

**SYNTHESIS OF TIO₂-PVDF MEMBRANE
WITH ENHANCED WETTING RESISTANCE
FOR MEMBRANE DISTILLATION
APPLICATION**

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UNIVERSITI SAINS MALAYSIA

2018

**SYNTHESIS OF TiO₂-PVDF MEMBRANE WITH ENHANCED WETTING
RESISTANCE FOR MEMBRANE DISTILLATION APPLICATION**

by

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**Thesis submitted in fulfillment of the
requirements for the degree of
Doctor of Philosophy**

August 2018

ACKNOWLEDGEMENT

By the name of Allah, the Most Merciful, who is listening to all prayers of His humble servants, I would like to first and foremost to express our boundless gratitude to Allah, for without His will I could never complete this dissertation in time. First of all, I would like to express my heart-felt thank you to my supervisor, Assoc. Prof. Dr.Ooi Boon Seng for his patient guidance, infinite suggestions and great inspiration throughout the research study. For my co-supervisor, Dr. Khairiah Abd. Karim I appreciate her encouragement that stimulates my heart and mind to work optimistically and energetically.

I would like also to express my gratitude to the Dean and Deputy Dean of School of Chemical Engineering for the support and research facilities available in the school. I would like to extend my heartfelt appreciation to SLAI UnIMAP, KPT and Research University Grant for providing me financial support. A deep appreciation is dedicated to all staffs and technicians in School of Chemical Engineering for their kindness assistant and co-operation. My special thanks to my beloved parents, Mohd Yatim Abu Bakar and Norhayati Bt Ali for their endless love, prayer, support and encouragement throughout my studies. Also, to my brother and sister, thank you for your support and courage.

My sincerely gratefulness and adored husband and son, Mohd Helmi B. Samta and Muhammad Fahim Izzudin B. Mohd Helmi, for his prayer, endless love, encourage and concerns throughout this study. Last but never the least; I would like to express my gratitude to all my fellow friends for their courage and moral support. Also, I would like to express my gratitude to all people who directly or indirectly help me throughout all this while.

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LIST OF ABBREVIATIONS

AGMD	Air-gap membrane distillation
APTES	3- aminopropyltriethoxysilane
AFM	Atomic force microscopy
BOD	Biological oxygen demand
BCA	Bicinchoninic acid assay
<i>B.Subtilis</i>	<i>Bacillus Subtilis</i>
COD	Chemical Oxygen Demand
CA	Contact angle
CB	Cassie-Baxter
DCMD	Direct-contact membrane distillation
DMF	Dimethyl formamide
DMAC	N, N-dimethyl acetamide
EE	Energy efficiency
<i>E.Coli</i>	<i>Escherichia coli</i>
ENM	Electron nanofibre membrane
FTCS	Fluorosilane , 1H,1H,2H,2H-Perfluorooctyltriethoxysilane
LMH	L/ m ² / hr
LEP _w	Liquid entry pressure of water
MD	Membrane distillation
MF	Microfiltration
MAPTMS	3-methacryloyloxypropyl trimethoxysilane
MMDES	methacryloyloxy methylenemethyl diethoxysilan
M-12	Neat Membrane with polymer concentration of PVDF in 12% w/v

M-16	Neat Membrane with polymer concentration of PVDF in 16% w/v
M-20	Neat Membrane with polymer concentration of PVDF in 20% w/v
M-PVDF	Neat PVDF Membrane
MT-0	Neat PVDF Membrane without TiO ₂
MT-0.01	Nano-composite membrane with 0.01g dosage TiO ₂
MT-0.1	Nano-composite membrane with 0.1g dosage TiO ₂
MT-0.5	Nano-composite membrane with 0.5g dosage TiO ₂
MT-1.0	Nano-composite membrane with 1g dosage TiO ₂
MT-UT	Nano-composite membrane with untreated TiO ₂
MT-AC	Nano-composite membrane with acid treated TiO ₂
MT-AL	Nano-composite membrane with alkali treated TiO ₂
MT-Si-2	Nano-composite membrane with silane treated TiO ₂ at pH 2
MT-Si-7	Nano-composite membrane with silane treated TiO ₂ at pH 2
MT-Si-12	Nano-composite membrane with silane treated TiO ₂ at pH 12
NF	Nanofiltration
NMP	N-methyl-2-pyrrolidone
NIPS	Non-solvent induced phase separation
OMW	Olive mill wastewater
PMR	Photocatalytic membrane reactor
PTFE	Polytetrafluoroethylene
PVDF	Poly(vinylidene fluoride)
PP	Polypropylene
PE	Polyofelin
POME	Palm oil mill effluent
PMSE	Paper mill SBR effluent

