effect of Artificial Cavitation Generator (ACG) installed on turbine blade and twisting angle of turbine blade on the blade performance while observing the changes in behaviour of cavitation. The optimal design of turbine blade with ACG and twisting angle is then suggested based on the finding. The analysis is done using Computational Fluid Dynamics (CFD) simulation software, ANSYS FLUENT. This research focuses on 3dimensional case study of a single blade which uses the profile NACA 4418. The modification of twist angle and also the installation of ACG were done using Computational Aided Design (CAD) software, SOLIDWORKS and Design Modular. The simulations were conducted using parameters from the literature review for validation purpose and also to compare the result of modified blade with original blade. The simulation was conducted at fluid velocity 1.9 m/s with multiphase viscous model, Re-Normalisation Group k-& model, cavitation model, Schnerr-Sauer model to simulate the cavitation phenomenon. From the simulations, it was found that the twisting angle changes the lift coefficient and also drag coefficient while the installation of ACG disrupts the cyclic behaviour of cavitation phenomenon. The optimal design for the blade is with the twisting angle of 4° and also with the installation of Artificial Cavitation Generator (ACG).

## KAJIAN PARAMETRIK PENGARUH KAVITASI TERHADAP BILAH TURBIN HIDROKINETIK 3D MENGGUNAKAN CFD

### ABSTRAK

Projek ini membincangkan mengenai kajian parametrik kavitasi di sekitar bilah turbin paksi mendatar. Karya ini terutamanya fokus pada kajian kes kavitasi dan pengaruh kavitasi kepada prestasi bilah turbin dari segi pekali angkat, pekali seret dan pekali momentum nada. Kavitasi adalah fenomena di mana ia merosakkan permukaan bilah turbin ketika rongga runtuh. Objektif kerja ini adalah untuk mengkaji kesan Penjana Kavitasi Buatan yang dipasang pada bilah turbin dan sudut putaran turbin terhadap prestasi bilah turbin sambil memerhatikan perubahan tingkah laku peronggaan. Reka bentuk bilah turbin yang optimum dengan Penjana Kavitasi Buatan dan sudut berpusing kemudian dicadangkan berdasarkan temuan. Analisis dilakukan menggunakan perisian simulasi 'Computational Fluid Dynamics' (CFD), ANSYS FLUENT. Penyelidikan ini memfokuskan pada kajian kes 3-dimensi dari bilah turbin tunggal yang menggunakan profil NACA 4418. Pengubahsuaian sudut putar dan juga pemasangan Penjana Kavitasi Buatan dilakukan dengan menggunakan perisian reka bentuk berbantu pengkomputeran (CAD), SOLIDWORKS dan 'Design Modular'. Simulasi dilakukan menggunakan parameter dari tinjauan sastera untuk tujuan pengesahan dan juga untuk membandingkan hasil bilah turbin yang diubah dengan bilah turbin asli. Ini adalah pendekatan untuk menghasilkan perbandingan dan hasil yang lebih berpengaruh. Simulasi dilakukan pada kecepatan bendalir 1.9 m/s dengan model multiphasa, model 'Re-Normalisation Group k- $\varepsilon$ ' peronggaan, model Schnerr-Sauer untuk mensimulasikan fenomena kavitasi.

Dari simulasi ini, didapati bahawa sudut berpusing mengubah pekali angkat, pekali seret dan pekali momentum nada sementara pemasangan Penjana Kavitasi Buatan mengubah tingkah laku kitaran fenomena kavitasi dan mengurangkan fenomena kavitasi. Apabila sudut berpusing berubah, pekali angkat, pekali seret dan pekali momentum nada juga berubah. Reka bentuk optimum untuk bilah turbin adalah dengan sudut putaran 4° dan juga dengan pemasangan Penjana Kavitasi Buatan.

