# MAXIMIZING PURITY AND RECOVERY OF CARBON DIOXIDE FROM BIOGAS BY EQUALIZED PRESSURE SWING ADSORPTION USING UiO66 ADSORBENT

TAN WERN KE

UNIVERSITI SAINS MALAYSIA

2018

# MAXIMIZING PURITY AND RECOVERY OF CARBON DIOXIDE FROM BIOGAS BY EQUALIZED PRESSURE SWING ADSORPTION USING UiO66 ADSORBENT

by

TAN WERN KE

Thesis submitted in partial fulfilment of the requirement for the degree of Bachelor of Chemical Engineering

June 2018

#### ACKNOWLEDGEMENT

First and foremost, I would like to express my highest gratitude to my supervisor, Prof. Dr. Mohd Roslee bin Othman for his endless support and precious advice for final year project research study. Whenever I needed assistance regarding my research, his assistance undeniably helped me a lots.

I would also extend my gratitude towards Dr.Iylia Idris for her kind cooperation and helping hands in guiding me. Next I am truly indebted to the postgraduates Ili Khairunnisa Binti Shamsudin and Aman Abdullah for guiding me in carrying out the lab experiment. They are willing to sacrifice their time in guiding and helping me throughout the experiment besides sharing their valuable knowledge.

Apart from that, I would also extend my utmost graditude to all School of Chemical Engineering staffs for their kind cooperation and helping hands. Indeed their willingness in sharing ideas, knowledge and skills are deeply appreciated. Once again, I would like to thank all the people, including those whom I might have missed out and my friends who have helped me directly or indirectly. Their contributions are very much appreciated. Thank you very much.

Tan Wern Ke

June 2018

### **TABLE OF CONTENTS**

ACK	NOWLEGMENT	ii
LIST	OF FIGURES	vii
LIT (	OF TABLES	X
LIST	OF SYMBOLS	xii
LIST	<b>OF ABBREVIATIONS</b>	xiii
ABST	ГРАК	xiv
ABST	ΓRACT	XV
CHA	PTER ONE: INTRODUCTION	1
1.1	Research Background	1
1.2	Problem statement	5
1.3	Research Objectives	6
CHA	PTER TWO: LITERATURE REVIEW	7
2.1	Biogas	7
2.2	Adsorption	.9
2.3	Pressure Swing Adsorption	10
2.4	Adsorbent	13
2.5	Zirconium-benzenedicarboxylate UiO66 Adsorbent	16
2.6	Breakthrough study	17
2.7	Breakthrough Study of CO2 Removal Using UiO66	18
2.8	Effect of adsorption time and blowdown time in PSA	19

2.9	Design Expert Response Surface Methodology (RSM) for optimization in	
	PSA	20
CHA	APTER THREE: MATERIALS AND METHOD	21
3.1	Research Methodology	21
3.2	Materials and Chemicals Required	22
3.3	Equipment Required	23
3.4	Adsorbent Preparation	24
3.4	.1 Zirconium-benzenedicarboxylate (UiO-66)	24
3.5	Adsorbent Characterization	25
3.5	.1 X-Ray Diffraction (XRD) Analysis	25
3.5	.2 Brunauer–Emmett–Teller (BET) Analysis	26
3.5	.3 Scanning Electron Microscope (SEM) Analysis	26
3.5	.4 Energy Dispersive X-Ray (EDX) Analysis	27
3.5	.5 Particle Size Analysis	27
3.6	Breakthrough Study	28
3.6	.1 Procedure of breakthrough studies	29
3.7	Design Expert Central Composite Design (RSM)	30
3.8	Pressure Swing Adsorption Studies	33
CHA	<b>APTER FOUR: RESULTS AND DISCUSSION</b>	37
4.1	Characterization of Adsorbents	37
4.1	.1 X-Ray Diffraction Analysis	37

4.1	.2 Brunauer–Emmett–Teller (BET) Analysis	39
4.1	.3 Scanning Electron Microscope (SEM) and Energy Dispersive X-Ray	
	(EDX) Analysis	42
4.1	.4 Particle Size Analyzer	44
4.2	Breakthrough Studies	45
4.2	2.1 Breakthrough Curve at pressure 3 bar	46
4.3	Design Expert Central Composite Design (RSM)	47
4.3	3.1 Experimental Design	47
4.3	3.2 Regression Equations and Model Fitting for Column 1	49
4.3	3.3 Analysis of variance (ANOVA) for column 1	50
4.3	3.4 Regression Equations and Model Fitting for Column 2	53
4.3	3.5 Analysis of variance (ANOVA) for column 2	54
4.3	3.6 Effect of Variables on the Selected Responses for column 1	56
4.3	3.7 Effect of Variables on the Selected Responses for column 2	58
4.3	8.8 Solution of optimisation high CO <sub>2</sub> and CH <sub>4</sub> purity and recovery for	
	column 1 and column 2	61
4.3	8.9 Validation of optimisation result of the models	63
4.3	3.10Comparison of experimental optimisation result of Palm Kernel Shell	
	Activated Carbon and UiO66 adsorbent.	64
CHA	APTER FIVE: CONCLUSIONS AND RECOMMENDATIONS	65
5.1	Conclusions	65

#### 5.2 Recommendations

#### REFERENCES

#### **APPENDICES**

APPENDIX A: UiO66 ADSORBENT APPENDIX B: PSA EQUIPMENT APPENDIX C: X'PERT HIGH SCORE SOFTWARE APPENDIX D: GAS CHROMATOGRAPH CALIBRATION CURVE APPENDIX E: BREAKTHROUGH CALCULATION APPENDIX F: DESIGN EXPERT RESULTS 66 68