PBS	Phosphate buffer saline
RO	Reverse Osmosis
RE	Renewable energy
SGMD	Sweep Gas membrane distillation
SEM	Scanning electron microscopy
T-AC	TiO ₂ treated with acid
T-AL	TiO ₂ treated with alkali
T-Si-2	TiO ₂ treated with silane at pH 2
T-Si-7	TiO ₂ treated with silane at pH 7
T-Si-12	TiO ₂ treated with silane at pH 12
TE	Thermal efficiency
TEM	Transmission electron microscopy
TIPS	Thermally induced phase separation
TiO ₂	Titanium dioxide
TPC	Temperature polarization coefficient
UF	Ultrafiltration
UT	Untreated TiO ₂
VMD	Vacuum membrane distillation
VIP	vapor induced phase separation
XRD	X-ray diffraction

LIST OF SYMBOLS

a	Air
A	Membrane area (m^2)
α_a, α_w	Collision water for air and water vapor
b	Bulk
δ, b	Thickness of membrane (m)
C_F	Initial COD in the feed (mg/L)
d	Mean pore size or nominal pore diameter (m)
d_m	Membrane thickness (m)
ε	Membrane porosity (%)
f_s & f_v	Area fractions of the solid and vapor (m^2)
F	Feed-side
H_g	Enthalpy of vapor (Jkg^{-1})
ΔH_v	Enthalpy of vaporization of water (Jkg^{-1})
ΔH_{LV}	Latent heat of vaporization (J/kg)
h_f	Feed-side heat transfer coefficient ($Wm^{-2} K^{-1}$)
h_m	Membrane heat transfer coefficient ($Wm^{-2} K^{-1}$)
h_p	Permeate-side heat transfer coefficient ($Wm^{-2} K^{-1}$)
J	Mass flux of water vapor across the membrane ($kgm^{-2} s^{-1}$)
ΔJ	Average mass flux of water vapor across the membrane ($kgm^{-2} s^{-1}$)
K_n	Knudsen number
K_B	Boltzman constant
k	Combined thermal conductivity of membrane ($Wm^{-1} K^{-1}$)
k_f, k_p	Thermal conductivity feed and permeate ($Wm^{-1} K^{-1}$)
λ, K_m	Thermal conductivity of membrane material ($Wm^{-1} K^{-1}$)
l	Mean free path of molecule

M_{tank}	COD in the permeate solution tank (mg/L)
m	Membrane-solution interface
m_p	Mass of the dry membrane
m_n	Mass of the absorbed butanol
M_i	Mass flow rate of stream (kg s^{-1})
M_i	Molar mass of species (kg kmol^{-1})
n	Molecular concentration (m^{-3})
N_i	Molar flux of species ($\text{kmolm}^{-2} \text{s}^{-1}$)
Nu	Nusselt numbers
σ_i	Molecular diameter of species (m)
Θ_c	Intrinsic contact angle ($^\circ$)
Θ_{CB}	Apparent contact angle ($^\circ$)
Θ	Contact angle ($^\circ$)
P	Bulk pressure in membrane pores (Pa)
P	Permeate-side
P_i	Partial vapor pressure of species (Pa)
Pr	Prandtl number
ρ_p	Density of the PVDF (1.78 g/cm^3)
ρ_n	Density of butanol (0.81 g/cm^3)
ΔQ	Average heat flux across the membrane (Wm^{-2})
Q	Heat flux across the membrane (Wm^{-2})
Q_c	Heat rejected to environment (W)
Q_1	Heat flux from feed (W)
Q_2	Heat flux from permeate (W)
Re	Reynolds number
R_{sw}	Rejection of synthetic nutrient water (%)
R_{rej}	Rejection ratio (%)

\dot{S}_{gen}	Rate of entropy generation (WK^{-1})
Sc	Schmidt number
Sh	Sherwood number
T	Mean Temperature ($^{\circ}\text{C}$ or K)
T_{H}	Hot temperature, temperature of heater or heat source (K)
T_{c}	Cold temperature, temperature of cooler or heat sink, temperature of environment (K)
τ	Membrane tortuosity
ΔT_{min}	Minimum approach temperature in the heat exchanger ($^{\circ}\text{C}$ or K)
Δt	Sampling time (h)
T_1, T_p	Temperature at membrane surface hot side (K)
T_2, T_f	Temperature at membrane surface permeate side (K)
V_{tank}	Volume of permeate reservoir (m^3)
w	Water vapor
\hat{W}_{in}	Work input (W)
ΔW	Quantity of distillate (L)

