

Fundamental Equations in Vibration

$$1. \zeta = \frac{c}{2m\omega_n};$$

$$2. x(t) = Ce^{-\zeta\omega_n t} \sin(\omega_d t + \psi), \quad \omega_d = \sqrt{1 - \zeta^2}\omega_n$$

$$C = \sqrt{x_0^2 + \frac{(\dot{x}_0 + \zeta\omega_n x_0)^2}{(1 - \zeta^2)\omega_n^2}} \quad ; \quad \psi = \tan^{-1} \frac{\sqrt{1 - \zeta^2}\omega_n x_0}{\dot{x}_0 + \zeta\omega_n x_0}$$

$$3. \text{ For } F(t) = me\omega^2 \sin \omega t$$

$$X = \frac{me\omega^2}{\sqrt{(k - M\omega^2)^2 + (c\omega^2)^2}}, \quad \phi = \tan^{-1} \left[\frac{c\omega}{k - M\omega^2} \right]$$

$$\frac{F_T}{F_0} = \left[\frac{1 + (2\zeta r)^2}{(1 - r^2)^2 + (2\zeta r)^2} \right]^{1/2}$$

$$4. \text{ For } y = Y \sin \omega t,$$

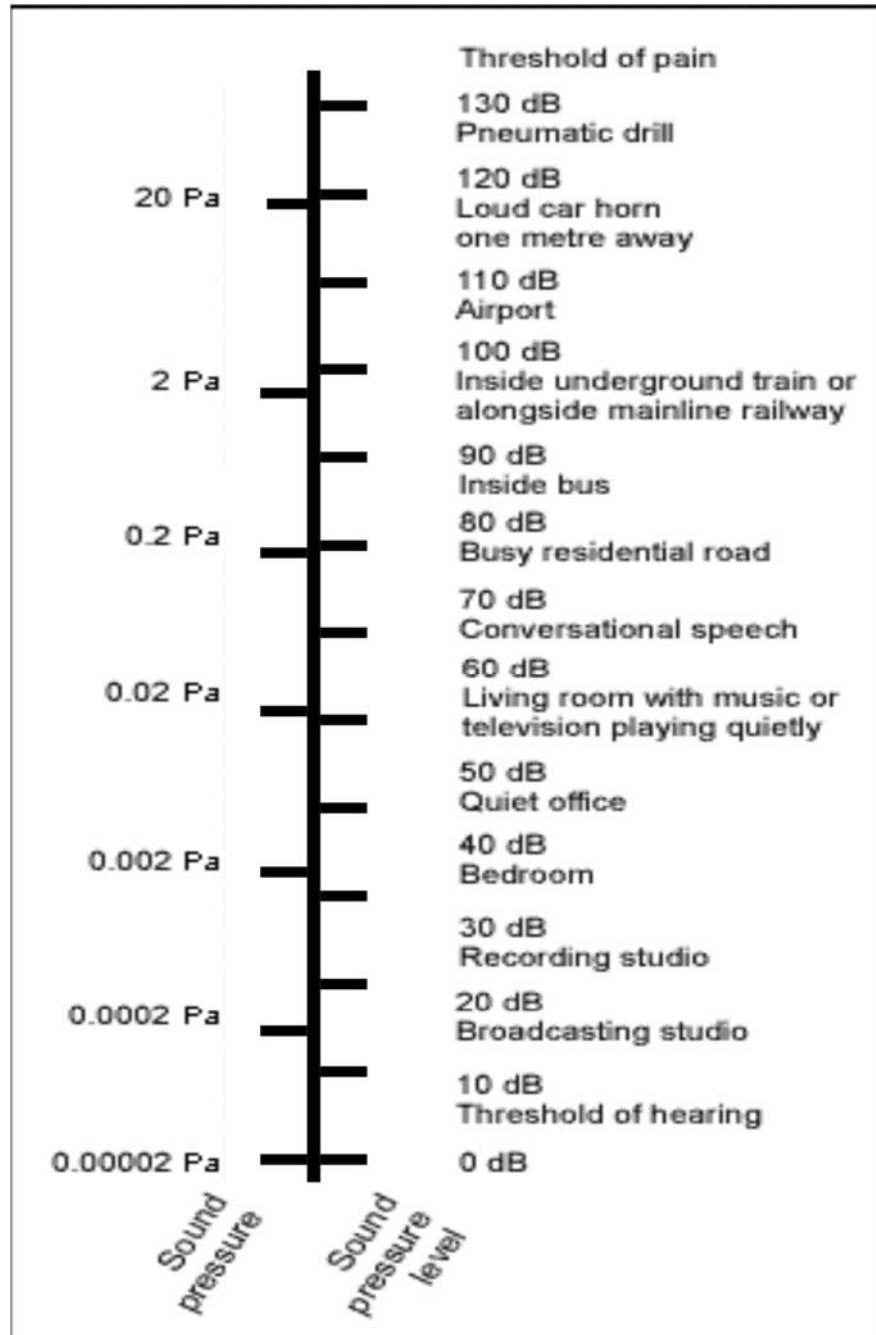
$$\frac{X}{Y} = \left[\frac{1 + (2\zeta r)^2}{(1 - r^2)^2 + (2\zeta r)^2} \right]^{1/2} \quad \phi = \tan^{-1} \left[\frac{2\zeta r^3}{1 + (4\zeta^2 - 1)r^2} \right]$$

$$\frac{F_T}{kY} = r^2 \left[\frac{1 + (2\zeta r)^2}{(1 - r^2)^2 + (2\zeta r)^2} \right]^{1/2}$$

$$5. \begin{pmatrix} a & b \\ c & d \end{pmatrix}^{-1} = \begin{pmatrix} d & -b \\ -c & a \end{pmatrix} \frac{1}{\Delta(\omega)} \quad ; \quad \det \begin{pmatrix} a & b \\ c & d \end{pmatrix} = ad - bc$$

$$6. \text{ For cantilever beam with load } P \text{ at the free end, } \delta_{\max} = PL^3(3EI)^{-1}$$

$$7. \text{ For cantilever beam with uniform load } w, \delta_{\max} = wL^4(8EI)^{-1}$$

