



Second Semester Examination  
Academic Session 2018/2019

June 2019

**EMH 222 – Fluid Dynamics**  
**[Dinamik Bendalir]**

Duration : 3 hours  
[Masa : 3 jam]

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Please check that this paper contains **TWELVE [12]** printed pages including appendix before you begin the examination.

*[Sila pastikan bahawa kertas soalan ini mengandungi **DUABELAS [12]** mukasurat bercetak beserta lampiran sebelum anda memulakan peperiksaan.]*

**INSTRUCTIONS** : Answer **ALL FIVE [5]** questions.  
**[ARAHAN** : Jawab **SEMUA LIMA [5]** soalan.]

In the event of any discrepancies, the English version shall be used.

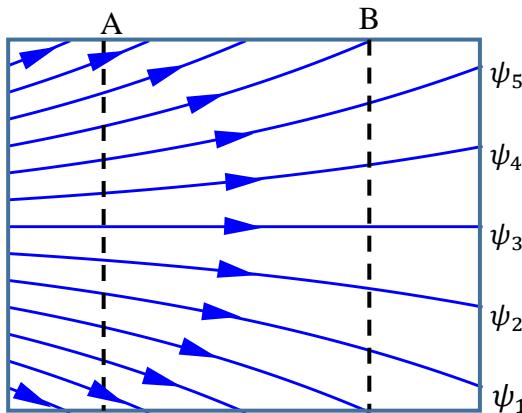
*[Sekiranya terdapat sebarang percanggahan pada soalan peperiksaan, versi Bahasa Inggeris hendaklah diguna pakai.]*

Thermodynamic Booklet is provided.  
*Buku Termodinamik adalah dibekalkan.*

1. [a] What is significant about curves of constant stream function? Discuss the flow at cross section A and at section B based on the streamlines depicted in Figure 1[a].

Apakah kepentingan keluk fungsi aliran malar? Bincangkan aliran rentas Seksyen A dan Seksyen B berdasarkan garis arus yang digambarkan dalam Rajah 1[a].

(20 marks/markah)



**Figure 1[a]**  
*Rajah 1 [a]*

- [b] What is the distinction between a Newtonian fluid and a non-Newtonian fluid? Name at least three Newtonian and non-Newtonian fluids.

Apakah perbezaan di antara bendalir Newtonian dan bendalir tak Newtonian? Namakan sekurang-kurangnya tiga bendalir Newtonian dan tak Newtonian?

(15 marks/markah)

- [c] The general control volume form of the linear momentum equation is:

Bentuk isipadu kawalan umum persamaan linear momentum ialah:

$$\int_{CV} \rho \vec{g} dV + \int_{CS} \sigma_{ij} \cdot \vec{n} dA = \int_{CV} \frac{\partial}{\partial t} (\rho \vec{V}) dV + \int_{CS} (\rho \vec{V}) \vec{V} \cdot \vec{n} dA$$

I                  II                  III                  IV

Define the momentum equation. Name the four labeled terms.  
Tentukan persamaan momen. Namakan empat istilah yang berlabel.

(15 marks/markah)

- [d] A thin flat plate is placed in between two parallel plates (top and bottom) as shown in Figure 1[d]. The distance separating this thin flat plate with both parallel plates is  $h$ . Apart from having a stationary top plate, the thin flat plate is moving at the velocity of  $U$  and the bottom plate is moving to the left at a velocity of  $0.2U$ .

*Satu plat nipis diletakkan di antara dua plat selari (atas dan bawah) seperti yang ditunjukkan dalam Rajah 1[d]. Jarak memisahkan plat ini dengan kedua-dua plat selari ialah  $h$ . Selain daripada plat atas tidak bergerak, plat nipis itu bergerak pada halaju  $U$ , manakala plat bawah bergerak ke kiri pada halaju  $0.2U$ .*

