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UNIVERSITI SAINS MALAYSIA

First Semester Examination  
2012/2013 Academic Session

January 2013

**ESA461/2 – Flight Stability and Control II**  
*[ Kawalan dan Kestabilan Pesawat II ]*

Duration : 2 hours  
*Masa : 2 jam*

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Please check that this paper contains **EIGHT (8)** printed pages, **TWO (2)** pages appendix and **FOUR (4)** questions before you begin the examination.

*Sila pastikan bahawa kertas soalan ini mengandungi **LAPAN (8)** mukasurat bercetak, **DUA (2)** mukasurat lampiran dan **EMPAT (4)** soalan sebelum anda memulakan peperiksaan.*

**Instructions** : Answer **FOUR (4)** questions.

**Arahan** : Jawab **EMPAT (4)** soalan.

1. **Appendix A/Lampiran A** [1 page/mukasurat]

2. **Appendix B/Lampiran B** [1 page/mukasurat]

Answer all questions in **English** OR **Bahasa Malaysia**.

*Menjawab semua soalan dalam **Bahasa Inggeris ATAU Bahasa Malaysia**.*

Answer to each question must begin from a new page.

*Jawapan untuk setiap soalan mestilah dimulakan pada mukasurat yang baru.*

In the event of any discrepancies, the English version shall be used.

*Sekiranya terdapat sebarang percanggahan pada soalan peperiksaan, versi Bahasa Inggeris hendaklah diguna pakai.*

1. [a] Briefly explain about directional stability and state the conditions required for an aircraft to remain stable in this motion.

*Terangkan dengan ringkas tentang kestabilan berarah dan nyatakan keadaan yang diperlukan untuk sebuah kapal terbang kekal stabil dalam pergerakan ini.*

**(6 marks/markah)**

- [b] Briefly explain about directional-lateral stability and state the conditions required for an aircraft to remain stable in this motion.

*Terangkan dengan ringkas tentang kestabilan berarah-sisian dan nyatakan keadaan yang diperlukan untuk sebuah kapal terbang kekal stabil dalam pergerakan ini.*

**(6 marks/markah)**

- [c] Vertical tail is one of the most influential components in directional stability. Its contribution to the aircraft's directional stability can be calculated from the following equation

*Ekor menegak merupakan salah satu komponen yang berpengaruh dalam kestabilan berarah. Sumbangannya kepada kestabilan berarah pesawat boleh dikira dengan menggunakan formula berikut*

$$C_{n_{\beta v}} = V_v \eta_v C_{L_{\alpha v}} \left( 1 + \frac{d\sigma}{d\beta} \right)$$

where

*di mana*

$$\eta_v \left( 1 + \frac{d\sigma}{d\beta} \right) = 0.724 + 3.06 \frac{S_v/S}{1 + \cos \Lambda_{c/4w}} + 0.4 \frac{z_w}{d} + 0.009AR_w$$

Let say a model of an airplane is tested in a wind tunnel with vertical tail off. Contributions of various components give  $C_{n_{\beta}} = -0.001 \text{ deg}^{-1}$ . If the vertical tail is to be positioned at a point on the aft end of the fuselage giving a tail length of 4.8 m, estimate the required vertical tail area to give an overall  $C_{n_{\beta}} = 0.001 \text{ deg}^{-1}$ ? Given  $C_{L_{\alpha v}} = 0.0454$ ,  $\Lambda_{c/4w} = 0$ ,  $S = 18 \text{ m}^2$ ,  $b = 10.6 \text{ m}$  and the wing is set at the middle of the fuselage.

*Katakan sebuah model pesawat tanpa ekor menegak diuji dalam sebuah terowong angin. Sumbangan pelbagai komponen pesawat tersebut memberikan  $C_{n_{\beta}} = -0.001 \text{ deg}^{-1}$ . Jika ekor menegak diletakkan pada bahagian belakang pesawat iaitu di hujung fuislaj dengan panjang ekor adalah 4.8 m, anggarkan luas permukaan ekor menegak yang diperlukan untuk memberi kestabilan keseluruhan  $C_{n_{\beta}} = 0.001 \text{ deg}^{-1}$ . Diberi  $C_{L_{\alpha v}} = 0.0454$ ,  $\Lambda_{c/4w} = 0$ ,  $S = 18 \text{ m}^2$ ,  $b = 10.6 \text{ m}$  dan pesawat diletakkan pada pertengahan fuislaj.*

**(15 marks/markah)**

2. [a] Explain why deflecting the ailerons produce a yawing moment.