### TABLE OF CONTENTS

END	ORSEME	NT	ii
ACK	NOWLEI	DGEMENT	iv
ABS	ГRACT		v
ABS	ГRAK		vi
TAB	LE OF CO	ONTENTS	viii
LIST	OF TAB	LES	xi
LIST	OF FIGU	JRES	xii
LIST	OF SYM	BOLS	xiv
LIST	OF ABB	REVIATIONS	xvi
LIST	OF APP	ENDICES	xvii
СНА	PTER 1	INTRODUCTION	
1.1	Malaysia	a's Current Energy Background	
	1.1.1	Hydro Energy	19
1.2	Hydroki	netic Turbine	
	1.2.1	Classification of hydrokinetic turbine	21
	1.2.2	Blade Design of Hydrokinetic Turbine	
1.3	Cavitatio	on Phenomenon	
1.4	Artificia	l Cavitation Generator (ACG)	
1.5	Computa	ational Fluid Dynamics	
1.6	Problem	Statement	
1.7	Objectiv	e of Research	
СНА	PTER 2	LITERATURE REVIEW	
2.1	Hydrofo	il	
	2.1.1	Performance Analysis of various hydrofoils	
2.2	Artificia	l Cavitation Generator (ACG)	

	2.2.1	Effect of Artificial Cavitation Generator on Cavitation	30
	2.2.2	Location and Size of Artificial Cavitation Generator	31
2.3	Angle of	f attack	31
	2.3.1	Impact of hydrokinetic turbine blade angle of attack on cavitation	31
2.4	Twisting	g angle	32
	2.4.1	Impact of hydrokinetic turbine twisting angle on turbine performance	32
2.5	Cavitatio	on	33
2.6	Summar	у	35
CHA	PTER 3	METHODOLOGY	36
3.1	Step Ove	erview	36
3.2	CAD Me	odelling of Turbine Blade	36
3.3	Domain	and Meshing of Blade Geometry	38
	3.3.1	Mesh quality	40
3.4	Grid Ind	ependence Test	41
3.5	Selection	n of setting and model for CFD	42
	3.5.1	Selection of numerical model	42
	3.5.2	Selection of viscous model	44
	3.5.3	Selection of cavitation model	45
	3.5.4	Selection of settings and mathematical model summary	47
3.6	Validatio	on	49
3.7	Artificia	l Cavitation Generator installation	50
3.8	Twisting	g angle modification on turbine blade	50
CHA	PTER 4	RESULTS AND DISCUSSION	51
4.1	Validatio	on Results	51
	4.1.1	Validation results on final mesh of turbine blade	51
	4.1.2	Validation on viscous model	53

	4.1.3	Validation on cavitation model	53
4.2	Performa coefficier	nce analysis for the twisting angle of the turbine blade lift and dr	ag 58
4.3	Effect of	twisting angle and Artificial Cavitation Generator on cavitation	62
4.4	Performa	nce analysis for the effect of Artificial Cavitation Generator (AC	G) 63
	4.4.1	Artificial Cavitation Generator effect on lift coefficient and drag coefficient	64
4.5	The effec drag coef	et of turbine blade operating angle of attack upon lift coefficient a	nd 70
4.6	The turbi	ne blade optimal design analysis	72
CHAF	TER 5	CONCLUSION AND FUTURE RECOMMENDATIONS	74
5.1	Conclusio	Dn	74
5.2	Recomme	endations for Future Research	75
REFE	RENCES		78
APPEI	NDICES		

### LIST OF TABLES

Page
------

Table 2.1	The value of parameters in simulation setup
Table 3.1	Skewness and aspect ratio result for all geometry models40
Table 3.2	The settings and mathematical model specifics in ANSYS FLUENT
Table 3.3	The initial condition parameter setup in ANSYS FLUENT49
Table 3.4	The coordinate of the ACG on top surface of turbine blade50
Table 4.1	The tabulated data of lift, drag and moment coefficient for validation
Table 4.2	The tabulated data of lift and drag coefficient for validation53
Table 4.3	The tabulated data of lift coefficient for varied twisting angle58
Table 4.4	The tabulated data of drag coefficient for varied twisting angle59
Table 4.5	The tabulated data of pitching moment coefficient for varied twisting angle
Table 4.6	The tabulated data of vapour volume fraction and pressure change per iteration for varied twisting angle
Table 4.7	Lift coefficient for different angle of attack and twist angle with ACG installed
Table 4.8	Drag coefficient for different angle of attack and twist angle with ACG installed
Table 4.9	Lift to drag coefficient for different angle of attack and twist angle with ACG installed