Sound Pressure Level**Figure Q5[a]: Sound Pressure Level***Rajah S5[a]: Paras Tekanan Bunyi*

APPENDIX 3 / LAMPIRAN 3

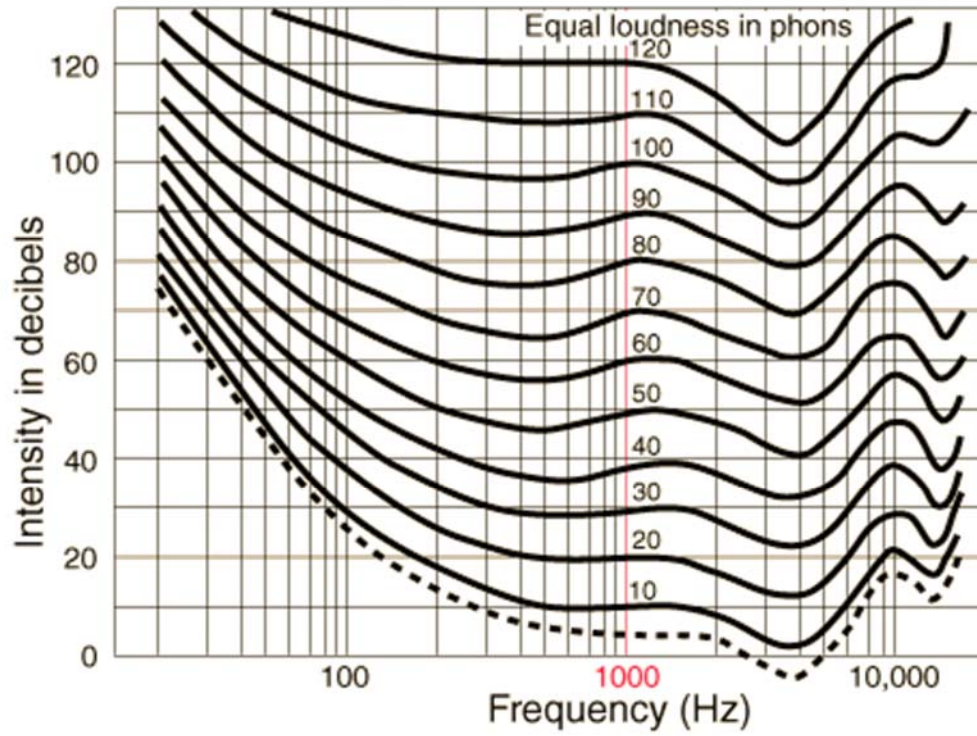


Figure Q5[c]: Equal Loudness Curves
Rajah S5[c]: Lengkungan Sama Nyaring

APPENDIX 4 / LAMPIRAN 4

Energy Attenuation Constant for Air**(a) 4m (1/ft)**

| Relative Humidity | Temperature °C(°F) | 2,000 Hz | 4,000 Hz | 6,300 Hz | 8,000 Hz |
|--------------------------|---------------------------|-----------------|-----------------|-----------------|-----------------|
| 30% | 15 (59) | 0.0044 | 0.0148 | 0.0322 | 0.0410 |
| | 20 (68) | 0.0036 | 0.0116 | 0.0256 | |
| | 25 (77) | 0.0035 | 0.0095 | 0.0209 | |
| | 30 (86) | 0.0034 | 0.0086 | 0.0172 | |
| 50% | 15 (59) | 0.0030 | 0.0087 | 0.0191 | 0.0260 |
| | 20 (68) | 0.0020 | 0.0074 | 0.0153 | |
| | 25 (77) | 0.0029 | 0.0072 | 0.0135 | |
| | 30 (86) | 0.0028 | 0.0071 | 0.0130 | |
| 70% | 15 (50) | 0.0027 | 0.0068 | 0.0138 | 0.0184 |
| | 20 (68) | 0.0026 | 0.0065 | 0.0122 | |
| | 25 (77) | 0.0026 | 0.0064 | 0.0118 | |
| | 30 (86) | 0.0025 | 0.0063 | 0.0117 | |

(b) 4m (1/m)

| | | | | | |
|------------|----------------|---------------|---------------|---------------|---------------|
| 30% | 15 (59) | 0.0143 | 0.0486 | 0.1056 | 0.1360 |
| | 20 (68) | 0.0119 | 0.0379 | 0.0840 | |
| | 25 (77) | 0.0114 | 0.0313 | 0.0685 | |
| | 30 (86) | 0.0111 | 0.0281 | 0.0564 | |
| 50% | 15 (59) | 0.0099 | 0.0286 | 0.0626 | 0.0860 |
| | 20 (68) | 0.0096 | 0.0244 | 0.0503 | |
| | 25 (77) | 0.0095 | 0.0235 | 0.0444 | |
| | 30 (86) | 0.0092 | 0.0233 | 0.0426 | |
| 70% | 15 (59) | 0.0088 | 0.0223 | 0.0454 | 0.0600 |
| | 20 (68) | 0.0085 | 0.0213 | 0.0399 | |
| | 25 (77) | 0.0084 | 0.0211 | 0.0388 | |
| | 30 (86) | 0.0082 | 0.0207 | 0.0383 | |