SCHOOL OF MATERIALS AND MINERAL RESOURCES ENGINEERING UNIVERSITY SAINS MALAYSIA

IMPACT OF POUR POINT DEPRESSANT ENHANCED WITH GRAPHENE OXIDE ON THERMAL AND MICROSTRUCTURE PROPERTIES OF SIMULATED CRUDE OIL MODEL

By

MUHAMMAD DANIAL BIN MOHD JOHARY

Supervisor: Prof. Dr. Azlan bin Ariffin

Dissertation submitted in partial fulfillment

of the requirement for the degree of Bachelor of Engineering with Honours

(Polymer Engineering)

University Sains Malaysia

MAY 2018

DECLARATION

I hereby declare that I have conducted, completed the research work and written the dissertation " **Impact of pour point depressant enhanced with graphene oxide on thermal and microstructure properties of simulated crude oil model**". I also declared that it has not been previously for the award for any degree or diploma or other similar title of this for any other examining body or university.

Name of Student	:Muhammad Danial bin Mohd Johary	Signature:
Date	:24 May 2018	
Witness by		
Supervisor	:Professor Dr. Azlan Ariffin	Signature:

Date :24 May 2018

ACKNOWLEDGEMENTS

First, I would like to show my highest gratefulness to ALLAH S.W.T for giving me a chance to be able completed my Final Year Project. I also like to offer my deepest to my supervisor, Prof Azlan Ariffin for the valuable guidance and advices while assisting me in completing my Final Year Project and I would like to express my special thanks t Dean of School of Materials and Minerals Resources Engineering USM for giving me full cooperation and endless patience during me study. I had gained lots of knowledge, which is ultimate useful for my future undertaking.

Apart from that, I would like to dedicated my thanks to Mr. Ridhwan Hafiz Rosdi that have provide me knowledge skills needed for the project research. Not to miss the technician's staffs of PPKBSM for sharing the information during conducted the testing. I am very grateful to have a comfortable and warming working place during my Final Year Project. It is a wonderful experience to have cooperated with all colleagues to USM for giving me the opportunity to do this project.

Last but not least, thanks to my mother Rohiza binti Jamaluddin, and my Father Mohd Johary bin Kamaruddin because of their support and encouragement towards me. Without the help and effort that have been contribute by everyone, this project will not be successfully completed. I thankful and appreciated for all of their kindness.

Contents	Page
DECLARATION	ii
ACKNOWLEDGEMENTS	iii
TABLE OF CONTENTS	iv
LIST OF TABLES	vii
LIST OF FIGURES	viii
LIST OF SYMBOLS	xi
LIST OF ABBREVIATIONS	xii
ABSTRAK	xiii
ABSTRACT	XV
Chapter 1	1
1.1 Research Background	1
1.2 Problem Statement	5
1.3 Objectives	7
1.4 Thesis outline	8
Chapter 2	10
LITERATURE REVIEW	10
2.1 Crude oil	10
2.1.1 Overview	10
2.1.2 Type of wax	13

2.1.3	Wax deposition treatment	14
2.2 Po	lymer as Pour Point Depressant (PPD)	18
2.2.1	Overview Background of Pour Point Depressant (PPD)	18
2.2.2	Mechanism of Pour Point Depressant (PPD)	21
2.3 Gi	aphene oxide as Nano-material	24
2.3.1	Introduction to Graphene oxide	24
2.3.2	Advance and Application of Graphene oxide	25
2.3.3	Mechanism of Formation	26
2.4 Na	no-hybrid pour point depressant	27
2.4.1	Overview	27
2.4.2	Impact on of microstructure of paraffin wax	29
2.4.3	Impact on thermal properties of wax (Wax Appearance Temperature)	30
2.4.4	Mechanism of nano PPD	32
CHAPTE	R 3	33
MATERIA	ALS AND METHODOLOGY	33
3.1 M	aterials	33
3.2 Re	search Methodology Overview	33
3.3 Ex	perimental Method	34
3.3.1	Preparation of Graphene Oxide	34
3.3.2	Physical Blending Process	38
3.3.3	Sample Characterization	40
3.3.4	Emulsion Evaluation	43
3.3.5	Applied test	44

СНАРТЕ	R 4	
RESULTS	S AND DISCUSSIONS	49
4.1 C	haracterization of Graphene Oxide	49
4.1.1	Functionality of Graphene oxide (GO)	49
4.1.2	Microstructure of Graphene Oxide (GO)	51
4.1.3	Lateral size of Graphene oxide (GO)	54
4.2 C	haracterization of PPD-GO Emulsion	56
4.2.1	Fourier transform infrared spectroscopy (FTIR)	56
4.2.2	Thermal Properties of Nano PPD emulsion	
4.2.3	Particle size distribution	59
4.2.4	Zeta Potential	70
4.3 A	pplied Test	76
4.3.1	ASTM D-97	76
4.3.2	Polarized Optical Microscopy (POM)	78
4.3.3	Wax Appearance Temperature (WAT) of PPD system	
4.3.4	Scanning electron microscopy (SEM)	
СНАРТЕ	R 5	
5.1 Con	clusion	
5.2 Reco	ommendation	91
REFERE	NCES	92

LIST OF TABLES

Table 2. 1 Hydrocarbon found in the crude oil (Speight, 2006)	_ 11
Table 2. 2 The comparison between micro and Nano composite filler	_ 29
Table 3. 1 Sonication time of Graphene Oxide	_ 35
Table 3. 2 Formulation for Nano-hybrid PPD	_ 39
Table 4. 1 Absorption of the Graphene oxide powder	_ 51
Table 4. 2 Average sizes of Graphene oxide with different sonication times.	_ 56
Table 4. 3 Absorption of the solution Emulsion Jaypol Normal (EJN), Emulsified	
Jaypol Graphene Oxide (EJGO 1-5)	_ 58
Table 4. 4 Data analysis of DSC curve for Heating cycle curve	_ 59
Table 4. 5 Particle size distribution of fresh Emulsified Nano-hybrid PPD at differen	nt
lateral size of GO	_ 60
Table 4. 6 The particle size and span of distribution of emulsified sample at isothern	nal
temperature with different week	_ 65
Table 4. 7 The particle size and span of distribution of emulsified sample at freeze t	haw
temperature with different week	_ 70
Table 4. 8 Zeta Potential of different fresh sample at different lateral size of GO	
in PPD	_ 71
Table 4. 9 Zeta potential of different lateral size of GO at isothermal	_ 73
Table 4. 10 Zeta potential of different lateral size of GO at freeze thaw	_ 75
Table 4. 11 Pour Point reduction for different PPD system at 1000ppm	_ 77
Table 4. 12 Data analysis of DSC	_ 84