### LIST OF FIGURES

### Page

Figure 1.1	Labelled diagram of horizontal axis hydrokinetic turbine21
Figure 1.2	Classification of hydrokinetic turbines
Figure 1.3	(a)Labelled diagram of hydrofoil, (b) Top view of turbine blade showing twist angle of 10 <sup>o</sup>
Figure 1.4	Illustration of cavitation phenomenon (Slurryflo 2020)24
Figure 1.5 Ero	sion damage caused by cavitation phenomenon (Catty Pattel. 2021)
Figure 1.6	Illustration of Artificial Cavitation Generator
Figure 1.7	Illustration of Artificial Cavitation Generator (a)side view and (b) isometric view
Figure 2.1	Illustration of Artificial Cavitation Generator on CAV200330
Figure 3.1	The workflow of methodology
Figure 3.2	(a) Blade with no ACG and 0° twist angle, (b) Blade with ACG and 0° twist angle, (c) Blade with CG and 6° twist angle
Figure 3.3	The ACG height, length and slant angle
Figure 3.4	The ACG height, length and slant angle
Figure 3.5	(a) Front view of domain (b) Side view of the length ratio for front and rear spacing of model with domain
Figure 3.6	Isometric view of domain with structured mesh
Figure 3.7	The sectioned symmetric view of geometry model meshing
Figure 3.8	Grid Independence Test results in terms of lift coefficient41
Figure 4.1	Vapour volume fraction at $\sigma=2$
Figure 4.2	Vapour volume fraction at $\sigma=1$

Figure 4.3	Graph of lift coefficient against cavitation number for experimental and simulated results
Figure 4.4	Graph of pitching moment coefficient against cavitation number for experimental and simulated results
Figure 4.5	Graph of drag coefficient against cavitation number for experimental and simulated results
Figure 4.6	Graph of lift coefficient for different twisting angle60
Figure 4.7	Graph of drag coefficient for different twisting angle60
Figure 4.8	Graph of pitching moment coefficient for different twisting angle61
Figure 4.9	Graph of lift coefficient against angle of attack for different twist angle with ACG installed
Figure 4.10	Graph of drag coefficient against angle of attack for different twist angle with ACG installed
Figure 4.11	Graph of lift to drag coefficient against angle of attack for different twist angle with ACG installed67
Figure 4.12	Vapour volume fraction contour from 1 second to 4 seconds flow time for $\alpha$ =4° and $\sigma$ =-6°
Figure 4.13	Vapour volume fraction contour from 1 second to 4 seconds flow time for $\alpha=0^{\circ}$ and $\sigma=-6^{\circ}$
Figure 4.14	The flow streamline around turbine blade at angle of attack 0°71
Figure 4.15	The flow streamline around turbine blade at angle of attack 12°71

### LIST OF SYMBOLS

$C_{1\epsilon}$	Constant with value of 1.44
$C_{2\epsilon}$	Constant with value of 1.92
$C_{3\epsilon}$	Constant with value of 0.09
Cd	Drag coefficient
Cı	Lift coefficient
Cı/Ca	Ratio of lift coefficient to drag coefficient
Cp	Pressure coefficient
F <sub>D</sub>	Drag force, N
FL	Lift force, N
G <sub>b</sub>	Generation of turbulence kinetic energy due to buoyancy
$G_k$	Generation of turbulence kinetic energy due to the mean velocity
	gradients
k	Turbulence kinetic energy
n	Bubble density numbers
Р	Local far-field pressure, Pa
$P_B$	Bubble surface pressure, Pa
Plocal	Local fluid static pressure, Pa
Pref	Reference hydrostatic pressure, Pa
$P_{v}$	Saturation vapor pressure, Pa
R	Mass transfer rate, m/s
$R_B$	Bubble radius, mm