77

### LIST OF FIGURES

		Page
Figure 1.1	Global Production and Consumption of energy from natural gas from 1989 to 2014	1
Figure 1.2	Global price of natural gas	2
Figure 1.3	Total number of biogas upgrading plants	3
Figure 1.4	Classification of application technologies for separation of CO <sub>2</sub>	4
	from methane (biogas upgrading)	
Figure 1.5	Classification of the distribution of technologies applied in	4
F' 0 1		10
Figure 2.1	Adsorption system consisting of a two component sorptive gas, adsorbate and the adsorbent.	10
Figure 2.2	Schematic design of the first two-column pressure swing	12
	adsorption unit and valve sequencing for different steps in the	
	cycle	
Figure 2.3	Schematic diagram of pore structure of adsorbent	13
Figure 2.4	Cluster structure of UiO66 adsorbent with its linker 1,4-	16
	benzene-dicarboxylate	
Figure 2.5	Solid concentration profile at different times	18
Figure 3.1	General layout of research flow diagram	21
Figure 3.2	X-ray Diffractometer (Bruker XRD D8)	25
Figure 3.3	Surface area and porosity analyzer (ASAP 2020)	26
Figure 3.4	Scanning electron microscope (Quanta FEG450)	27
Figure 3.5	Particle size analyzer (CILAS 1180).	28
Figure 3.6	Pressure swing adsorption flow integrated design (FID)	30
Figure 3.7	Rotatable design	32
Figure 3.8	Set of experiments	32
Figure 3.9	PSA cycle	33
Figure 4.1	Figure 4.1: XRD patterns of UiO66 adsorbent synthesized at	37
	120°C, 1atm about 30 minutes from mixture ZrCl <sub>4</sub> ,	
	dimethylformamide (DMF) and 1,4 benzendicarbolylix	
	acid(BDC), cooling time duration 2 hours, precipitate washed	
	and dried at 70°C	

- Figure 4.2 Nitrogen sorption isotherms for UiO66 adsorbent synthesized 40 at 120°C, 1atm about 30 minutes from mixture ZrCl<sub>4</sub>, dimethylformamide (DMF) and 1,4 benzendicarbolylix acid(BDC), cooling time duration 2 hours, precipitate washed and dried at 70°C
- Figure 4.3 SEM micrographs of UiO66 adsorbent synthesized at 120 °C, 42 1atm about 30 minutes from mixture ZrCl<sub>4</sub>, dimethylformamide (DMF) and 1,4 benzendicarbolylix acid(BDC), cooling time duration 2 hours, precipitate washed and dried at 70°C at magnifications of (a) 5 KX, (b) 10.00 KX and (c) 20.00KX
- Figure 4.4 EDX analysis of UiO-66 UiO66 adsorbent synthesized at 43 120°C, 1atm about 30 minutes from mixture ZrCl<sub>4</sub>, dimethylformamide (DMF) and 1,4 benzendicarbolylix acid(BDC), cooling time duration 2 hours, precipitate washed and dried at 70°C
- Figure 4.5 Particle Size Distribution of UiO-66 synthesized at 120°C,1atm 44 about 30 minutes from mixture ZrCl<sub>4</sub>, dimethylformamide (DMF) and 1,4 benzendicarbolylix acid(BDC), cooling time duration 2 hours, precipitate washed and dried at 70°C
- Figure 4.6 Breakthrough curves for methane and carbon dioxide using 46 UiO66 adsorbent synthesized at 120 °C,1atm about 30 minutes from mixture ZrCl4,dimethylformamide (DMF) and 1,4 benzendicarbolylix acid(BDC), cooling time duration 2 hours, precipitate washed and dried at 70°C with fixed feed gas compositions (70%CO<sub>2</sub> and 30%CH<sub>4</sub>) and 3 bar

- Figure 4.7 plots depicting the effect of adsorption time (minutes) and 57 blowdown time (minutes): (a) Purity of CO<sub>2</sub>(%) and Recovery of CO<sub>2</sub> (%) at constant blowdown time 2.5 minutes; (b) Purity of CO<sub>2</sub>(%) and Recovery of CO<sub>2</sub> (%) at constant adsorption time 2.5 minutes and (c) Purity of CH<sub>4</sub> (%) and Recovery of CH<sub>4</sub>(%) at constant blowdown time 2.5 minutes and (d) Purity of CH<sub>4</sub>(%) at CH<sub>4</sub>(%) and Recovery of CH<sub>4</sub>(%) at constant adsorption time 2.5 minutes for column 1
- Figure 4.8 plots depicting the effect of adsorption time (minutes) and 59 blowdown time (minutes): (a) Purity of CO<sub>2</sub>(%) and Recovery of CO<sub>2</sub> (%) at constant blowdown time 2.5 minutes; (b) Purity of CO<sub>2</sub>(%) and Recovery of CO<sub>2</sub> (%) at constant adsorption time 2.5 minutes and (c) Purity of CH<sub>4</sub> (%) and Recovery of CH<sub>4</sub>(%) at constant blowdown time 2.5 minutes and (d) Purity of CH<sub>4</sub>(%) at constant blowdown time 2.5 minutes and (d) Purity of CH<sub>4</sub>(%) and Recovery of CH<sub>4</sub>(%) at constant adsorption time 2.5 minutes for column 2

62

Figure 4.9 Desirability analysis in maximizing purity and recovery of CO<sub>2</sub> and CH<sub>4</sub> (a) column 1 (b) column 2