LIST OF FIGURES

Figure 2. 1 Wax deposition on wall (left) and gelation (right) of waxy crudes in	
pipeline (Yang et al., 2015)	11
Figure 2. 2 Main paraffinic wax structures	14
Figure 2. 3 Cross section for typical single tube welded system (PENTAIR Raychem	
Tracer, 2010)	16
Figure 2. 4 Wax molecule formation without present of PPD (Souchik, 2009)	22
Figure 2. 5 Wax molecule formation with present of PPD (Souchik, 2009)	22
Figure 2. 6 Image of POM treated crude oil and non-treated crude oil	24
Figure 2. 7 Chemical structure of graphene oxide with moieties group	25
Figure 2. 8 The two graphene sub-lattice (blue and red) and unit cell (Avouris and	
Dimitrakopoulos, 2012)	26
Figure 2. 9 Mechanism of formation graphene oxide (Al-Sabagh et al., 2016)	27
Figure 2. 10 Schematic structure of nanocomposite formed by combining polymer	
and layered inorganic material (Wang, Kalali and Wang, 2016)	28
Figure 2. 11 Polarizing optical microscopy images of untreated and treated BWCO at	
-1°C	30
Figure 2. 12 DSC curve to determine the WAT	31
Figure 3. 1 Flow Chart of overall research project	34
Figure 3. 2 A drop of Graphene oxide on the silicon wafer	37
Figure 3. 3 Dried Graphene oxide after dry in the oven for 30 minutes	37
Figure 3. 4 Parameter Graph of temperature range used in Differential Scanning	
Calorimetry (DSC) for emulsion PPD-GO	41
Figure 3. 5 Malvern folded capillary cells	42
Figure 3. 6 Flow chart for aging test and freeze thaw test.	43

rigure 5. / rurameter Graph of temperature range used in Differential Seaming	
Calorimetry (DSC) for applied simulated paraffin wax	_ 46
Figure 3. 8 The sample preparation of POM for applied sample	_ 47
Figure 4. 1 FTIR Spectra for different sonication time of Graphene oxide	_50
Figure 4. 2 SEM image of GO 1	_ 52
Figure 4. 3 SEM image of GO 2	_ 52
Figure 4. 4 : SEM image of GO 3	_ 52
Figure 4. 5 SEM image of GO 4	_ 53
Figure 4. 6 SEM image of GO 5	_ 53
Figure 4. 7 Average lateral size of GOs as function of sonication time	_ 54
Figure 4. 8 Energy input of sonication vs sonication time	_ 55
Figure 4. 9 FTIR Spectra for PMMA emulsion with different lateral size of GO	
samples	_ 57
Figure 4. 10 Heating cycle of DSC thermogram for PPD Nano emulsion	_ 59
Figure 4. 11 Particle size distribution of fresh sample at different lateral size of GO_	_ 60
Figure 4. 12 Particle size distribution of EJN sample at Isothermal temperature	_ 62
Figure 4. 13 Particle size distribution of EJGO1 sample at Isothermal temperature	_ 63
Figure 4. 14 Particle size distribution of EJGO1 sample at Isothermal temperature	_ 63
Figure 4. 15 Particle size distribution of EJGO3 sample at Isothermal temperature	_ 64
Figure 4. 16 Particle size distribution of EJGO4 sample at Isothermal temperature	_ 64
Figure 4. 17 Particle size distribution of EJGO5 sample at Isothermal temperature	_ 65
Figure 4. 18 Particle size distribution of EJN sample at freeze thaw	_ 67
Figure 4. 19 Particle size distribution of EJGO1 sample at freeze thaw	_ 67
Figure 4. 20 Particle size distribution of EJGO2 sample at freeze thaw	_ 68
Figure 4. 21Particle size distribution of EJGO3 sample at freeze thaw.	_ 68

Figure 3. 7 Parameter Graph of temperature range used in Differential Scanning

Figure 4. 22 Particle size distribution of EJGO4 sample at freeze thaw 69
Figure 4. 23 Particle size distribution of EJGO5 sample at freeze thaw 69
Figure 4. 24 Zeta Potential of fresh sample (EJN, EJGO (1-5)) 71
Figure 4. 25 Zeta Potential of EJN, EJGO (1-5) of at Isothermal temperature 73
Figure 4. 26 Zeta potential of EJN and EJGO (1-5) under freeze thaw 75
Figure 4. 27 Pour Point reduction for different PPD system at 1000ppm 76
Figure 4. 28 Pour point reduction of Paraffin wax treated with different lateral size of
GO 77
Figure 4. 29 Polarizing optical microscopy (POM) images of crystal morphologies of
PW and doped with EJN and EJGO 5 78
Figure 4. 30 Polarizing optical microscopy images of crystal morphologies of PW with
(GO1, GO2, GO3, GO4, GO5) PPDs at different temperatures 79
Figure 4. 31 Polarizing optical microscopy images of crystal morphologies of PW and
doped with EJN and EJGO 5 81
Figure 4. 32 Polarizing optical microscopy images of crystal morphologies of PW with
(GO1, GO2, GO3, GO4, GO5) PPDs at different temperatures 82
Figure 4. 33 Heat flow curve of EJN and GO (1-5) 84
Figure 4. 34 SEM image of extracted wax crystal (a) Paraffin wax, (b) EJN,
(c) EJGO 5 87

LIST OF SYMBOLS

°C	Degree Celcius
g	Gram
μm	Micrometer
%	Percentage
mV	Millivolt
r _c	Radius of critical nucleus
ΔH	Enthalpy change
T_g	Glass Transition Temperature
T_m	Melting Temperature