*Terangkan mengapa dengan memesongkan aileron menghasilkan momen rewang.*

**(6 marks/markah)**

- [b] For the twin engine airplane shown in Figure 1, determine the rudder size to control the airplane if one engine needs to be shut down. Use the following flight information

*Untuk kapal terbang dengan enjin berkembar seperti dalam Gambarajah 2, tentukan saiz kemudi untuk mengawal kapal terbang jika salah satu daripada enjin tersebut perlu dimatikan. Gunakan informasi penerbangan berikut*

Wing:

Sayap:  $S = 980 \text{ ft}^2 \quad b = 93 \text{ ft}$

Vertical tail:

$S_v = 330 \text{ ft}^2 \quad AR_v = 4.3 \quad l_v = 37 \text{ ft} \quad \eta_v = 1.0$

Ekor tegak:

$C_{L_{\alpha_v}} = 4.02 \text{ rad}^{-1}$

Rudder:

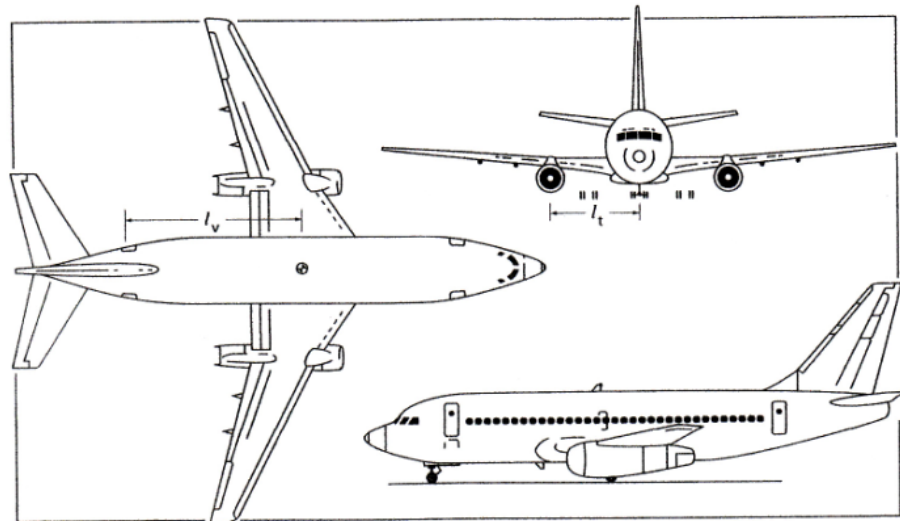
Kemudi:  $\delta_r = \pm 15^\circ$

Propulsion:

Pendorongan:  $T = 14\,000 \text{ lb each} \quad y_T = 16 \text{ ft}$

Flight condition:

Keadaan penerbangan:  $V = 250 \text{ ft/s} \quad \rho = 0.002378 \text{ slug/ft}^3$



**Figure 1 /Rajah 1**

**(13 marks/markah)**

- [c] Briefly explain how the force equations and moment equations of the aircraft are developed.

*Terang secara ringkas bagaimana persamaan-persamaan daya dan persamaan-persamaan momen untuk pesawat diterbitkan.*

**(4 marks/markah)**

3. Figure 2 illustrates a wind tunnel model that can only perform yawing motions. Using the data for general aviation airplane in Appendix A, determine the following;

*Rajah 2 menunjukkan model terowong angin yang hanya boleh melaksanakan pergerakan rewang. Dengan menggunakan data bagi pesawat penerbangan umum di lampiran A, tentukan berikut;*

- [a] The yawing moment equation rewritten in state-space form.  
*Persamaan momen rewang ditulis dalam bentuk ruang keadaan.*  
(7 marks/markah)
- [b] The characteristics equation and eigenvalues for the system.  
*Persamaan ciri-ciri dan nilai-nilai eigen bagi sistem.*  
(8 marks/markah)
- [c] The damping ratio,  $\zeta$ , and undamped natural frequency,  $\omega_n$ .  
*Nisbah redaman  $\zeta$ , dan frekuensi tabii tak terendam,  $\omega_n$ .*  
(7 marks/markah)
- [d] The response of the airplane to a  $5^\circ$  rudder input. Assume the initial conditions are  $\Delta\beta(0)=0, \Delta r(0)=0$ ;  
*Sambutan pesawat tersebut kepada masukan  $5^\circ$  kemudi. Andaikan keadaan awal adalah  $\Delta\beta(0)=0, \Delta r(0)=0$ ;*  
(8 marks/markah)