# LIST OF TABLES

		Page
Table 2.1	Biogas upgrading process in reducing global warming potential	8
Table 2.2	Result of comparison of the selection criteria necessary for	15
	CO <sub>2</sub> capture	
Table 3.1	List of materials and chemicals	22
Table 3.2	List of equipment	23
Table 3.3	List of items used for the breakthrough study	28
Table 3.4	Adsorption bed configuration parameters	30
Table 3.5	Numeric factors and their coded levels	31
Table 3.6	Dependents factors (responses)	31
Table 4.1	Crystal size and lattice strain of 3 peaks of UiO66 adsorbent	38
	synthesized at 120 °C,1atm about 30 minutes from mixture	
	ZrCl <sub>4</sub> ,dimethylformamide(DMF) and 1,4 benzendicarbolylix	
	acid(BDC), cooling time duration 2 hours, precipitate washed	
	and dried at 70°C.	
Table 4.2	Properties of UiO66 adsorbent synthesized at 120 °C,1atm	39
	about 30 minutes from mixture ZrCl4,dimethylformamide	
	(DMF) and 1,4 benzendicarbolylix acid(BDC), cooling time	
	duration 2 hours, precipitate washed and dried at 70°C.	
Table 4.3	Elemental analysis of UiO66 adsorbent synthesized at	44
	120 °C,1atm about 30 minutes from mixture	
	ZrCl <sub>4</sub> ,dimethylformamide(DMF) and 1,4 benzendicarbolylix	
	acid(BDC), cooling time duration 2 hours, precipitate washed	
	and dried at 70°C	
Table 4.4	Elemental analysis of UiO66 adsorbent synthesized at	45
	120 °C,1atm about 30 minutes from mixture	
	ZrCl <sub>4</sub> ,dimethylformamide(DMF) and 1,4 benzendicarbolylix	
	acid(BDC), cooling time duration 2 hours, precipitate washed	
	and dried at 70°C	

- Table 4.5Independent variables and experimental values of the<br/>response variables for the central composite design (CCD) in<br/>Column 148Table 4.6Independent variables and experimental values of the49
- response variables for the central composite design (CCD) in Column 2.
- Table 4.7Analysis of variance results for response surface linear model51for purity of CO2(%) in column 1
- Table 4.8Analysis of variance results for response surface quadratic51model for recovery of CO2(%)in column 1
- Table 4.9Analysis of variance results for response surface linear model52for purity of CH4 (%) in column 1.
- Table 4.10Analysis of variance results for response surface quadratic52model for recovery of CH4 (%) in column 1
- Table 4.11Analysis of variance results for response surface quadratic54model for purity of CO2(%) in column 2
- Table 4.12Analysis of variance results for response surface quadratic for55model recovery of CO2 (%) in column 2.
- Table 4.13Analysis of variance results for response surface quadratic55model for purity of CH4 (%)in column 2
- Table 4.14Analysis of variance results for response surface quadratic56model for recovery of CH4 (%)in column 2
- Table 4.15Predicted (P) vs. Experimental (M) values for validation data63
- Table 4.16 Palm Kernel Shell activated carbon (PKS) vs. UiO66 64 adsorbent (U) values for responses data at 3.2 minutes (adsorption times) and 2.737 minutes (blowdown time) at pressure 3 bar for column 1 and 3.2 minutes (adsorption times) and 3 minutes (blowdown time) at pressure 3 bar for column 2

xi

# LIST OF SYMBOLS

	Symbol	Unit
Å	Interatomic distance	m
SABET	Specific surface area (Brunauer–Emmett–Teller)	$m^2/g$
tb	Breakthrough time	min
ts	Saturation time	min
Θ	Scattering angle	o
V	Voltage	V

# LIST OF ABBREVIATIONS

NBP	National Balancing Point
LNG	Liquefied Natural Gas
BABIU	Bottom Ash Upgrading
AwR	Alkaline with Regeneration
HPWS	High Pressure Water Scrubbing
As	Chemical Scrubbing
Cry	Cryogenic Separation
OPS	Organic Physical Scrubbing
MS	Membrane Separation
UiO66	Zirconium 1,4-dicarboxybenzene MOF
BDC	1,4-benzenedicarboxylic acid
PSA	Pressure Swing Adsorption
TSA	Temperature Swing Adsorption
VPSA	Vacuum Pressure Swing Adsorption
ppm	Parts Per Million
MOF	Metal organic framework
CCD	Central Composite Design
RSM	Response Surface Methodology
ANOVA	Analysis of variance
BET	Brunauer–Emmett–Teller
EDX	Energy dispersive x-ray
SEM	Scanning electron microscope
XRD	X-ray diffractometer
GC	Gas Chromatograph
IUPAC	International Union of Pure and Applied Chemistry

#### ABSTRAK

Harga gas asli yang semakin tinggi disebabkan oleh keperluan tinggi dan isu-isu percemaran alam sekitar yang disebabkan oleh pelepasan metana dan karbon dioksida(gas rumah hijau) daripada biogas telah menyumbang kepada menaikkan taraf biogas. Dalam Kajian ini, penjerap UiO66 telah dipilih untuk menaikkan taraf biogas. Penjerap UiO66 telah disediakan dan dicirikan dengan menggunakan analisa Pembelauan Sinar-X (XRD), analisa Brunauer-Emmett-Teller (BET), analisa Mikroskopi Elektron Imbasan (SEM), analisa X-Ray Tenaga Sebaran (EDX) dan analisa saiz partikel. Ujian pencirian menunjukkan penjerap UiO66 ialah berliangmeso, kristal struktur dan bentuk celah serta mempunyai BET kawasan permukaan yang rendah. Kajian masa titik bolos dilakukan pada penjerap UiO66 dengan menggunakan komposisi gas(30%CH<sub>4</sub>-70%CO<sub>2</sub>) dalam tekanan 3 bar. CO<sub>2</sub> dibuktikan sedikit baik daripada CH<sub>4</sub> bila diserapkan ke dalam penjerap UiO66 kerana masa titik bolos CO<sub>2</sub> panjang sikit daripada titik bolos CH<sub>4</sub>. Masa pelepasan dan penyerapan telah ditentukan berdasarkan pada masa titik bolos dan masa tepu untuk memperolehi ketulenan dan pemulihan gas karbon dioksida dan metana daripada penjerapan buaian tekanan. Maksimum ketulenan and pemulihan gas CO<sub>2</sub> ialah 82.70% dan 36.24%, maksimum ketulenan and pemulihan gas CH<sub>4</sub> ialah 38.22% dan 86.92% dalam 3.2 minit (masa penyerapan) dan 3minit (masa pelepasan) dengan menggunakan tekanan 3 bar.