LIST OF ABBREVIATIONS

PPD	Pour Point Depressants	
WAT	Wax Appearance Temperature	
EJN	Emulsified Jaypol Normal	
EJGO	Emulsified Jaypol Graphene Oxide	
EJGO1	Emulsified Jaypol Graphene Oxide 1	
EJGO2	Emulsified Jaypol Graphene Oxide 2	
EJGO3	Emulsified Jaypol Graphene Oxide 3	
EJGO4	Emulsified Jaypol Graphene Oxide 4	
EJGO5	Emulsified Jaypol Graphene Oxide 5	
GO	Graphene Oxide	
DSC	Differential Scanning Calorimetry	
POM	Polarized Optical Microscope	
FTIR	Fourier Transform Infrared Spectroscopy	
SEM	Scanning Electron Microscopy	
JAYPOL 658G	Acrylate Polymer	
DEA	Diethylamine	
MWV	Meadwestvaco	
MSZW	Meta-stable zone width	

KESAN AGEN TEKAN TITIK TUANG (PPD) DENGAN GALAKKAN GRAPHENE OKSIDA TERHADAP CIRI-CIRI HABA DAN MIKROSTRUKTUR KEPADA MODEL SIMULASI MINYAK MENTAH

ABSTRAK

Perbezaan saiz sisi Graphene Oksida (GO) yang direndahkan mengunakan alat sonik telah dikaji keterbandingan dengan penambahan agen tekan titik tuang (PPD) akan menambah baik kemampuan mengalir bagi model simulasi minyak mentah, GO terbahagi kepada 5 kategori, dimana berbezanya masa sonik. GO1, GO2, GO3, GO4, dan GO5 di sonikkan dengan masa yang berbeza masing-masing 0 min,10 min,30 min,60 min and 100 min. GO1 adalah sebagai sampel rujukan, sebagai penanda aras terhadap hasil kajian. Penyediaan emulsi PPD bermula dengan menyediakan larutan berasaskan air termasuk GO dan larutan berasaskan minyak, bersama kedua-dua larutan dikacau di dalam mandian air. Tambahan pula, sifat morfologi tersonik dikaji mengunakan scanning electron microscopy (SEM), dan Fourier-transform infrared (FTIR). Daripada imej SEM memaparkan pengurangan saiz sisi GO seiring dengan peningkatan masa sonik. GO yang telah disonik dikenalpasti dengan mengunakan FTIR, keputusan hasil kajian menunjukkan corak puncak adalah sama dengan sampel rujukan. Ujian kestabilan telah dijalankan salama 4 minggu, saiz zarah sampel meningkat dengan aktiviti beku cair, tetapi tidak menjejaskan kestabilan emulsi. Keupayaan zeta adalah dalam lingkungan (-50mV - -60 mV) ini menunjukkan emulsi berada dalam lingkungan yang stabil. Imej pembentukkan kristal telah dikaji. mekanisme heterogen nukleasi, keseragaman, dan bentuk batang kristal telah dilihat mengunakan Polarizing Optical Microscopy (POM),imej menunjukkan dengan kehadiran GO akan melambatkan pembentukkan lilin kristal dan kecenderungan membentuk kelihatan batang daripada bentuk mengelupas pada suhu rendah. Lebih kecil saiz GO akan mempamerkan menyebaran yang baik di dalam simulasi minyak mentah. Untuk kajian yang lebih mendalam terhadap pembentukkan kristal, perubahan dinamik rangkaian struktur kristal telah dikaji. Kajian terma telah dijalankan mengunakan Differential Scanning Calorimetry (DSC), ianya menunjukkan corak menaik terhadap suhu kemunculan lilin (WAT) apabila hadirnya saiz sisi GO yang kecil walau bagaimanapun ianya lebih tinggi daripada sampel kosong (lilin asli) Permukaan simulasi minyak mentah telah dikaji mengunakan Scanning Electron Microscopy (SEM).Permukaan sampel kosong menunjukkan corak berombak ,ini kerana terhasilnya rangkaian struktur 3 dimensi, Bagi Emulsified Jaypol Graphene Oxide 5 (EJGO5) menunjukkan permukaan seperti kulit manusia ,dimana GO bertindak sebagai tapak nukleasi yang teredar dengan baik. Prestasi titik tuang bagi Nano-hibrid PPD telah ditambah baik jika dibandingkan dengan emulsi biasa PPD (EJN). Peningkatan corak prestasi dengan pengurangan saiz sisi GO menunjukkan saiz sisi GO adalah faktor yang mempengaruhi peningkatan prestasi titik tuang dan keupayaan mengalir bagi emulsi PPD.

IMPACT OF POUR POINT DEPRESSANT ENHANCE WITH GRAPHENE OXIDE ON THERMAL AND MICROSTRUCTURE PROPERTIES OF SIMULATED CRUDE OIL MODEL

ABSTRACT

Different lateral size of Graphene oxide (GO) reduce by sonication were comparatively investigated as additive for PPD to improve the flow ability of crude oil simulated crude oil model. The GO was divided into 5 categories ,which is different in sonication time. The GO1, GO2, GO3, GO4, GO5 were sonicated at different time which is 0 min,10 min,30 min,60 min and 100 min respectively. The GO1 will be the control sample, as a bench mark of the result. The preparation of the emulsified PPD begin with the preparation of water-based solution which include the GO and oil-based solution together both of the solution stirrer in the water bath. Furthermore, the morphology properties of sonicated GO were investigated using scanning electron microscopy (SEM) and, Fourier-transform infrared (FTIR) .From SEM image it seems as reduction lateral size of GO as increase the sonication time. Sonicated GO surface properties was confirmed by the FTIR results that show the same peak pattern from control sample. The stability test are conducted about 4 weeks the particle size of the sample increased by freeze thawed activities, but does not affect the stability of the emulsion. The zeta potential is about (-50mV - -60 mV) showing that the emulsion is in the stable range. The image of the crystal formation was studied. The heterogeneous nucleation mechanism, uniform and rod-like shape crystals were observed by polarizing optical microscopy ,the POM image showing that , when present of GO it will delay the formation of wax crystal and tendency to form rod like instead of flake like at low temperature, the smaller size of GO will exhibit good dispersion in the simulated crude oil. For further study on crystal formation, the dynamic changes of crystal structure network were taken apart in this

study. The thermal study was conducted using Differential Scanning Calorimetry (DSC), that shows the improving the Wax Appearance Temperature (WAT) when adding the smaller lateral size of GO but higher from the blank sample (pure paraffin wax). The surface of the simulated crude oil was study using Scanning Electron Microscopy (SEM) , The surface of the blank sample show wavy pattern , this due to the formation of the 3D structure network, for Emulsified Jaypol Graphene Oxide 5 (EJGO5) show the surface like a human skin , which is GO act as well distributed nucleation site . The pour point performance of Nano-hybrid PPD was improved compared with Emulsified Normal PPD (EJN) The increasing trends of performance by reducing lateral size of GO showing that the GO lateral size is the most influenced factor that increased pour point and flow ability performance of Emulsified PPD.