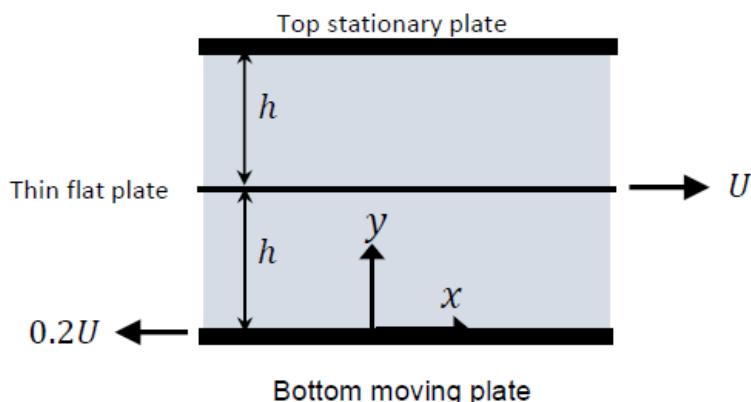
**Show that the governing equation can be simplified to  $\frac{d^2u}{dy^2} = 0$ .**

*Tunjukkan bahawa persamaan pentadbiran dapat diringkaskan ke  $\frac{d^2u}{dy^2} = 0$ .*

**Also, plot the resulting velocity profile. Given,  $U$  is 10 m/s.**

*Juga, plotkan profil halaju terhasil. Diberi,  $U$  ialah 10 m/s.*

**(50 marks/markah)**



**Figure 1[d]**  
*Rajah 1 [d]*

2. [a] In the non-dimensionalized incompressible Navier-Stokes equation, there are four non-dimensional parameters. Label each parameter and explain its physical significance when the parameter is very small or large?

*Dalam persamaan Navier-Stokes tanpa dimensi, terdapat empat parameter tanpa dimensi. Labelkan setiap parameter dan terangkan kepentingan fizikal apabila parameter adalah sangat kecil atau besar?*

$$\left[ \frac{fL}{V} \right] \frac{\partial \vec{V}^*}{\partial t^*} + (\vec{V}^* \cdot \vec{\nabla}^*) \vec{V}^* = - \left[ \frac{P_0 - P_\infty}{\rho V^2} \right] \vec{V}^* P^* + \left[ \frac{gL}{V^2} \right] \vec{g}^* + \left[ \frac{\mu}{\rho VL} \right] \nabla^{*2} \vec{V}^*$$

(20 marks/markah)

- [b] Derive whether the following flow is rotational or irrotational?**

Takrifkan sama ada aliran berikut adalah berputar atau tak berputar?

- (i)  $\phi = x^2 - y^2 + z^2$
- (ii)  $\phi = \sin(x + y + z)$

(30 marks/markah)

- [c] Air flows over a smooth flat plate with a free-stream velocity of 10 m/s (as shown in Figure 2c). The streamwise velocity component of the steady, incompressible and laminar flow can be approximated by a simple expression:**

Udara merentasi satu plat rata licin dengan halaju aliran bebas 10 m/s (seperti yang ditunjukkan dalam Rajah Q2c). Dalam aliran yang mantap, tak termampat dan laminar, komponen halaju boleh dianggarkan dengan ungkapan mudah:

$$\frac{u}{U} = \left( \frac{y}{\delta} \right) - \left( \frac{y}{\delta} \right)^2$$

**Where U is the free-stream velocity and  $\delta$  is the boundary layer thickness. Calculate:**

Di mana  $U$  adalah halaju aliran bebas dan  $\delta$  ketebalan lapisan sempadan. kirakan:

- (i) **The thickness of the laminar boundary layer at 50 cm from the leading edge.**  
Ketebalan lapisan sempadan laminar pada 50 cm daripada tepi depan
- (ii) **The local velocity and the velocity gradient at  $(x,y) = (0.5, 0.001)$ , located 50 cm from the leading edge and 0.1 cm above the plate.**  
Halaju setempat dan kecerunan halaju pada  $(x, y) = (0.5, 0.001)$ , terletak 50 cm dari tepi depan dan 0.1 cm di atas plat.