# MAXIMIZING PURITY AND RECOVERY OF CARBON DIOXIDE FROM BIOGAS BY EQUALISED PRESSURE SWING ADSORPTION USING UiO66 ADSORBENT

#### ABSTRACT

High price of natural gas due to high demand and environmental issues that caused by releasing methane and carbon dioxide (greenhouse gases) from biogas make biogas upgrading necessary. In this study, UiO66 adsorbent in pressure swing adsorption (PSA) processes was selected for biogas upgrading. The UiO66 adsorbent was prepared and characterized using X-Ray Diffraction (XRD) analysis, Brunauer-Emmett-Teller (BET) Analysis, Scanning Electron Microscope (SEM) analysis, Energy Dispersive X-Ray (EDX) analysis and Particle Size Analysis. The characterization tests showed that UiO-66 was mesoporous, slit-shaped, has low BET surface area and crystalline structure. Breakthrough study was carried out on the UiO66 adsorbent with feed gas composition (30%CH<sub>4</sub> - 70% CO<sub>2</sub>) under 3 bar. CO<sub>2</sub> is the slightly strong adsorbed species compared to CH<sub>4</sub> in a UiO66 adsorbent which was proven by its slightly longer breakthrough time than CH<sub>4</sub> breakthrough time. Blowdown and adsorption time were selected based on breakthrough and saturated time and applied in PSA to obtain purity and recovery of CO<sub>2</sub> and CH<sub>4</sub>. Maximum purity and recovery of CO<sub>2</sub> are 82.70% and 36.24% respectively whereas maximum purity and recovery of CH<sub>4</sub> are 38.22% and 86.92% respectively at 3.2 minutes of adsorption time and 3 minutes of blowdown time under 3 bar.

# CHAPTER ONE INTRODUCTION

Chapter one introduces the overview of this research and how pressure swing adsorption (PSA) is significant for the capture of carbon dioxide (CO<sub>2</sub>) gas for biogas upgrading. In general, this chapter outlines the research background of raising price of natural gas, environment problems and pressure swing adsorption for biogas upgrading, the problem statement and objectives of this study.

#### 1.1 Research Background

Natural gas well was first drilled in 1821 by William Hart and the gas, natural gas generate significant energy that bring great impact towards transport, industry, residential and power sector. Production and consumption on natural gas globally increase from low level in year 1989 to a yearly output of nearly 3500 Billion Cubic Meters in the year 2014 as illustrated in Figure 1.1.



Figure 1.1: Global Production and Consumption of energy from natural gas from 1989 to 2014 (Faramawy *et al.*, 2016)

Consumption of natural gas resource can be distributed into 4 areas which are Asia pacific, Europe & Eurasia, North America and the rest of world with accounting for 19.9%, 29.6%, 28.3% and 22.2%. Almost the same, the percentage of production of natural gas in those areas just slightly higher than consumption of natural gas resource. Although there is enough supply of natural gas but the high demand of natural gas will be the key indicator to cause the raising in price. Figure 1.2 depicts the global price of natural gas.



Figure 1.2: Global price of natural gas (Energy, 2015)

In 2014, the price of natural gas (US Henry Hub, Average German Import Price cif, UK National Balancing Point (NBP) and Japan Liquefied Natural Gas (LNG) cif still remain higher than the price in 1997. These hikes price of natural gas is the leading source in upgrading biogas. Biogas mainly consist of carbon dioxide and methane. Biogas upgrading can be act as substitution of natural gas by removing impurity carbon dioxide,  $CO_2$  and increasing the methane rating (Petersson and WELLINGE, 2009).



Figure 1.3:Total number of biogas upgrading plants (Petersson and WELLINGE, 2009)

From year 1987 to 2009, the importance of biogas upgrading have been widespread into many countries like Japan, Iceland, Switzerland, Netherlands, Germany, France and Austria. Therefore, figure 1.3 show clearly the trend, the total number of biogas upgrading plant have been increased drastically from 3 to 99.

Besides, not only reducing the price of natural gas, biogas upgrading also gain environment benefit of avoiding greenhouses gases methane and carbon dioxide emission to atmosphere. Carbon dioxide,  $CO_2$  was separated and stored whereas the methane can be directly used as production of heat and steam, electricity, vehicle fuel and chemicals. Thus, importance of technologies separating between carbon dioxide and methane raise the attention worldwide (Starr Durany *et al.*, 2012). Figure 1.4 classifies the technologies of removing  $CO_2$  from methane (biogas upgrading) and Figure 1.5 classifies the distribution of technologies applied in industrial.



Figure 1.4: Classification of application technologies for separation of CO<sub>2</sub> from methane (biogas upgrading) (Warren, 2012)



Figure 1.5: Classification of the distribution of technologies applied in industrial (HOYER *et al.*, 2016)

5 important technologies that can be applied to separate out  $CO_2$  for biogas upgrading are adsorption, absorption, membrane, cryogenic and biological. Among these technologies, pressure swing adsorption have been acknowledged as third largest technology employed in biogas upgrading just behind the chemical scrubber technology which is 72 as stated in figure 1.5. PSA is a cyclic batch process where adsorptions are carried out at a comparatively higher pressure and desorption is accomplished at a lower pressure. In order to maximizing the purity and recovery of certain gas, type of adsorbent and the time evolution for gas adsorption play a vital role(Grande, 2012).