Chapter 1

INTRODUCTION

1.1 Research Background

The Pour Point Depressant (PPD) is the best other alternative way have been given to the wax solidification in the oil and gas production industry stated by (Manka and Ziegler, 2001). The precipitation of wax crystal from crude oil can cause significant issues during production, transportation and storage. The solidification of paraffin wax will form solid deposits, which reduce the cross-section of flow lines (Hassan Ali, 2012). The content of the crude oil is the other reason ,precipitation of wax , the crude oil often contains substantial amounts of paraffin wax ,which constitutes the saturated aliphatic fluid fraction .When the crude oil temperature falls beneath the wax appearance temperature (WAT) also known as cloud point ,the paraffin wax precipitate in an orthorhombic unit cell as needle or plate-like crystal (Jafari Ansaroudi *et al.*, 2013). Untreated crude oil can imparting high pour point ,high viscosity ,high yield stress ,and non-Newtonian flow behaviour to waxy crude oil .

The precipitation of paraffin waxes brings immense difficulties to the production and pipeline transportation on waxy crude oil .The paraffin wax begin to precipitate from the oil due to super-saturation ,when the temperature of waxy crude oil is below its wax appearance temperature (WAT) (Pedersen and Rønningsen, 2003). Nowadays, several methods have been develop to minimise the problems caused by wax crystal deposition and aggregation. The prevention technique is mechanical remediation (pigging), applying heat or using hot solvent flush and the chemical inhibitor treatment such as poly(acrylate) base as pour point depressants (PPD),thermodynamic (TWI) and crystal modifiers (Yang *et al.*, 2015). Nevertheless, the chemical prevention of the wax to precipitate is more convenient. Chemical treatment is chosen to inhibit of the wax deposited since chemical treatment is more economical and more efficient compared to other methods.

Generally, pour point depressant selected in treatment the wax deposited via chemical inhibitor treatment . (Manka and Ziegler, 2001) found that , pour point depressant (PPD) are polymeric material with long hydrocarbon chains that interact with the paraffin in the crude oil and inhibit the formation of large wax crystal matrices . The co-crystallization occur between wax molecule and PPD will retards the wax crystal formation and growth, alters the paraffin's heat of crystallization and depressant the crude's pour point while affecting the size and shape of the crystal. The addition of GO will form a nucleation site and prevent it to form a large 3-dimensional structure crystal network that make improve in flow ability. The observation can clearly seen in Polarizing optical microscopy (POM) to look deep into the kinetic growth of wax crystal at certain temperature .According to (Yang *et al.*, 2015), most polymeric additives is categorized as crystalline-amorphous copolymer, ethylene-vinyl acetate copolymers and comb polymers. Hence, pour point depressant consist of polymers, which has comb structure that avoid the wax crystal growth on pipeline wall .

Acrylate polymer such as ethylene vinyl acetate (EVA) and poly methacrylate (PMA) become preferred choice in treating wax deposition. It is because EVA is a block olefin copolymer with rubber like properties and has excellent viscosity properties

(Totten, 2003). Meanwhile, PMA is known as comb polymer family due to their comblike structure. Comb polymer has excellent ability to act as pour point depressant since it can withstand low temperature condition, which is below 0° C (Totten, 2003).

Most of the conventional polymeric PPDs are in solution form. This limits the PPD application in at cold climates for example during winter season. This is because PPD solutions are easily solidified at low temperature. The solidification problem of PPD will ruin the treatment itself as it cannot be injected into the pipeline in solid form, other things is about mobility or the movement of the solid ,it is quite heavy to homogenous spread in the pipeline compared to solution which the PPD in emulsion system ,it is more convenient to get efficient spread of the PPD in the turbulent flow in the transportation pipeline (Becker, 1999). The costing for preheating and dilution is a prerequisite to be considered for its utilization in a crude oil industry. So, it is impractical to use the PPD solution in the cold environments.

Emulsion technology has been viewed to solve the PPD solidification at room temperature. According to (Admiral, Abdullah and Ariffin, 2016), they successfully established the emulsion PPD which could flow at room temperature. At the same time, the behaviour of emulsion such as freezing point, viscosity at room temperature, particle size and zeta potential still improved. Nevertheless, there is some issue on PPD performance during emulsion even it possesses a good thermal stability emulsion. Introduction of nano-size filler into a polymer become a well-known method to enhance the existing polymer properties (Boccaccini et.al, 2010). This polymer classification is known as polymer nanocomposites. This polymer nanocomposites concept can be employed to boost the PPD emulsion in treating the paraffin wax. In recent year, graphene and graphene oxide become the current attention in research world. It gives positive impact toward the polymer nano composites properties. Graphene is the strongest material because of π - π stacking in chemical structure. The π - π bond is described as the non-covalent interactions, which involves in the stacking of aromatic molecules. Aromatic network of sp² carbon atoms makes this interaction important in graphene functionalisation.

Graphene and graphene oxide were applied in biomedical field. Graphene was used as a substrate for addition or adsorption of molecules and the functional groups in a controlled manner (Mao et.al, 2013). Covalent and non-covalent surface modifications have been performed to improve biocompatibility and colloidal stability.

In this work, graphene oxide was used to study the behaviour of nanocomposite in the PPD emulsion and improve the PPD performance. In addition, the research work on sonication graphene oxide for different lateral size of GO-PPD on wax crystal still limited. So, it is importance to gain a new generation of nano hybrid pour point depressant used in oil and gas technology application. The work study more on the wax apparent temperature (WAT),which the temperature start to form , and morphology of the crystal formation arrangement of wax using SEM .The kinetic behaviour of wax crystal formation also studied using polarized optical microscopy (POM) .