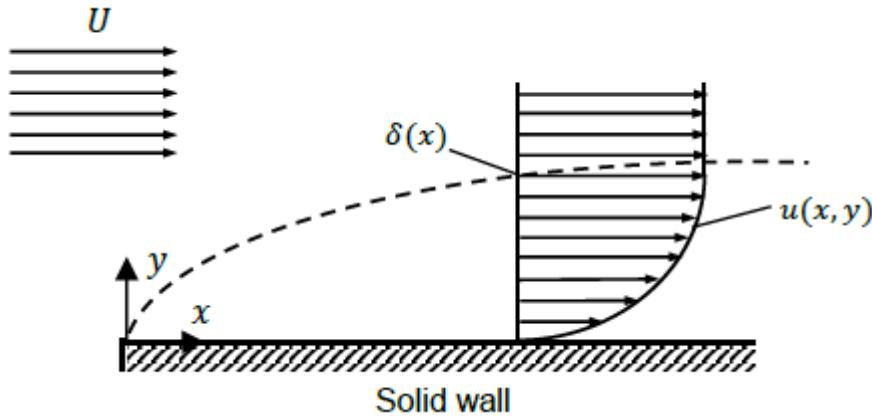
**Given, the air density and dynamic viscosity are**

$$\rho_{air} = 1.2 \text{ kg/m}^3 \text{ and } \mu_{air} = 1.9 \times 10^{-5} \text{ Ns/m}^2.$$

*Diberi, ketumpatan udara dan kelikatan dinamik ialah*

$$\rho_{udara} = 1.2 \text{ kg/m}^3 \text{ dan } \mu_{udara} = 1.9 \times 10^{-5} \text{ Ns/m}^2.$$

**(50 marks/markah)**



**Solid wall**

**Figure 2[c]**

*Rajah 2 [c]*

3. [a] A 3.5 mm spherical plastic sphere with a density of  $1100 \text{ kg/m}^3$  is dropping into water at  $30^\circ\text{C}$ . By assuming the fluid flow over the sphere is laminar and the drag coefficient is constant, calculate the terminal velocity of the sphere in water.  
(Given: The drag coefficient for sphere in laminar flow,  $C_D=0.5$ )

Satu sfera 3.5 mm plastik yang berketumpatan  $1100 \text{ kg/m}^3$  sedang jatuh ke dalam air pada  $30^\circ\text{C}$ . Dengan mengandaikan aliran bendarilir keatas sfera ialah laminar dan pekali seret malar, kirakan halaju terminal sfera dalam air.

(Diberikan : Koefisien seret untuk sfera dalam aliran laminar  $C_D=0.5$ )

**(30 marks/markah)**

- [b] Consider a circular sign with diameter 55cm as shown in Figure 3 subjected to normal air up to 160 km/h at 115 kPa and  $10^\circ\text{C}$ . The air flow is steady, incompressible and turbulent. If the drag force on the pole is negligible, calculate:

Pertimbangkan sebuah papan tanda bulatan yang berdiameter 55 cm seperti yang ditunjukkan dalam Rajah 3 dikenakan udara normal sehingga 160 km/h pada 115 kPa dan  $10^\circ\text{C}$ . Aliran udara ialah mantap, tak boleh mampat dan bergelora. Jika daya seret ke atas tiang diabaikan, kirakan:

- (i) **Drag force acting on the sign.**

*Daya seret yang bertindak pada papan tanda*

- (ii) **Bending moment at the bottom of the pole if the height from the ground to the bottom of the sign is 1.3 m.**  
*Momen lentur pada bahagian bawah tiang jika ketinggian daripada tanah ke bahagian bawah papan tanda tersebut ialah 1.3 m.*