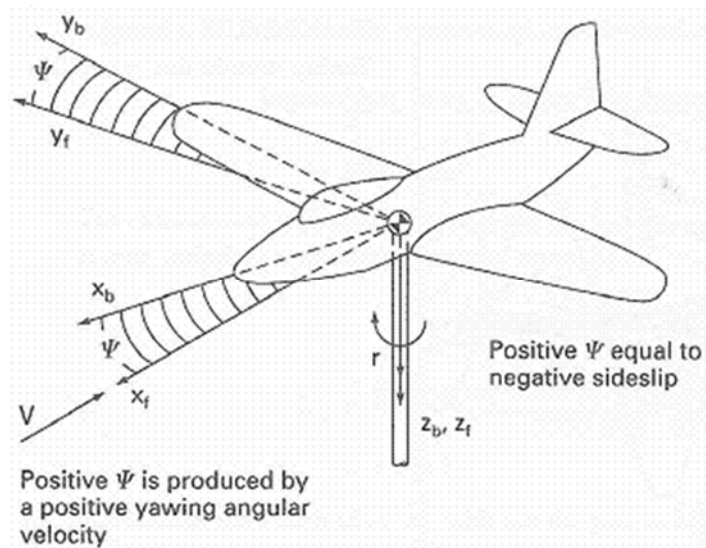


Figure 2/Rajah 2

4. The vertical motion of an airplane subjected to a sharp-edged gust is described by the equation  $\Delta w(t) = A_g(1 - e^{-t/\tau})$ , where  $\Delta w$  is in the vertical velocity,  $A_g$  is a magnitude of the gust, and  $\tau$  is the time constant of the airplane. Using the information in Figure 3, determine the maximum vertical acceleration and the time constant of the airplane.

*Gerakan tegak kapal terbang tertakluk kepada tiupan tajam seperti digambarkan oleh persamaan  $\Delta w(t) = A_g(1 - e^{-t/\tau})$ , di mana  $\Delta w$  dalam halaju menegak dan  $A_g$  adalah magnitud tiupan dan  $\tau$  adalah pemalar bagi masa pesawat tersebut. Dengan berpandukan Rajah 3, tentukan pecutan maksimum menegak dan pemalar masa bagi pesawat tersebut.*

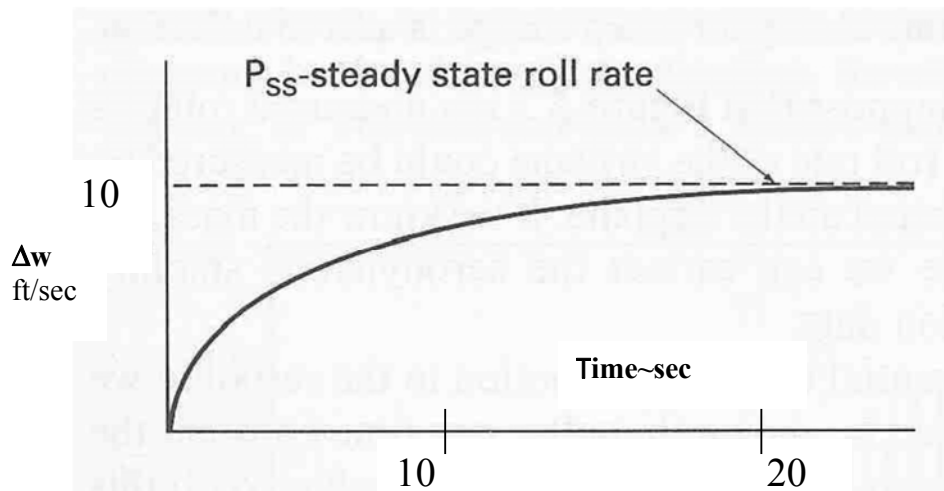


Figure 3/Rajah 3

(20 marks/markah)