1.2 Problem Statement

Huge numbers of the world's oil endure when paraffin wax precipitates out and solidifies in formation pores and fluid flow channels, at the wellbore ,on the side walls of wells ,in the tubing ,casings ,perforations, pump strings ,rods, and the complete oil transfer system of flow lines and pipelines (Mahmoudkhani *et al.*, 2017) .Paraffin wax deposition is expensive, causing diminished of the production ,equipment failure ,bottlenecks ,loss of storage ,clogging of refinery pipework ,and loss of efficiency .It is one of the oil industry's most expensive problematic nuisances. Paraffin wax is the initial glue that causes asphaltenes ,corrosion and debris to stick ,collect and build up ,due to paraffin wax deposition ,currently there are thousands of well shut-in with no production ,numerous pipelines blocked ,transport vessels taken out of service ,tanks locked-in and refinery equipment shut down , also the expanded plausibility of failures and catastrophic event caused by build-up The alteration of crude oil is very significant to avoid or delay the deposition of paraffin wax. The PPD was applied to overcome the problem above by chemical treatment ,which is more convenient for low cost of operation.

The conventional PPD faces the solidification issue, due to the solidification at room temperature. In addition, it is difficult to deliver the high active content of polymer at low viscosity value. According to (Becker, 1999), some PPD is less efficient especially for pour point reduction. If PPD dissolve, it is quite hard to achieve high active content, hence higher dosage of PPD must be used. The imprecation is that high dosage contributes to high treatment cost. The conventional PPD consist of active content in the high range of 5-10 wt.%.

Admiral, Abdullah et al. 2016 suggested that the emulsion method can be used on PPD to solve the solidification issue. However, it still has limitations on PPD performance. It is ideal to get a PPD which can be utilized at any range of temperature. The advantage for proposing nano hybrid pour point depressant where the active content in range of 30-50 wt. % can be achieved and high molecular weight and environment friendly (reduce solvent usage) PPD can be produced. However, PPD emulsion still lacks in term of application performance even possess a good flow-ability at low temperature. Since the performance of PPD is merely dependable on the existing of polymer properties.

The performance issue can be solved by incorporating of nano size graphene oxide with emulsified PPD. It is interesting alternative when smaller lateral size of graphene oxide can boost the PPD performance subjected to inhibit the wax crystal in paraffin wax. Addition of graphene oxide in the PPD emulsion is very promising route to solve the above problem as it can produce an immense improvement in polymer properties. Graphene oxide consist of π - π interaction which is non-covalent interaction involve in the stacking of aromatic ring molecules. This interaction prevent graphene oxide aggregation through steric or electrostatic repulsion. Therefore, in this study, it is hypothesized that the lateral size of Graphene oxide (GO) will improve the PPD performance through steric or electrostatic repulsion. This repulsion force will prevent the crystal growth formation on the pipeline wall

The suitable method to achieve the smaller lateral nano-size of Graphene oxide is by sonication. The sonication promote the energy to break of the sheet of graphene oxide ,which creates shear stresses and cavitation in the solvent. This has the effect of breaking apart graphene oxide and exfoliating the sheets into individual graphene oxide flakes .Shi et.al (2007) proved that, the nanocomposites have an intercalated and flocculated structure.

The integration of graphene oxide in the PPD emulsion give a new alternative for the manufacturer petroleum industry to improve their performance of current PPD product. Moreover, graphene oxide more economical that it can reduced the costing.

1.3 Objectives

- 1. To study the impact of lateral size of nano graphene oxide to inhibit the wax crystal.
- 2. To study the kinetic crystal formation of paraffin wax after applied the nano hybrid PPD
- 3. To study the wax apparent temperature (WAT) of paraffin wax with addition different lateral size of graphene oxide as nano-hybrid PPD

1.4 Thesis outline

In this thesis, there are five chapters discusses on poly (acrylate) base of Nano graphene oxide as Nano-hybrid pour point depressants. A brief description on each chapter are elaborated as follows:

- **Chapter 1** briefly introduced the research project. This chapter cover the introduction about the research background, problem statement, objectives and outline of the thesis
- Chapter 2 is the literature review part. In this chapter, it covers brief introduction on graphene oxide. This chapter also covers the overview of background pour point depressants, development of pour point depressants, mechanism of pour point depressants, and general intro of PPD-emulsion. Application of Nano-hybrid polymeric material in advancement of polymer nanocomposites and graphene oxide in polymeric pour point depressant and emulsion product discussed. Moreover, several physical blending methods has been reviewed in this chapter such as in situ intercalative polymerization, solution intercalation and melt intercalation method. The best method has been chosen to be applied in physical blending of graphene oxide in emulsified PPDs.
- **Chapter 3** covers the methodology used in this works including materials, experimental method that is physical blending process, sample characterization, applied test and evaluation of emulsion
- Chapter 4 consist of result and discussion of the research project
 - **4.1** focuses on the results characterization of different system (GO1/GO2/GO3, GO4/GO5). The testing conducted including Fourier

Transform Infrared Spectroscopy (FTIR), Scanning Electron Microscopy (SEM)

- 4.2 focuses on the results characterization of Graphene Oxide loading. The testing was conducted such as Differential Scanning Calorimetry (DSC), Fourier Transform Infrared Spectroscopy (FTIR), Particle Size and Zeta Potential.
- 4.3 focuses on application of Nano-hybrid pour point depressants. In the application of Nano-hybrid PPDs section, Pour Point Measurement Based on ASTM D97, Differential Scanning Calorimetry (DSC), Fourier Transform Infrared Spectroscopy (FTIR), effect of Different lateral size of Graphene oxide and Impact microstructure of paraffin wax using Polarized Optical Microscopy (POM) are discussed.
- **Chapter 5** concludes the findings from the research project with few recommendations for future work.

Chapter 2 LITERATURE REVIEW

2.1 Crude oil

2.1.1 Overview

The crude oil industry are suffering during the transportation and storage of the crude oil ,because of the solidification occur on the crude oil give trouble in the pipeline .A number of variables contribute to the possibility that a well or flowline will experience flow assurance problems in its lifetime. Particularly critical in deep-water field development, flow assurance has been addressed using a conservative approach in the past. Millions of dollars have been invested in preventive and mitigation techniques ranging from chemical inhibitors to electrically heated seabed flowlines. Most of these techniques have met with success, and they have become part of the conventional wisdom.