**(Given: Drag coefficient for a thin circular disk is  $C_D = 1.1$ )**

*(Diberi: Pekali seretan untuk cakera nipis bulatan ialah  $C_D = 1.1$ )*



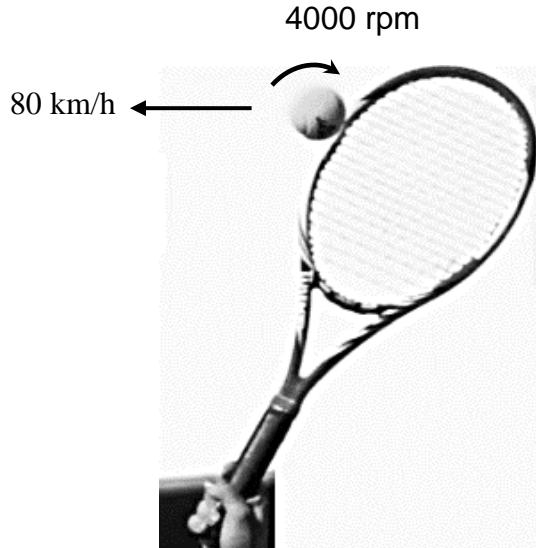
**Figure 3[b]**  
*Rajah 3[b]*

**(30 marks/markah)**

- [c] A tennis ball with a diameter of 6.5 cm and a mass of 52 g is hit with an initial velocity of 80 km/h and a backspin of 4000 rpm as shown in Figure 3 [c]. The outer surface of the ball is smooth and the racquet hit the ball horizontally. Given the density and kinematic viscosity of the air at 1 atm and are  $1.184 \text{ kg/m}^3$  and  $v = 1.562 \times 10^{-5} \text{ m}^2/\text{s}$ .

*Sebiji bola tenis berdiameter 6.5 cm yang berjisim 52 g dipukul dengan laju awal 80 km/j dan pusingan belakang 4000 rpm seperti ditunjukkan dalam Rajah 3 [c]. Permukaan luar bola itu lembut dan raket memukul bola dalam keadaan mendatar. Diberikan ketumpatan dan kelikatan kinematik bagi udara pada 1 atm sebagai  $1.184 \text{ kg/m}^3$  and  $v = 1.562 \times 10^{-5} \text{ m}^2/\text{s}$ .*

- (i) **Calculate the Lift**  
*Kirakan daya angkat*
- (ii) **By considering the effect of gravity and lift due to short spinning, determine the condition of the ball (fall or rise).**  
*Dengan mengambil kira kesan graviti dan daya angkat yang disebabkan pusingan pendek, tentukan keadaan bola (jatuh atau naik).*



**Figure 3 [c]**  
*Rajah 3[c]*

(40 marks/markah)

4. [a] Define Mach number.  
*Terangkan nombor Mach.*

(20 marks/markah)

- [b] In a supersonic wind tunnel, air is flowing with low velocity through a converging-diverging nozzle at temperature 300 K and pressure 1.5 MPa. At the exit nozzle, the normal shock wave occurs at Mach number,  $Ma = 2.5$ . By assuming the air is an ideal gas with constant specific heats and the flow is steady, calculate the Mach number, pressure, temperature, and velocity downstream the shock.

(Given: the properties of air,  $R = 0.287 \text{ kJ/kg.K}$ , and  $k=1.4$ )

*Di dalam terowong angin supersonik, udara sedang mengalir dengan halaju rendah melalui muncung menumpu-mencapah pada suhu 300 K dan tekanan 1.5 MPa. Pada bahagian keluar muncung, gelombang kejutan normal berlaku pada nombor Mach,  $Ma = 2.5$ . Dengan mengandaikan udara ialah gas unggul dengan haba tentu yang malar dan aliran adalah mantap, kirakan nombor Mach, tekanan, suhu dan halaju selepas kejutan*

(Diberikan: sifat-sifat udara,  $R = 0.287 \text{ kJ/kg.K}$ , dan  $k = 1.4$ )

(60 marks/markah)

- [c] Give TWO (2) differences between oblique shocks and normal shocks.

Berikan **DUA** (2) perbezaan tentang kejutan oblik dan kejutan normal.

(20 marks/markah)

5. [a] Define the following terms:  
Takrifkan istilah-istilah berikut:

- (i) pump,  
*pam,*
- (ii) turbine,  
*turbin,*
- (iii) positive-displacement machines, and  
*mesin sesaran positif,*
- (iv) dynamic machines.  
*mesin dinamik.*

(20 marks/markah)

- [b] At a hydroelectric power station, the gross head from the reservoir to the tailrace is 100 m and the volume flow rate of water through each turbine is 138 m<sup>3</sup>/s at 20°C. There are 15 identical parallel turbines, each with an efficiency of 93.2%, and all other mechanical energy losses are estimated to reduce the output by 2.5%. The generator has an efficiency of 93.5%. Assume the turbines are working at their best efficiency point, and the diameter of the turbine is  $D = 1.80$  m, and spins at  $n = 180$  rpm. Assuming the density of water at 20°C is 998 kg/m<sup>3</sup>.