**SINTESIS MEMBRAN TiO₂-PVDF DENGAN SIFAT RINTANGAN
PEMBASAHAN TAMBAHAN UNTUK APLIKASI MEMBRAN
PENYULINGAN**

ABSTRAK

Membran penyulingan (MD) merupakan teknologi yang penting di dalam industri seperti penyulingan air laut dan rawatan sisa air kerana membran penyulingan memerlukan tenaga yang lebih rendah dan secara teorinya berkecenderungan pengotoran yang rendah. Bagi mengelakkan berlakunya pembasahan membran, kaedah rendaman dua kali diperkenalkan bagi menyesuaikan morfologi membran untuk meningkatkan keliangan, kekasaran permukaan serta kristalisasi polimer. Hidrofobisiti membran boleh ditingkatkan dengan menambah kekasaran permukaan membran melalui penambahan zarah bersaiz nano TiO₂. Namun begitu, penambahan TiO₂ pada membran mengurangkan keliangan disebabkan oleh penyekatan liang dan juga merendahkan hidrofobisiti akibat kehadiran kumpulan hidroksil. Masalah penghalang liang boleh diatasi dengan meminimumkan saiz zarah melalui penggunaan bahan kimia iaitu asid pada membran. Akan tetapi, sifat hidrofilik intrinsik TiO₂ yang berterusan yang menyebabkan masalah pembasahan yang tidak diingini. Dengan mengurangkan saiz liang, sifat-sifat antibakteria pada membran terhadap *E.Coli* dapat ditingkatkan di mana masalah penyumbatan oleh bakteria pada membran dapat dikurangkan dengan menambahkan asid pengubah suai membran TiO₂/PVDF. Bagi meningkatkan hidrofobisiti membran, TiO₂ dirawat dengan fluorsilan yang diubahsuai di bawah keadaan asid, neutral dan alkali. TiO₂ yang dirawat silan pada pH 7 meningkatkan sudut sentuhan (131.7 ± 4), peningkatan

penyerapan fluks ($12\text{kg/m}^2\cdot\text{h}$), nilai LEPw yang tinggi, pengurangan nutrien sehingga 99.65%, dan saiz liang yang lebih kecil yang dapat mengurangkan kemungkinan pembasahan liang. Membran yang paling optimum ini diuji dengan sisa air yang mempunyai kandungan pepejal yang tinggi iaitu sisa air dari kilang kertas SBR (PMSE) dan air sisa dari kilang minyak kelapa sawit (POME) selama 7 jam. Nilai fluks stabil sekitar $6\text{ kg/m}^2\cdot\text{h}$ untuk air sisa dari kilang kertas SBR (PMSE) boleh dicapai dan menunjukkan pembasahan membran dan rintangan penyumbatan adalah baik. Kecekapan sistem adalah sekitar 55% boleh dibandingkan dengan proses air tulen (50%). Walaubagaimanapun, membran tersebut tidak sesuai digunakan untuk merawat sisa air dari kilang minyak kelapa sawit yang kaya dengan minyak kerana fluks telah menurun dari 6 hingga $2\text{ kg/m}^2\cdot\text{h}$ selepas 7 jam beroperasi. Didapati bahawa sisa air dari kilang minyak kelapa sawit memberikan kecekapan terma terendah iaitu 26% berbanding dengan proses-proses lain kerana gejala pengotoran.

SYNTHESIS OF TiO₂-PVDF MEMBRANE WITH ENHANCED WETTING RESISTANCE FOR MEMBRANE DISTILLATION APPLICATION

ABSTRACT

Membrane distillation (MD) has emerged as an important technology for applications in industries such as seawater desalination and wastewater treatment due to lower energy requirement and theoretically low fouling propensity. However, the main obstacle to obtain high separating efficiency in MD lies on the availability of porous hydrophobic membrane that can withstand pore wetting and membrane fouling. A dual coagulation bath method was introduced to fine tune the membrane morphology to increase its porosity, surface roughness as well as polymer crystallinity. To increase the membrane hydrophobicity, membrane roughness was induced by adding TiO₂ nanoparticles. However, this brought concomitant impacts on lower porosity due to the pore blocking and it also reduces hydrophobicity due to availability of hydroxyl group. The pore blocking problem can be solved by minimizing the particle size via surface acid modification. Nonetheless, the intrinsically hydrophilic nature of TiO₂ still persist which brings unwanted wetting problem. By decreasing the particle size, it was interesting to note that the antibacterial properties on membrane towards *E.Coli* also improved, which means that the membrane bio-fouling problem can be mitigated by incorporating acid modified TiO₂/PVDF membrane. To further enhance the hydrophobicity of the membrane, TiO₂ was treated with fluoro-silane which was modified under acid, neutral and alkaline conditions. Silanized TiO₂ with pH 7 gave higher contact angle