#### **1.2 Problem statement**

Biogas can be obtained during anaerobic digestion by breaking down organic material using different type of microorganism. In general, biogas composition consists of 40-70% methane, 30-60% carbon dioxide and small trace amount of hydrogen and hydrogen sulphide (Kossmann and Pönitz, 2007) whereas natural gas consist of 80-90% methane, 5% carbon dioxide and other gases (Faramawy *et al.*, 2016). Biogas and natural gas always have an unbreakable relationship. Both of them are renewable resources to generate electricity or act as fuel vehicle. However, natural gas seem to have more market value and high price when the demand increase yearly. In order to increase market value of biogas, researches were most likely to be conducted to reduce the  $CO_2$  level because carbon dioxide reduce total energy calorific value of fuel gas.Moreover, $CO_2$  is an acidic gas. It can become carbonic acid upon contact with moisture such as shown by equation 1.

$$CO_2 + H_2O \to H_2CO_3 \tag{1}$$

This acid tends to corrode the pipeline and equipment which can increase the maintenance cost as well.

#### **1.3** Research Objectives

The objectives of this research project are:

- To prepare and characterize Zirconium-benzenedicarboxylate (UiO66) in terms of surface area, surface morphology and surface chemistry.
- To study the breakthrough analysis of carbon dioxide and methane gas using Zirconium-benzenedicarboxylate (UiO66).
- iii) To obtain the highest CO<sub>2</sub> and CH<sub>4</sub> purity & recovery and by optimizing time of adsorption and blowdown using Design Expert software.

# CHAPTER TWO LITERATURE REVIEW

Chapter two briefly presents the previous discoveries and reviews available from credible scientific records and references that are related to this research topic. In general, this chapter outlines the overview of biogas, adsorption, and of significance, pressure swing adsorption (PSA) and adsorbent, specific UiO66. Then, a review on breakthrough studies involving UiO66 is presented to signify the importance of use in this research. Next, an extensive review of significance, pressure swing adsorption (PSA) is presented covering optimization and effect of the selected adsorption process variables.

#### 2.1 Biogas

Biogas is one of the clean and renewable alternative energy that work as combustion fuel. Biogas main composition comprised of CH<sub>4</sub> and CO<sub>2</sub> and it is originated from feedstock agricultural, manure, crop residues, municipal waste (MSW) and industrial organics via anaerobic digestion process involving different types of microorganisms. Anaerobic process took place through 4 crucial steps which are 1) hydrolysis 2) Acidogenesis 3) Acetogenesis and 4) Methanogenesis. (Demirbas and Balat, 2009)

Specific emphasis also should be place on environment problems which is emission of greenhouses gases ( $CO_2$  and  $CH_4$ ) that contribute to global warming. Manure, sewage, waste water from livestock farm and industrial plant, as well as agricultural waste release biogas that contain of  $CO_2$  and  $CH_4$  which are not utilised and discharged to atmosphere, eventually causing environment issues. Therefore, there must be some technologies to be applied. Table 2.1 showcase the biogas upgrading process in reducing global warming potential.

<b>Upgrading Process</b>	Global Warming Potential(g of	
	CO <sub>2</sub> .Eqv)	
BABIU	-1977	
AwR	-1794	
HPWS	-1766	
As	-1761	
Cry	-1758	
PSA	-1714	
OPS	-1691	
MS	-1489	

Table 2.1:Biogas upgrading process in reducing global warming potential (Starr

Pressure swing adsorption (PSA) that recognised as mature technology requires more research and studies to improve the recovery and purity of  $CO_2$  and then to be stored whereas high methane rating can be utilised to largely reduce the global warming potential.

Durany et al., 2012)

#### 2.2 Adsorption

Adsorption processes may be classified as purification or bulk separation, depending on the concentration in the feed of the components to be adsorbed (Seader et al., 2010). The solid that adsorbs a component is called the adsorbent, and the component adsorbed is called adsorbate. Adsorption may happen on the surface of liquid but it is less practical importance than adsorption in solid. The adsorption process occurred because of the interaction between the adsorbate molecules and the surface of the adsorbent. If the sorbed molecules attach to the surface, the process is called adsorption whereas the sorbed molecules are distributed throughout a liquid phase, the process is called absorption. The reverse of adsorption is called desorption. Pressure and temperature both are important factor to be used to determine out the amount of solute adsorbed per unit mass of adsorbent at equilibrium. Adsorption is favoured at high pressure and low temperature. On the contrary, desorption is favoured at low pressure and high temperature. Other than that, the strength of attachment between adsorbate and adsorbent is relied on the chemical or physical bonds that formed. For the strong chemical bond that formed between them can be known as chemisorption whereas the weak Van der Waal's force and electrostatic force that promote the physical bond is called as physical adsorption (DUTTA, 2007). Figure 2.1 illustrate the process of adsorption.



Figure 2.1: Adsorption system consisting of a two component sorptive gas, adsorbate and the adsorbent.(Keller and Staudt, 2005)

The interaction between adsorbent and adsorbate in terms of transferring of molecules from the gas or liquid phase to the surface of the solid phase, normally an exothermic process. Conversely, desorption is the transfer of molecules sticking to the surface of the solid back to the gas or liquid phase, normally an endothermic process.

#### 2.3 Pressure Swing Adsorption

Pressure Swing adsorption(PSA) is one of the separation technology can be widely applied in different applications for example hydrogen purification, air separation, OBOGS (on-board gas generation system) CO<sub>2</sub> removal, noble gases (He, Xe, Ar) purification, CH<sub>4</sub> upgrading, n-iso paraffin separation, and so forth (Grande, 2012). Pressure swing adsorption technology always been selected to investigate due to its low energy, cost effective and ease of operation when compared with other technologies. For instance, cryogenic processes require the equipment and devices, like compressors, turbines, heat exchangers, insulators, and distillation columns in result of high capital cost (Sarkar, 2016).In biogas upgrading, amine scrubber need high heat temperature in associate to heat up the amine solvent about 150-170 °C for regeneration and maintaining the adsorption efficiency. Undoubtedly, it will consume massive amount of energy in term of high cost and raise up the concern about safety issue (Miltner *et al.*, 2017).