To prevent the occurring of solidification of crude oil shown in Figure 2.1, the study of the crude oil content itself need to focus more on that .Which is the new technologies of improving the PPD using nano GO can play the main role in this study to inhibit the formation of the wax precipitation in the crude oil.

The main component of natural gas is methane but other hydrocarbons, such as ethane, propane, butane and also present of sulphur, oxygen, and nitrogen contents in crude oils. Crude oils contain different hydrocarbon and heteroatom containing molecules and the comprehensive review of the composition and the chemistry of crude oils was published (Speight, 2006). Table 1.2 shows that the hydrocarbon found in crude oil





Figure 2. 1 Wax deposition on wall (left) and gelation (right) of waxy crudes in pipeline (Yang et al., 2015)

Hydrocarbon	Chemical	Name
	Straight chain	n-Paraffin
Contractor 1	Branched chain	iso-Paraffin
Saturated	Alicyclic	Naphthanes
	1-Ring	Benzenes
Aromatic	2-Ring	Naphthalene
	3-Ring	Phenanthrenes

Table 2. 1 Hydrocarbon found in the crude oil (Speight, 2006)

Petroleum or the equivalent term " crude oil " is a mixture of gaseous, liquid, and solid molecules that occur in rock deposits found in different parts of the world. The oil recovery from porous sedimentary rocks depends on the efficiency with which oil is displaced by some other fluids (Morrow, 1991). The flow behaviour of crude oil, gas, and brine in the porous rock medium of petroleum reservoirs is controlled largely by the interactions occurring at the interfaces within the various fluid (Group, 2007). The composition and properties of crude oils, such as viscosity, vary with the age of the oil field. As an increase in viscosity of crude oils, their density increases. The density of crude oils, expressed in terms of API gravity, relates to specific gravity.

(Kok *et al.*, 1996) state that in their study the API density is varied depend on the weather of country, the paraffin contents of the crude oils were determined by DSC, analysis as previously described . The pour points were determined by the ASTM procedure (ASTM D97-87). According to some estimates from the International Energy Agency (IEA), heavy oil represents at least half of the recoverable oil resources of the world. Heavy oil is defined as petroleum which has a density equal or lower than 20 API, but if petroleum has 10 API or less it is considered as extra heavy oil or bitumen, which is denser than water. The difference between bitumen and extra heavy oil is ambiguous and usually refers to the production technology, so we will include both under the term extra-heavy oil. As a framework, conventional oil such as Brent or West Texas Intermediate has a density ranging between 38 and 40 API.(Martínez-Palou *et al.*, 2011)

In fact ,the demand for heavy and extra-heavy crude oil has been marginal ,this is because of their high viscosity and composition complexity that make them more difficult and expensive to produce ,transport and refine .Referring to Table 2.1 above shows that Orinoco Belt in Venezuela and Libya are good example of region producing extra heavy oil.(Martínez-Palou *et al.*, 2011) state that to replace the declining production of conventional middle and light oil it takes over next two decades .

2.1.2 Type of wax

Paraffin waxes consist of straight chain saturated hydrocarbons with carbons atoms ranging fromC₁₈ to C₃₆. Paraffin wax consists mostly with normal paraffin content (80–90%), while, the rest consists of branched paraffin (iso-paraffins) and cycloparaffin. The petroleum waxes are generally categorized into two groups, paraffin wax and microcrystalline wax, present in petroleum distillates and residues. Paraffin waxes consist of straight chain saturated hydro- carbons with carbon atoms ranging fromC₁₈ to C₃₆.(Rehan *et al.*, 2016).

Microcrystalline waxes are composed of branched and cyclic hydrocarbons with carbon atoms ranging from C30 to C60 (Speight, 1991). The reasons for high molecular weight or larger carbon number waxes in oils are still under exploration. One possible explanation is that the larger carbon number waxes are composed of shorter carbon number molecules produced at lower temperature reactions. For instance, C_{50} wax consists of two C_{25} and C_{70} consist of two C_{355} . According to (Pu,H., *et al.*, 2014) fossilized organic matter shows waxes of C_{25} to C_{45} are produced from land plant sand bacteria. This is one of the reasons that why non-marine oils contain more waxes than marine oils. Figure 2.2 shows main paraffin structures. Normal paraffin is a saturated hydrocarbon with molecules containing carbon atoms linked in a straight (unbranched) chain.

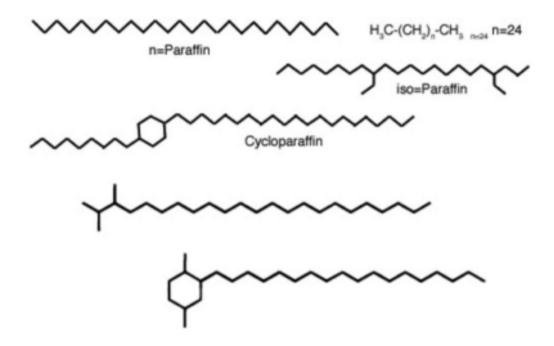


Figure 2. 2 Main paraffinic wax structures

2.1.3 Wax deposition treatment

Many of the researcher straggling to improve the treatment become more sustainable and low-cost of the maintenance .If the crude oil are not treated well ,the catastrophic failure will occur to the transportation pipeline towards the end ,and it will disturbing the production continuity. Nowadays, two type of treatment are being applied to the crude oil industry, which is more practical to apply.

2.1.3.1 Physical treatment

In the scope of the physical treatment of wax deposition ,divided into thermal, magnetic, and pigging . But they provide only temporary relief and often cause problem of their own. Most importantly, they stop the production ,sometimes for several days at a time dependent on the severity of the precipitation and deposition.

2.1.3.1.1 Pigging

Pigging is widely used in pipelines for wax removal. However, pigging operation relies heavily on "rules of thumb." Because of its complexity, rather-limited pigging models were presented to predict the wax-removal mechanics in past decades. This work aims to develop a pigging model for wax removal in pipelines. In field operation, the mechanical pig is widely used for removing the wax build-up from the internal pipeline wall (Davidson, 2002).