Rc	Mass transfer source terms connected to the collapse of the vapor
	bubbles
Re	Mass transfer source terms connected to the growth of the vapor
	bubbles
$S_{ij}$	Strain rate tensor
Sk	User-defined source terms for k
S∈	User-defined source terms for $\epsilon$
V	Free stream flow velocity, m/s
$\overrightarrow{V_{v}}$	Vapor phase velocity, m/s
Yм	Contribution of the fluctuating dilatation in compressible turbulence
	to the overall dissipation rate
α	Vapor volume fraction
ρ	Fluid density, kg/m3
ρι	Liquid density, 998.2 kg/m3
$ ho_v$	Vapor density, kg/m3
σ	Cavitation number
$\sigma_k$	Turbulent Prandtl numbers for k with constant value 1.0
$\sigma_\epsilon$	Turbulent Prandtl numbers for $\epsilon$ with constant value 1.3
V	Vapor phase
π	Pi number, constant value 3.142
ε	epsilon
τij	Viscous stress tensor
μ	Effective molecular viscosity
$\delta_{ij}$	Kronecker delta function

### LIST OF ABBREVIATIONS

- ACG Artificial cavitation bubble generator
- CAD Computer-aided design
- CFD Computational Fluid Dynamics
- GIT Grid Independent Test
- RE Renewable energy
- RNG Renormalization group
- 2D 2-Dimensional
- 3D 3-Dimensional
- USM Universiti Sains Malaysia

### LIST OF APPENDICES

Appendix AThe Sample Graphs From Ansys Simulation Of Twisting Angle<br/>Of 10°

#### **CHAPTER 1**

#### **INTRODUCTION**

#### 1.1 Malaysia's Current Energy Background

Renewable energy (RE) has been the eye of focus of Malaysian government over the past decade. The 10 years' plan, Malaysia Energy Supply Industry 2.0 (MESI 2.0) was launched by Malaysian government as an initiative to rev up the country's RE capacity. The government has planned to rev up the RE capacity by 20 percent by the year 2025. Malaysian government resort to this initiative as a result of increase in emission of carbon dioxide, carbon monoxide, greenhouse effect and other pollutions such as acid rains. Thus, the government decided to be less dependent on fossil fuels, petroleum and other pollution friendly fuel sources. Looking into statistics, until 2016, up to 86.7% electricity generation in Malaysia were solely dependent on non-renewable energy resource which consists of coal, natural gas and petroleum. Whereas, the remaining 13.3% of electricity generation depends on renewable energy resource which consist of solar, wind and hydro (Suruhanjaya Tenaga, 2017, p. 34). Amidst of all the renewable energy, hydro energy has the most potential to be efficiently and massively implemented due to the geographical terrain and certain climate occurrence of Malaysia. For instance, Malaysia have many large rivers and also have monsoon climate which improves the potential of hydro energy implementation. To be precise, Malaysia consist of 189 rivers with the length of 57300 km. (Abdullah et al. 2019).

#### 1.1.1 Hydro Energy

Hydro energy is a form of energy where it refers to the conversion from the motion of water into electrical energy. Hydro energy is under the category of renewable energy because water is continuously renewable throughout the water cycle. This hydro energy is commonly generated by devices called generators and turbines where the potential energy in the water converts into mechanical energy when it moves or spin the turbine blade and this mechanical energy turned into electrical energy due to the mechanism of the turbine or generator. Moreover, hydro plants can be specified into 3 types, which is Pump storage facility, Run-of-river facility and Impoundment facility (U.S. Department of Energy, 2003, p. 4). Usually the Impoundment facility is the typical hydro plant that will be implemented where dam is built to create a man-made reservoir, then the water from the reservoir will be directed through the large scale turbine to generate electricity. However, this method has its own drawback where the construction cost is high for the dam to be built, whereas the failure of the dam system will have massive impact on the surrounding ecosystem and landscape. On the contrary, the Runof-river facility shows promising result which does not require large construction cost. Thus, the hydrokinetic turbine shows large potential which may change Malaysia's future electrical energy generation system.