Pressure swing adsorption, PSA is a cyclic process which employs equilibrium establishment in separation and mass transfer rate driven among adsorbate and adsorbent. When high pressure is applied, adsorption will occur and increase the amount of adsorbed impurities leading to high purity of product. Whereas when the pressure is reduced and reached back to atmospheric pressure, regeneration will occur, impurities can be desorbed and discharged from the system. This shown that relationship of equilibrium concentration of adsorbed impurities with the pressure. If the pressure is significantly reduced below the atmospheric pressure it is called as vacuum swing adsorption (VSA).For the mass transfer rate, it is greatly depend on the suitable selection of adsorbent that well installed in PSA system and has matching pore size for the given adsorbate species to make it preferably to be adsorbed (Seader *et al.*, 2010).

Pressure swing adsorption consist of two or more beds that installed by adsorbents and operated by means of proper valves arrangement. The term 'swing' in PSA represent high pressure in feed change to low pressure while regeneration. PSA technology was firstly introduced by Charles Skarstorm, the four step of 'Skarstrom cycle' will be feed, blowdown, purge and pressurization. Figure 2.2 shows the schematic design of the PSA.



Figure 2.2: Schematic design of the first two-column pressure swing adsorption unit and valve sequencing for different steps in the cycle (Grande, 2012)

If the pressure in the system replaced by temperature, which mean low temperature in feed and high temperature at regeneration process. It can be considered as temperature swing adsorption (TSA). Temperature swing adsorption (TSA) has its own benefit and drawback. TSA can be adopted during strong adsorption of mixture impurities to adsorbent in result good regeneration. However, TSA cycle time is much longer than PSA(Crittenden and Thomas, 1998). In the years after Skarstrom invention, pressure equalization step was introduced to modify Skarstrom cycle to improve energy recovery. (Chua *et al.*, 2013) employed formula equations to evaluate energy converse by using pressure equalization step whereas (Yang *et al.*, 1997) studied effect of pressure equalization time on H<sub>2</sub> purity and recovery for H<sub>2</sub>/CH<sub>4</sub> separation. Longer the step time, the better of recovery and purity obtained.

#### 2.4 Adsorbent

Selection of adsorbent always be the first consideration for the designation of PSA (Jain *et al.*, 2003).Different type of solid adsorbents like zeolites, molecular sieve, silica gel and activated carbon all of them have their own attributes that pose a strength in binding toward their selective separation of mixture. It is noted that selectivity, adsorption capacity and reversibility of adsorption mainly depend upon adsorbent characteristics like particle size, porosity, specific surface area, structure strength and stability. Micropores (<20Å diameter), mesopores (20-500 Å diameter) and macropores (>500 Å diameter ) truly define the pore size of the adsorbents (DUTTA, 2007).



Figure 2.3: Schematic diagram of pore structure of adsorbent (Suresh Kumar *et al.*, 2017)

Activated carbon is a member of a family of carbons ranging from carbon blacks to nuclear graphites, from carbon fibres and composites to electrode graphites, and many more. Mostly, activated carbon production are made of peat as well as woods, fruit stones and nutshells, as with coconut shells, as well as some synthetic organic polymers. Activated carbon is treated to enhance the porosity which become preferable for adsorption or chemical reactions (Marsh and Rodríguez-Reinoso, 2006). Activated carbon can be applied in refrigerator application. Their surface area typically within the range of 800–1500 m<sup>2</sup>g<sup>-1</sup>, larger the surface area, the better the performance of adsorption. Activated carbon also has larger working pressure (approximately 16 bar) and allows better performance in heat and mass transfer to decrease the bad smell and corrosiveness (Ullah *et al.*, 2013). (Rios *et al.*, 2013) studied on experimental binary equilibrium isotherms for CO<sub>2</sub>-CH<sub>4</sub> mixtures on an activated carbon at 293K. CO<sub>2</sub> presented at highly adsorbed amounts on activated carbon with respect to CH<sup>4</sup>. A maximum selectivity of around 8.7 was observed for a nearly equimolar mixture at 0.1 MPa.

Zeolites are naturally occurring microporous crystalline silicate framework materials that have properties used in adsorption and ion exchange. Natural zeolite Crystals can be found from volcanic sediments in closed alkaline and saline lake-systems. Naturally occurring zeolites can be categorized into 40 different types. In order to fulfill the huge demand of industrial, they are also synthesized in the laboratory by using hydrothermal synthesis techniques at temperatures of around 25–150 ° C (usually 100 ° C)(Xu *et al.*, 2009). Artificial zeolites can be synthesized and distributed as 150 types which are named by one letter or a group of letters, such as type A, type X, type Y, type ZSM and so on (Nagah *et al.*, 2013). The internal modification of zeolites like pore opening, pore size and thermal stability allow researchers to focus on new innovative approaches to be introduced so that high selectivity zeolite has the capacity to separate substances based on differences in sizes and shapes of particles. Adsorption processes are normally reversible in practice. This permits the zeolite to be reused many times, swinging between adsorption and desorption steps (Dąbrowski, 2001).

Moreover, from previous works, researchers have carried out certain experiment by using different appropriate adsorbents in order to remove  $CO_2$ .Adsorption capacity, thermal stability and regeneration rate in regard with different pore structure of adsorbents will be the benchmark for that researchers to figure out (Majchrzak and Nowak, 2017). The result of comparison of the selection criteria necessary for  $CO_2$  capture can be concluded in Table 2.2.

Table 2.2 Result of comparison of the selection criteria necessary for CO<sub>2</sub> capture

	Activated Carbon	Zeolites
Sorption capacity	Lower than zeolites (at ambient condition),higher at higher pressure	Higher than activated carbons(at ambient conditions),lower at higher pressures
Thermal Stability	Stable at multiple cycles	Stable at multiple cycles
Level of regeneration	The easiest to regenerate	Harder to regenerate than activated carbon
Influence of other factors	The least influence of NO <sub>X</sub> and SO <sub>X</sub> (level of ppm)	Greater impact of other compounds: SO <sub>X</sub> and NO <sub>X</sub> than for AC
Impact of moisture	The least influence in compare to other adsorbents	High impact of moisture on sorption capacity.