In short, most of the findings for wax removal in pipes in the past were refined from laboratory experiments with waxy gels or mixtures of commercial wax and mineral oil. So far, the pigging model development is still not mature. In response, this paper (Huang *et al.*, 2017) aims to develop a pigging model to predict the wax-breaking force . which reveals that the wax-failure stress always exceeds the yield stress of the same wax deposit during pipeline pigging. In this paper, a laboratory setup is used to conduct pigging experiments to investigate the effect of the hardness of the scraping element in the pig on wax removal. Furthermore, a pigging model is developed to describe the wax removal from the pipe wall. This model could be a practical tool in designing the optimal pigging programs.

2.1.3.1.2 Thermal

The latest technology successfully integrated state-of-the-art in a heat management system to offer safe, reliable and cost-effective crude oil transfer. The pipeline is a versatile heat management system designed to deliver heat for pipelines that can be hundreds of kilometres long. When the heat are supply ,the temperature of the crude oil are always above the WAT the followability of the crude oil much more easier . The paraffin wax are not crystallize above the WAT . It is good for transporting the crude oil . Consequently, a huge amount of energy is consumed to heat the crude oil by hot water or electrical power every year

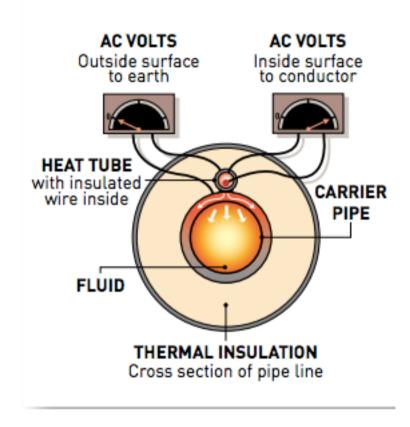


Figure 2. 3 : Cross section for typical single tube welded system (PENTAIR Raychem Tracer, 2010)

2.1.3.1.3 Magnetic Radiation

In order to save the energy cost, the magnetic paraffin control technology is presented and evaluated with the hot oiling method, and accordingly the effect of the magnetic radiation on the oil transportation is detailed. According to (Zhang, Zhang and Dong, 2010) the magnetic treatment can compensate for the resistance rising of the pipeline caused by the hot water reduction. Especially, the transportation of crude oil (at the surrounding temperature of -10°C~-30°C) without any heating has been observed in the Daqing oil field under the radiation of a magnetic field of 120 mT. In addition, the effect of the length of pipelines on the performance of magnetic treatment was also investigated.

In recent years, magnetic paraffin control (MPC) technology has been utilized as an assistance of conventional paraffin control methods (Tung *et al.*, 2003). Magnetic field treatment can aggregate paraffin particles inside the crude oil into large ones by reorienting paraffin molecules of magnetic anisotropy (Zhang *et al.*, 2015)(Takahashi *et al.*, 2004). The aggregation will increase the particle size and lead to the viscosity reduction of crude oil, which lowers the pressure drop and decreases the resistance of pipeline transportation. The magnetic treatment is performed with magnetic field activators installed on oil pipelines, which is safe and easy to adopt for practical applications. It is meaningful for transporting high-viscosity and paraffin-rich oils, especially for transportation of offshore oil via deep-water pipelines.

2.1.3.2 Chemical treatment

A lot of the crude oil industry ,preferred to applied the chemical treatment, because of the cost is much lower than physical treatment in term of maintenance. The usage of the chemical is minimum for the transportation of crude oil, this is because the chemical in liquid state, which easily to distribute after injected into pipeline. The turbulent flow in the pipeline help the chemical to well disperse to all the crude oil.

To overcome the problem in the pipeline of crude oil, ten years investigation has resulted in substantial progress in identification and chemical treatment of these problem areas. The chemical treatment inhibit the formation of the factor that make the flow ability of the crude oil in pipeline affected. The paraffin inhibitors or known as pour point depressant are polymers capable of crystal distortion or modification during the deposition process. Because of this co-crystallization mechanism, it is necessary to have the chemical in solution above the cloud-point temperature. This prevents or interferes with the molecular diffusion mechanism of deposition. It also modifies the crystal structure of waxes precipitated into small, highly branched structures with low cohesive properties. Three popular crystal modifiers are copolymers in these groups: (1) Group A-copolymer of ethylene vinyl acetate, (2) Group B-copolymer of C18 through C22 methacrylate, and (3) Group C-copolymer of olefin/maleic anhydride esters.

2.2 Polymer as Pour Point Depressant (PPD)

2.2.1 Overview Background of Pour Point Depressant (PPD)

Nowadays, the alternatives for managing cold flow issues were extremely restricted. Heat was a conspicuous arrangement, stories of flames being worked under the sumps of vehicles are for sure authentic. A more sensible option, in any event in a few cases, was to build the solvency power of the fluid portion of the oil by the addition of kerosene to the lubricant, however this additionally diminished the viscosity of the oil at high temperature. There was likewise the option of including one of a few normally happening materials, for example, asphaltenic resins or microcrystalline waxes, which were evacuated at different phases of the refining process. Unfortunately, while such materials were now and again sensibly powerful, they were not broadly applicable.

These materials depress the pour point of oil, they were designated pour point depressants. The presence of these naturally occurring pour point depressants proposed that there could well be synthetic materials that could function at low temperature and presumably better. The structures of natural hydrocarbon pour point depressants, is the greater part of the waxy materials themselves, if clear clues to the early synthetic efforts. The alkylated naphthalenes, wherein the alkyl groups contained linear waxy paraffinic structures. This improvement empowered the trial of other waxy materials.

Throughout the years, a wide assortment of synthetic materials has been presented industrially as pour point depressants. Chlorinated wax is the most outstanding case of small-molecule chemistry, however most business items are direct to high molecular weight polymers, for example, polymethacrylate, polyacrylate, acrylate-styrene copolymers, esterified olefin-or styrene maleic anhydride copolymers, alkylated polystyrene, and vinyl acetate-fumarate copolymers.

Dispersants are often blended with polymeric inhibitors to improve the additive performance. Low cost wax dispersants include alkyl sulfonates, fatty amine ethylates and other alkylated product. These products function well only when blended with polymeric inhibitor, (Hassan Ali, 2012) . Normal method to controlling the wax deposition for subsea pipelines is by regular pigging. According to Figure 2.4, this method improved the flow due to the passing the pipe is probably caused by a combination of smoothing of the rough wax layer and removal of the wax back into the

19

flowing oil. The smoothing of the pipeline deposits can significantly reduce the friction factor in turbulent flow (Zhang Fusheng, 1995).