#### **1.2** Hydrokinetic Turbine

Hydrokinetic turbines are the new backbone of hydro energy harnessing system. These devices are recently developed which can convert the kinetic energy from the water current into electrical energy. The concept of hydrokinetic turbine is similar to wind turbine where the water is used to turn the turbine blades which generates electricity. The difference is just that a denser fluid, water moves the turbine blade instead of air. The most crucial components for a hydrokinetic turbine are briefly explained below (Oblas, 2016):

- a) Diffuser: The diffuser is the structural member which connects the leading components which consist of front shaft, runner hub, nose supports with trailing components which consist of rear components, mooring supports and nacelle. This component features to increase the available pressure drop across the turbine by drawing more fluid through the turbine.
- b) Gearbox: The gearbox serves to speed up the rotation rate of rotor when functioning.
- c) Generator: The generator converts the mechanical energy produced from the rotor to electrical energy.
- d) Nacelle: The nacelle act as a housing space for the turbine components and prevent the breach of water from affecting them.
- e) Runner: The runner consists of the blades mounted to the central hub. The design of runner is to mainly change the fluid flow power into rotary motion.



Figure 1.1 Labelled diagram of horizontal axis hydrokinetic turbine

### **1.2.1** Classification of hydrokinetic turbine

There are several types of hydrokinetic turbine which can be classified into 2 categories. The first category is the horizontal axis hydrokinetic turbine while the second category is the vertical axis hydrokinetic turbine. The first category, horizontal axis turbine has central axis of blades rotating normal to the vector of flowing water direction. The second category, vertical axis turbine has central axis perpendicular to the flowing water direction. While the vertical axis turbine does not need complicated blade design, the horizontal axis turbine needs a well-designed turbine blade to achieve desired performance. The classification of all the hydrokinetic turbines are as shown below:



Figure 1.2 Classification of hydrokinetic turbines

### **1.2.2** Blade Design of Hydrokinetic Turbine

The main critical criterion of a well performing hydrokinetic turbine is the turbine blade design. The turbine blades produce lift force which allows the rotor to rotate continuously. Thus, the design of the turbine blade has larger impact on the performance of the hydrokinetic turbine. The blades are usually constructed using hydrofoil shape. The hydrofoil shape technically has more curvature shape on the top surface than the bottom surface. The top surface and bottom surface has a flat line connecting both of it which is known as chord line. Then, the locus of mid-points between top surface and bottom surface known as the camber line. The front point intersecting the top surface and bottom surface known as the leading edge while the rear point of intersection known as trailing edge.

Little variation in twist angle has more effect on the performance of hydrokinetic turbine blade. The twist angle is very sensitive to the fatigue life of the blade than the chord length and the blade length (Liu et al., 2017). The fatigue life increases

exponentially with the increase in twist angle, while there is parabolic relation between the fatigue life of the blade and the chord length. The fatigue life decreases with increase in the blade length linearly. Due to increase in fatigue life of the blade, the cost of the hydrokinetic turbine plant gets reduced with more reliability. Hence the care should be taken about the twist angle of the hydrokinetic turbine blade while manufacturing. There should always be an optimum twist angle to get optimum power output.



Figure 1.3 (a)Labelled diagram of hydrofoil, (b) Top view of turbine blade showing twist angle of 10°

### **1.3** Cavitation Phenomenon

There is another critical aspect that influences the performances and the lifespan of hydrokinetic turbine blade which is cavitation. Cavitation is a phenomenon where the rapid fluctuation in pressure of flowing water causes the formation of vapor bubbles or known as cavities. To be precise about this phenomenon, when the local static pressure drops below the vapor pressure of liquid, this condition leads to the formation of the vapor bubbles. The vapor bubbles have tendencies to move to higher pressure region as water flow through the turbine blade passage. Then, when the local static pressure rises above the vapor pressure of the liquid due to, the vapor bubbles which present at the region collapse and cause an implosion. The vapor bubbles collapse because it could not withstand the high pressure. The implosion caused by the collapsing vapor bubbles will imitate a supersonic fluid micro jet which hits the surface of the turbine blade. This occurrence will cause surface erosion of the turbine blade. Thus, this affects the performance and lifespan of the turbine blade. Reduction of cavitation impact must be an important aspect taken into consideration when design hydrokinetic turbine blade. Figure 1.5 shown below is the image of erosion damage caused by cavitation phenomenon.



Figure 1.4 Illustration of cavitation phenomenon (Slurryflo 2020)