*Di satu stesen janakuasa hidroelektrik, turus kasar dari takungan ke alur limpah ialah 100 m dan kadar aliran isipadu air melalui setiap turbin ialah 138 m<sup>3</sup>/s pada 20°C. Terdapat 15 turbin selari yang serupa, masing-masing dengan kecekapan sebanyak 93.2%, dan semua kerugian tenaga mekanikal lain dianggarkan mengurangkan keluaran sebanyak 2.5%. Penjana berkecekapan sebanyak 93.5%. Anggapkan turbin bekerja pada titik kecekapan yang terbaik, dan diameter turbin ialah  $D = 1.80$  m, dan berputar pada  $n = 180$  rpm. Anggap ketumpatan air pada 20°C ialah 998 kg/m<sup>3</sup>.*

**Calculate:**

*Kirakan:*

- (i) brake horsepower of each existing turbine,  
*kuasa kuda brek untuk setiap turbin yang sedia ada,*

- (ii) the total electric power production from the station in MW by using the existing turbines.

*jumlah kuasa elektrik yang terjana dari stesen dalam MW dengan menggunakan turbin yang sedia ada.*

**(30 marks/markah)**

If you are required to retrofit the turbines by scaling up the existing turbines. The new turbines will spin at 100 rpm and gross head is 130 m.

*Jika anda diminta untuk naiktaraf turbin dengan peningkatan skala turbin yang sedia ada. Turbin baru akan berputar pada 100 rpm dan turus kasar ialah 130 m.*

**Calculate:**

*Kirakan:*

- (iii) the diameter of the new turbine as it operates most efficiently,

*diameter turbin semasa ia beroperasi pada titik kecekapan yang terbaik,*

- (iv) volumetric flow rate of water through each new turbine,

*kadar aliran isipadu air melalui setiap turbin baru,*

- (v) brake horsepower of each new turbine,

*kuasa kuda brek untuk setiap turbin baru,*

- (vi) the total electric power production from the plant in MW by using the new turbines.

*jumlah kuasa elektrik yang terjana dari stesen dalam MW dengan menggunakan turbin yang baru.*

**(50 marks/markah)**

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**Appendix 1**  
*Lampiran 1*

