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Second Semester Examination  
2020/2021 Academic Session

July/August 2021

**EAS458 – Pre-Stressed Concrete Design**

Duration : 1 hour

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Please ensure that this examination paper contains **FIVE (5)** printed pages including appendix before you begin the examination.

**Instructions:** This paper contains **THREE (3)** questions. Answer **TWO (2)** questions.

All questions **MUST BE** answered on a new page.

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1. A simply supported post-tensioned prestressed beam of a rectangular section 300 mm wide is to be designed for a permanent load of 2.5 kN/m (excluding self-weight) and a variable load of 5.5 kN/m which is uniformly distributed on a span of 10 m. The member is to be designed with a concrete strength class C50/60. The equations for inequalities are given in the **Appendix**.

- (a). Taking the density of pre-stressed concrete to be 25 kN/m<sup>3</sup> and the characteristic compressive strength of the concrete at transfer is 33 MPa, determine the minimum depth of the beam if the losses are 20%.

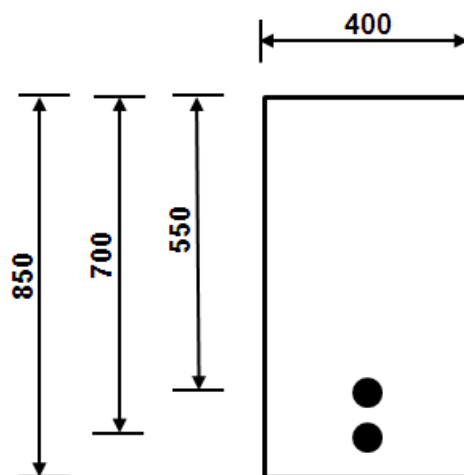
[18 marks]

- (b). If the economic value of pre-stressing force is to be designed for this section, determine the range of eccentricities at the mid-span for the cable zone limit.

[32 marks]

2. **Figure 1** shows the cross-section of a 400 mm × 850 mm post-tensioned beam at the mid-span and the corresponding double tendon. Each tendon consists of prestressing strand with area,  $A_{ps} = 1056 \text{ mm}^2$  and characteristic tensile strength,  $f_{pk} = 1770 \text{ N/mm}^2$ . If the initial pre-stress applied to each tendon is  $1000 \text{ N/mm}^2$  and 30% losses are anticipated, determine the ultimate moment of resistance for the section. Take  $f_{ck} = 40 \text{ N/mm}^2$ ,  $E_p = 205 \text{ kN/mm}^2$ ,  $\gamma_m = 1.15$  and  $\gamma_p = 0.9$ . Verify that  $x = 349 \text{ mm}$  can be used as the depth of the neutral axis.

[40 marks]



All dimensions in mm

Figure 1

- (b). In the case where the ultimate moment of resistance ( $M_{Rd}$ ) is found to be slightly lower than the design moment ( $M_{Ed}$ ), propose with justification **TWO (2)** economical methods that can be adopted in order to increase  $M_{Rd}$ .

[10 marks]

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3. **Figure 2** shows the end and side elevations of anchorage zone of a flexural member with the given dimensions. The size of the square bearing plate is 315 mm with a duct diameter of 106 mm. Given the strength of concrete at transfer is 35 MPa and jacking force is 3000 kN. Assuming the design load is  $1.15 P_j$  and  $\phi=0.6$ , determine

- (a). the design strength by considering bearing is taken as 50 % greater than the value obtained in the equation below.

$$F_b = \phi \times 0.85 f'_{ci} \sqrt{\frac{A_2}{A_1}} \quad (\leq \phi \times 1.7 f'_{ci})$$

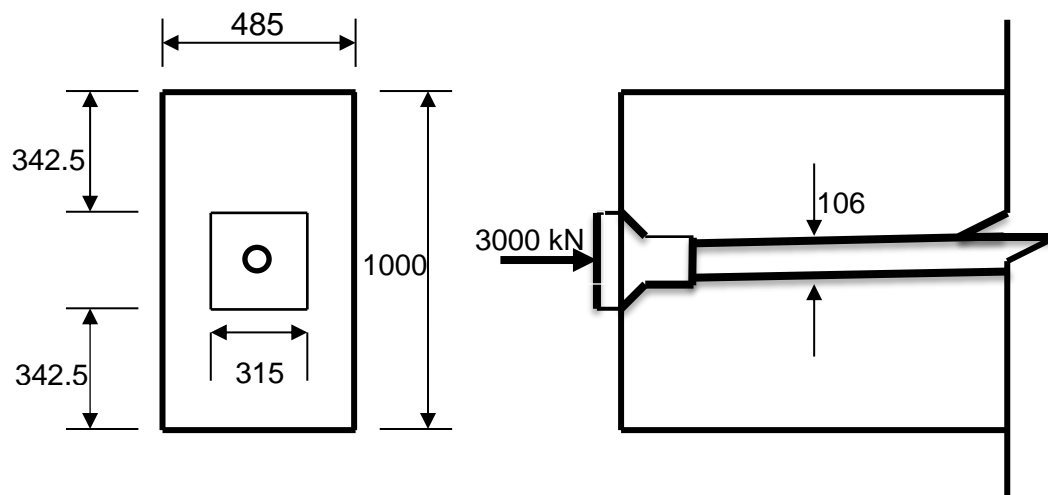
[15 marks]

- (b). the amount of vertical transverse reinforcement by assuming  $\sigma_s=150$  MPa.

[18 marks]

- (c). the amount of horizontal transverse reinforcement.

[17 marks]



All dimensions in mm

Figure 2

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**APPENDIX****Governing inequalities:****At transfer:**

$$\frac{P_{m0}}{A_c} - \frac{P_{m0}e}{Z_t} + \frac{M_0}{Z_t} \geq f_{ct,0} \text{ --- top fibre}$$

$$\frac{P_{m0}}{A_c} + \frac{P_{m0}e}{Z_b} - \frac{M_0}{Z_b} \leq f_{cc,0} \text{ --- bottom fibre}$$

**At service:**

$$\frac{P_{m,t}}{A_c} - \frac{P_{m,t}e}{Z_t} + \frac{M_T}{Z_t} \leq f_{cc,t} \text{ --- top fibre}$$

$$\frac{P_{m,t}}{A_c} + \frac{P_{m,t}e}{Z_b} - \frac{M_T}{Z_b} \geq f_{ct,t} \text{ --- bottom fibre}$$

**Minimum section moduli:**

$$(M_T - \Omega M_0) \leq (f_{cc,t} - \Omega f_{ct,0})Z_t$$

$$(M_T - \Omega M_0) \leq (\Omega f_{cc,0} - f_{ct,t})Z_b$$

**Losses:**

The remaining force after elastic shortening,  $P'$  (pretensioned) = 
$$\frac{P_{m0}}{1 + m \frac{A_p}{A_c} \left(1 + \frac{e^2 A_c}{I}\right)}$$

Loss of prestressing force due to creep = 
$$E_p P' \frac{A_p}{A_c} \left(1 + \frac{e^2 A_c}{I}\right) \left(\frac{\varphi(\infty, t_0)}{1.05 E_{cm,0}}\right)$$

Loss in prestressing force due to shrinkage = 
$$\varepsilon_{cs} E_p A_p$$

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