(Majchrzak and Nowak, 2017)

Τ	`able	2.2	continue	d
---	-------	-----	----------	---

	Carbon molecular	Sorbents modified with
	sieves	amines
Sorption capacity	Lower than activated	Lower than physical
	carbon and zeolites(at	adsorbents at 25 °C but
	ambient condition)	higher at 70-90 °C
Thermal Stability	Stable at multiple cycles	Stable at multiple cycles
Level of regeneration	More difficult to	Easy to regenerate, but
	regenerate than activated	harder than activated
	carbon, but much easier	carbon
	than zeolites	
Influence of other	The least influence of	The largest effect of SO <sub>X</sub>
	$NO_X$ and $SO_X$ (level of	and NO <sub>X</sub> on sorption
factors	ppm)	capacity.
Impact of moisture	Slight influence on	Minimal or no impact of
	moisture	moisture on sorption
		capacity

#### 2.5 Zirconium-benzenedicarboxylate UiO66 Adsorbent

UiO66 is synthetic porous solid adsorbent that coordination via zirconium and its linker 1,4-benzene-dicarboxylate. It can be grouped as metal-organic framework(MOF) adsorbent. (Cavka *et al.*, 2008) The cluster structure of UiO66 has shown in Figure 2.4.



Figure 2.4: Cluster structure of UiO66 adsorbent with its linker 1,4-benzene-

dicarboxylate (Cavka et al., 2008)

Commonly, zeolite is the good adsorbent to be employed in capturing CO<sub>2</sub> owing to its high surface area (SA<sub>BET</sub> =726m<sup>2</sup>/g), small pore volume (0.25cm<sup>3</sup>/g) and high thermal and chemical stability. But, interestingly, recently metal-organic framework (MOFs) are an emerging new class of solid crystalline and decided to be investigated by many researchers because of its high specific surface area and adsorption capacity leading to large capacity of CO<sub>2</sub> to be adsorbed (Sumida *et al.*, 2012). From previous research, it indicate that UiO66 (SA<sub>BET</sub>=1250m<sup>2</sup>/g)(Huang *et al.*, 2017). Eventually, it exhibit that UiO66 has much better adsorption capacity than zeolite adsorbent.

Furthermore, UiO66 metal-organic framework can undergo development and alter the pore size to achieve higher adsorption capacity. Different kind of modulator the acid solvents can be added to compensate the ligand of the structure UiO66. The BET surface areas can change from  $1175 \text{ m}^2\text{g}^{-1}$  to  $1777 \text{ m}^2 \text{ g}^{-1}$  that have been reported in recent research (Shearer *et al.*, 2016).

#### 2.6 Breakthrough study

Breakthrough studies can act as guidance to evaluate the performance of bed which mean the adsorbent that installed in column. In pressure swing adsorption (PSA), it also allow the determination of duration of adsorption in order to control the purity of product. Beyond the duration of adsorption, the purity of product will decrease significantly (Warren, 2012).Breakthrough curve can be plotted by y-axis, C/Co which convey feed concentration after pass through the bed over concentration before feed in against x-axis, time. After injection of adsorbate, the process adsorption will start to occur and as the time pass three region will be established inside the bed at certain length which are saturated zone, mass transfer zone and unused zone as shown in Figure 2.5.



Figure 2.5: Solid concentration profile at different times

Once it reach the breakthrough time ( $t_b$ ) concentration of effluent can be determined. Then concentration of effluent continues to increase until it meet the saturated point at the time ( $t_s$ )(DUTTA, 2007).On the other hand, if the bed height is increased, mass transfer zone will be extended, causing the longer breakthrough and saturated time (Chowdhury *et al.*, 2013).

#### 2.7 Breakthrough Study of CO<sub>2</sub> Removal Using UiO66

In previous work, UiO66 has been applied for removal of  $CO_2$  from  $N_2$  at different pressure and the breakthrough curve is plotted. At pressure 3 bar, UiO66 achieved a breakthrough 400 second (6.67minutes) in their study. At pressure 4 bar, UiO66 achieved a breakthrough 500 second (8.3minutes) in their study. This reported that as pressure increase, the adsorption capacity of adsorbent increase (Andersen *et al.*, 2013). Rather than using UiO66,the same class adsorbent (MOF) Cu-BTC tablets has been researched by studying the breakthrough curve in separation of 83% methane and 4.5% CO<sub>2</sub> at 1.1 bar and 308K,others will be helium gas. The breakthrough time for CO<sub>2</sub> removal was 1000 second (16.67 minutes) (Asadi and Ehsani, 2013). Other than that, 30PEI-impregnated UiO-66 has been characterized and explored by researchers to find out the breakthrough of binary mixture CO<sub>2</sub>/CH<sub>4</sub> (ratio 1:9) at 308 K and compared with the UiO-66 without undergo process impregnated UiO-66 for CO<sub>2</sub> breakthrough time for UiO-66 is 40s whereas 30PEI-impregnated UiO-66 for CO<sub>2</sub> breakthrough time has been increased until 250s.(Xian *et al.*, 2015)

#### 2.8 Effect of adsorption time and blowdown time in PSA

Adsorption time and blowdown time both are important parameters to affect the performance of pressure swing adsorption, PSA. (Rao *et al.*, 2010) examine on the optimization of combination adsorption time and blowdown time to maximize oxygen purity via stimulation COMSOL software by using adsorbent 5 Å and partially Ag exchanged-Li-substituted 13X zeolite adsorbents in two steps pulse pressure swing adsorption. From their findings, they discovered that very long adsorption time 0.24s will cause impurity like nitrogen penetrate through the bed and affect product oxygen purity at fixed desorption time 1.2 second. Same point have been reported in (Jain *et al.*, 2003) about the adsorption time cannot go beyond the breakthrough time of impurity. The adsorption time that stay within the limit also have to adjust to meet the high purity and recovery of product. It was discovered that increasing total adsorption time, at the same time the purity of product will increase but recovery of product will decrease. (Kim *et al.*, 2000) studied experimentally about blowdown time ratio to the adsorption time using double layer bed of activated carbon and zeolite 5A to separate gas mixture ( $H_2/CO_2/CH_4/CO$ ). It showed that 0.2 ratio of blowdown time to adsorption time achieve highest recovery which exceeded 84% of recovery by using adsorbent ratio 60/60, 70/50 and 80/40 respectively.