**Formula**

$$1. \ C_D = \frac{F_D}{\frac{1}{2}\rho V^2 A}$$

$$2. \ C_L = \frac{F_L}{\frac{1}{2}\rho V^2 A}$$

$$3. \ F_D = W - F_B$$

$$4. \ W = \rho_S g V$$

$$5. \ F_B = \rho_f g V$$

$$6. \ Re = \frac{\rho V D}{\mu}$$

$$7. \ \rho = \frac{P}{RT}$$

$$8. \ M = F_D L$$

$$9. \ \text{No dimensional rate of rotation} = \omega D / 2V$$

$$10. \ F_L = C_L A \frac{\rho V^2}{2}$$

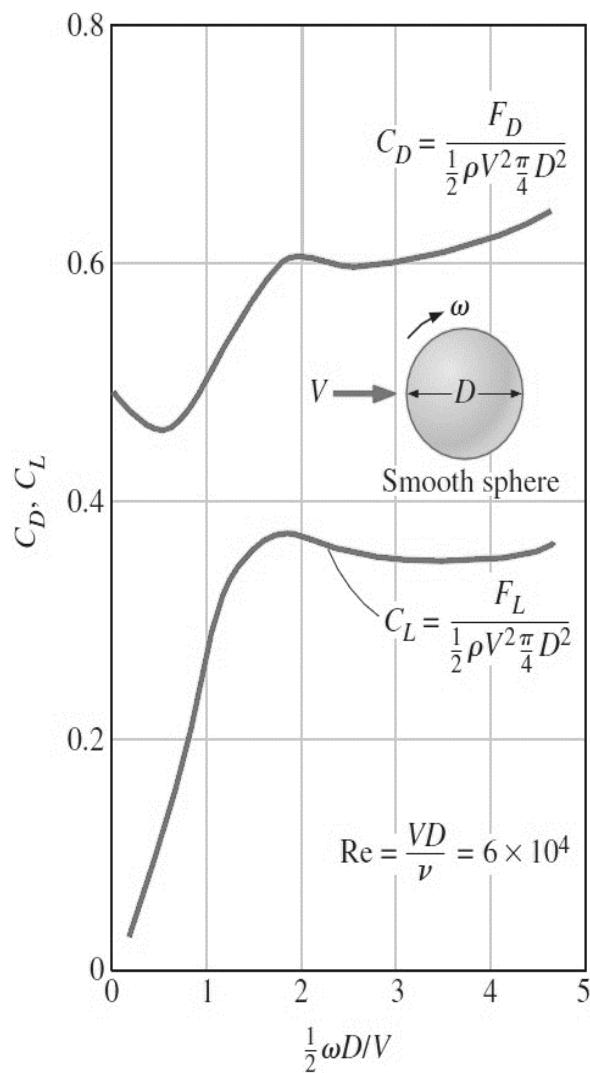
$$11. \ Re_L = \frac{VD}{\nu}$$

$$12. \ \text{Sphere, } A = (\pi D^2)/4$$

$$13. \ \frac{T_o}{T} = 1 + \left( \frac{k-1}{2} \right) Ma^2$$

$$14. \ \frac{P_o}{P} = \left[ 1 + \left( \frac{k-1}{2} Ma^2 \right) \right]^{k/(k-1)}$$

$$15. \ \frac{\rho_o}{\rho} = \left[ 1 + \left( \frac{k-1}{2} Ma^2 \right) \right]^{k/(k-1)}$$

**Appendix 2**  
*Lampiran 2*

### Appendix 3

*Lampiran 3*

Summary of expressions for laminar and turbulent boundary layer on a smooth flat plate aligned parallel to a uniform stream

Property	Laminar	Turbulent
Boundary layer thickness	$\frac{\delta}{x} = \frac{4.91}{\sqrt{Re_x}}$	$\frac{\delta}{x} = \frac{0.16}{(Re_x)^{1/7}}$
Displacement thickness	$\frac{\delta^*}{x} = \frac{1.72}{\sqrt{Re_x}}$	$\frac{\delta^*}{x} = \frac{0.020}{(Re_x)^{1/7}}$
Momentum thickness	$\frac{\theta}{x} = \frac{0.664}{\sqrt{Re_x}}$	$\frac{\theta}{x} = \frac{0.016}{(Re_x)^{1/7}}$
Local skin friction coefficient	$C_{f,x} = \frac{0.664}{\sqrt{Re_x}}$	$C_{f,x} = \frac{0.027}{(Re_x)^{1/7}}$

Water horsepower:  $\dot{W}_{\text{water horsepower}} = \dot{m}gH = \rho g \dot{V}H$

Volume flow rate:  $\dot{V} = 2\pi r_1 b_1 V_{1,n} = 2\pi r_2 b_2 V_{2,n}$

Tangential velocity,  $V_{1,t} = V_{1,n} \tan \alpha_2$

Net head:  $H = \frac{1}{g} (\omega r_2 V_{2,t} - \omega r_1 V_{1,t})$

Affinity laws  $\frac{\dot{V}_B}{\dot{V}_A} = \frac{\omega_B}{\omega_A} \left( \frac{D_B}{D_A} \right)^3$

$$\frac{H_B}{H_A} = \left( \frac{\omega_B}{\omega_A} \right)^2 \left( \frac{D_B}{D_A} \right)^2$$

$$\frac{\text{bhp}_B}{\text{bhp}_A} = \frac{\rho_B}{\rho_A} \left( \frac{\omega_B}{\omega_A} \right)^3 \left( \frac{D_B}{D_A} \right)^5$$