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## APPENDIX A/ LAMPIRAN A

**TABLE B.1**  
General aviation airplane: NAVION

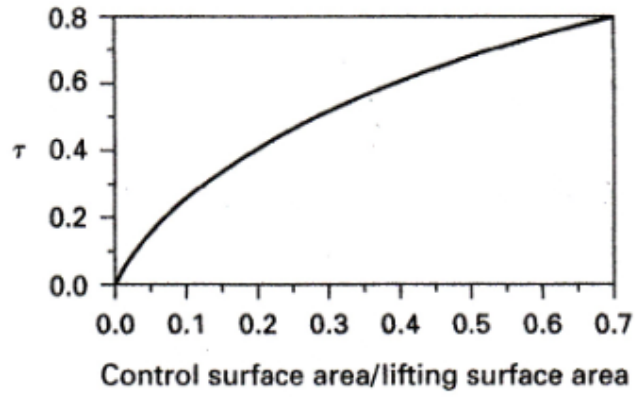
Longitudinal M = 0.158	$C_L$	$C_D$	$C_{L\alpha}$	$C_{D\alpha}$	$C_{m\alpha}$	$C_{L\dot{\alpha}}$	$C_{m\dot{\alpha}}$	$C_{Lq}$	$C_{mq}$	$C_{LM}$	$C_{DM}$	$C_{mM}$	$C_{L\dot{\alpha}_e}$	$C_{m\dot{\alpha}_e}$
Sea level	0.41	0.05	4.44	0.33	-0.683	0.0	-4.36	3.8	-9.96	0.0	0.0	0.0	0.355	-0.923
Lateral M = 0.158	$C_{y\beta}$	$C_{lp}$	$C_{n\beta}$	$C_{lp}$	$C_{nr}$	$C_{lr}$	$C_{nr}$	$C_{l\dot{\beta}}$	$C_{n\dot{\beta}}$	$C_{y\dot{\beta}}$	$C_{l\dot{\beta}}$	$C_{n\dot{\beta}}$		
Sea level	-0.564	-0.074	-0.071	-0.410	-0.0575	0.107	-0.125	-0.134	-0.0035	0.157	0.107	-0.072		

Note: All derivatives are per radian.

**TABLE 5.1**  
Summary of lateral directional derivatives

$$\begin{aligned}
 Y_{\beta} &= \frac{QSC_{y\beta}}{m} \quad (\text{ft/s}^2 \text{ or } \text{m/s}^2) & N_{\beta} &= \frac{Q Sb C_{n\beta}}{I_z} \quad (\text{s}^{-2}) & L_{\beta} &= \frac{Q Sb C_{l\beta}}{I_x} \quad (\text{s}^{-2}) \\
 Y_p &= \frac{Q Sb C_{yp}}{2mu_0} \quad (\text{ft/s} \text{ or } \text{m/s}) & N_p &= \frac{Q Sb^2 C_{np}}{2I_z u_0} \quad (\text{s}^{-1}) \\
 L_p &= \frac{Q Sb^2 C_{lp}}{2I_x u_0} \quad (\text{s}^{-1}) \\
 Y_r &= \frac{Q Sb C_{yr}}{2mu_0} \quad (\text{ft/s} \text{ or } \text{m/s}) & N_r &= \frac{Q Sb^2 C_{nr}}{2I_z u_0} \quad (\text{s}^{-1}) \\
 L_r &= \frac{Q Sb^2 C_{lr}}{2I_x u_0} \quad (\text{s}^{-1}) \\
 Y_{\delta a} &= \frac{Q SC_{y\delta a}}{m} \quad (\text{ft/s}^2 \text{ or } \text{m/s}^2) & Y_{\delta r} &= \frac{Q SC_{y\delta r}}{m} \quad (\text{ft/s}^2 \text{ or } \text{m/s}^2) \\
 N_{\delta a} &= \frac{Q Sb C_{n\delta a}}{I_z} \quad (\text{s}^{-2}) & N_{\delta r} &= \frac{Q Sb C_{n\delta r}}{I_z} \quad (\text{s}^{-2}) \\
 L_{\delta a} &= \frac{Q Sb C_{l\delta a}}{I_x} \quad (\text{s}^{-2}) & L_{\delta r} &= \frac{Q Sb C_{l\delta r}}{I_x} \quad (\text{s}^{-2})
 \end{aligned}$$

**APPENDIX B/ LAMPIRAN B**



**Flap effectiveness parameter**