# 2.9 Design Expert Response Surface Methodology (RSM) for optimization in PSA

RSM was introduced since 1951 and act as excellent platform to figure out optimum condition in experiments. It was set up by modelling techniques that involving mathematic and statistic theories which can provide robustness and flexibility in design system (Khuri and Mukhopadhyay, 2010). There were a few features inside RSM for example Central Composite, Box-Behnken,3 Level Factorial and so on. Among these features, one of commonly used feature will be Central Composite design (CCD). (Ribeiro Sant Anna *et al.*, 2015)adopted central composite design (CCD) for optimization of operational pressure to separate mixture gases (CH4/N<sub>2</sub>) in pressure swing adsorption. High pressure 6 bar, Intermediate 5.5 bar and low pressure 0.1 bar were the optimum condition to allow high N<sub>2</sub> purity 96.61% and N<sub>2</sub> recovery 89.81% to be produced. (Saberimoghaddam and Nozari, 2016) studied intensively on optimization purge/feed ratio and adsorption time for purification of hydrogen in an H<sub>2</sub>/CO<sub>2</sub> mixture. Their result concluded that at intermediate condition purge/feed ratio 0.2 and desired adsorption time 10.42 minutes can obtain maximum of purity and recovery.

#### **CHAPTER THREE**

#### MATERIALS AND METHODS

This chapter covers the overall experimental aspects of the research project including the general research flow diagram, materials utilized, adsorbent preparation and characterization, experimental rig set-up for breakthrough studies and pressure swing adsorption along with optimization software Design Expert Central Composite Design (CCD).



#### 3.1 Research Methodology

Figure 3.1: General layout of research flow diagram.

# 3.2 Materials and Chemicals Required

The list of materials and chemicals used in this research are shown in Table

3.1.

Chemical	Molecular	Purity	Supplier	Usage
	formula	(%)		
Methane	CH <sub>4</sub>	99.9	Araztech- engineering	PSA and Breakthrough studies
Carbon dioxide	CO <sub>2</sub>	99.9	Araztech- engineering	PSA and Breakthrough studies
Zirconium (IV) Chloride	ZrCl4, anhydrous powder,	99.99	Sigma-Aldrich	Preparation of adsorbent UiO66
Dimethylformamide (DMF)	HCON(CH <sub>3</sub> ) <sub>2</sub> ,	99.8	Sigma-Aldrich	Preparation of adsorbent UiO66
1,4 benzenedicarboxylic acid (BDC)	C <sub>9</sub> H <sub>6</sub>	-	Sigma-Aldrich	Preparation of adsorbent UiO66
Ethanol	CH <sub>3</sub> CH <sub>2</sub> OH,	99.8	Sigma-Aldrich	Preparation of adsorbent UiO66

Table 3.1: List of materials and chemicals.

### 3.3 Equipment Required

Different types of equipment were used for different purposes in this research such as preparation of adsorbents, breakthrough study and PSA studies. The list of equipment used in the study are shown in Table 3.2.

Equipment	Model	Application
X-Ray Diffractometer (XRD)	Bruker XRD D8 Advance	<ul> <li>To study the crystallinity and atomic spacing of sample.</li> <li>To analyse the crystalline phases and orientation.</li> </ul>
Surface Area and Porosity Analyser (SAPA)	ASAP 2020	A surface area analysis conducted to determine the surface area (BET) of the adsorbents
Scanning Electron Microscope (SEM)	Quanta FEG450	<ul> <li>To determine a better view and clear understanding on the structural surface and pore arrangement of the adsorbent samples. Different magnification power was used to show the most suitable image.</li> </ul>
Energy Dispersive X-Ray Spectroscopy	Quanta FEG450	To identify chemical composition of the adsorbent sample.
Particle Size Analyser	CILAS 1180	To study the size of particle based on diffraction pattern obtained.
Gas Chromatograph (GC)	Agilent Technologies 7890A	To determine the composition of binary gas mixture and adsorption capacity.

Equipment	Model	Application
Furnace	GSL-1100X,MTI Corp.	To provide thermal treatment to increase pore area of adsorbent.
Oven	Heraeus	<ul> <li>For drying purpose.</li> <li>To regenerate the adsorbent by removing moisture and impurities.</li> </ul>
Flow meter analyser	AALBORG	<ul> <li>Binary mixture flow rate checking</li> </ul>

#### **3.4** Adsorbent Preparation

#### 3.4.1 Zirconium-benzenedicarboxylate (UiO-66)

Firstly, 1.06 g of zirconium (IV) chloride (ZrCL4) was dissolved with 30 ml of dimethylformamide (DMF) and follows with 30 minutes of stirring. After that, 0.78 g of 1,4 benzenedicarboxylix acid (BDC) was dissolved into 30 ml of DMF at 25 °C in a volumetric flask. Both dissolved solutions were mixed and stirred together with 2 ml of deionized water and placed in an oil bath. The mixture was then go through thermal treatment process in furnace at 120 °C about 30 minutes. After the process, the solution was then cooled down to room temperature for 2 hours. Finally, precipitate was obtained as expected. Absolute ethanol was then used to washed the resulting precipitate repeatedly for 3 times. The washed precipitate was then dried at 70 °C for overnight.