According to (Souchik, 2009), they found that the treated PPD will change the structure of the paraffin wax mixture by partially transformed from orthorhombic into hexagonal form. This is important in wax plays the role of lowering the melting point of wax.

Polymeric materials have been advanced adequately to function for a wide temperature range by modify the flow properties of lubricants. There are few types of polymer commonly used, as wax inhibitor chemical, which are, olefin-based polymer and ester polymer. Ethylene vinyl acetate (EVA) and poly methacrylate (PMA) are the most common types of olefin and ester polymer used nowadays. Both types of the polymer have their own advantage and disadvantage. EVA is a block olefin copolymer with rubber like properties and has excellent viscosity modified properties. However, it has the lower pour point ability compare to the PMA.

The pour point is the lowest temperature which oil or fuel will pour under low temperature condition while the pour point depressant (PPD) is the chemical used to enhance the pour point of the fuel. PMA is belonging to acrylate family or commonly known as comb polymer family due to their comb-like structure. Comb polymer has excellent ability to act as pour point depressant since it can withstand low temperature condition, which is below 0°C. The high molecular weight PMA can act as both PPD and viscosity modifier. High molecular weight PMA can act as both PPD and viscosity modifier.

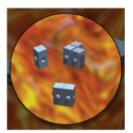
2.2.2 Mechanism of Pour Point Depressant (PPD)

The mechanism of the paraffin wax dispersant is to penetrate the into waxy oil gel, be adsorbed on individual particle, and reduce the tendency of wax particles to stick together. Moreover, the dispersants may adsorb on the inner surface of the pipeline and reduce the ability of wax to adhere to pipe wall.

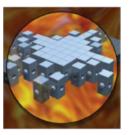
Figure 2.4 and Figure 2.5 show, the prevention mechanism of interlocking wax crystal by polymer additive. Figure 2.5 show the mechanism to modify the wax growth crystal ,it prevent agglomeration primarily involves the structure of the PPD to disrupt the crystal habit of wax crystal. The structure involved in this mechanism process which is the pendant chains, which use to co-crystallize with the wax and the polar end group. These groups are responsible for disrupting the orthorhombic crystal structure into a compact pyramidal form . This process prevents the crystal from agglomerating and forming a gel like structure to deposit in the pipeline surface.

When the paraffin wax are not treated with PPD the crystal structure easy to grow ,the lateral growth forms needles or plates like .The crystal structure continues to grow below the cloud point temperature ,so the large structure 3D crystal network formatting ,crystal size >100um ,the oil ceases to flow

The treated paraffin wax with PPD ,the co-crystallization occurs between wax molecules and PPD crystal units , the crystal confine to form a structured crystal due to present of polymer that modified the wax crystal growth .The interlocking of wax crystal is prevented ,leading to smaller and more random structure , hence creating fault in wax crystal which change the shape and size of wax crystal and prevent the interlocking of crystal into different shape . The end good of paraffin wax is no aggregation of gel-like wax network. The oil continues to flow without yield stress .



Crystallization of wax molecules below cloud point temperature



Mainly lateral growth forms needles or plates



Wax crystal structure continues to grow

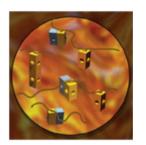


Large, structured 3D crystal network formation, crystal size >100um, oil ceases to flow

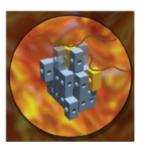
Figure 2. 4 Wax molecule formation without present of PPD (Souchik, 2009)

2.2.2.1 Adsorption and Co-crystallization theory

The polymer either being adsorbed into the face of the wax crystal if the PPD is comb polymer shown in Figure 2.5. Thus, the wax like components of the additive are incorporated into the wax crystal lattice and thus modify the morphology of the growing crystal (DeYoreo and Vekilov, 2003)



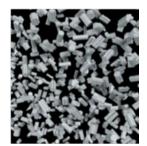
Co-crystallization occurs between wax molecules and PPD crystal units



PPD modified wax crystal growth



Interlocking of wax crystals is prevented, leading to smaller and more random structure



No aggregation of gel-like wax network, oil continues to flow wothout yield stress

Figure 2. 5 Wax molecule formation with present of PPD (Souchik, 2009)

According to (Yang *et al.*, 2015), at temperature near or below the WAT, many polymeric wax inhibitors and PPDs co-crystallize with wax molecules or adsorb on growing surface of precipitated wax crystal. Incorporation of polymeric wax inhibitor and PPDs into wax crystal disrupts growth, inhibiting wax deposition, and improving flow ability. Molecular dynamic (MD) simulation has been used to investigate the effect of polymeric Wax Inhibitors and PPDs on the growth of wax crystals (Yang *et al.*, 2015).

2.2.2.2 Nucleation theory

The additive heterogeneously nucleates the wax crystal and this result in crystal of relatively smaller size (DeYoreo and Vekilov, 2003). According to (Yang *et al.*, 2015), at temperature well above the WAT, certain polymeric WIs and PPDs self-assemble into micelle-like aggregate exhibition a crystalline core and soluble hairy brushes surrounding the core, creating a larger number of subcritical size wax nuclei (so-called poly nucleation) shown at Figure 2.6. Partially shielded nuclei reduce super saturation, reduce crystal growth rates, and facilitate of more abundant smaller wax crystals. Wax crystal size reduction facilities inhibition and rheological beneficiation.



Figure 2. 6 Image of POM treated crude oil and non-treated crude oil

2.3 Graphene oxide as Nano-material

2.3.1 Introduction to Graphene oxide

Graphene oxide has been study in the context of many application such as polymer nanocomposite, energy related materials, sensors, paper like materials, field effect transistor, and biomedical applications due to its excellent electrical, mechanical and thermal properties.(Potts *et al.*, 2011) Graphene oxide is a strongly oxygenated and highly hydrophilic layered material that can be readily exfoliated in water to yield stable dispersion consisting mostly of single-layer sheets which referred to as Graphene oxide sheets.