## DEVELOPMENT AND ANALYSIS OF HYDROTALCITE-MODIFIED POROUS MEMBRANES FOR CARBON DIOXIDE SEPARATION

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by

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## LIST OF SYMBOLS

## Symbol Description

## Unit

| Α                | Surface area   | $m^2$                    |
|------------------|--|--------------------------|
| А                | Factor code of pressure difference                   | -                        |
| В                | Factor code of temperature                           | -                        |
| С                | Factor code of CO <sub>2</sub> feed concentration    | -                        |
| $D_s$            | Surface diffusivity                                  | cm <sup>2</sup> /s       |
| F                | Mole flow rate                                       | mol/s                    |
| f                | Amount of adsorbed gases on the membrane surface     | cm <sup>3</sup> /g       |
| $\Delta H_{ads}$ | Heat of adsorption                                   | kJ/mol                   |
| Κ                | Gas permeance  | mol/m <sup>2</sup> .s.Pa |
| L                | Length of the cylindrical pore                       | cm                       |
| М                | Molecular weight                                     | g/gmol                   |
| Ν                | Mole flux  | mol/m <sup>2</sup> .s    |
| $\overline{P}$   | Average feed pressure                                | Pa                       |
| $P_H$            | Pressure in feed side                                | Pa                       |
| $P_L$            | Pressure in permeate side                            | Pa                       |
| $\Delta P$       | Pressure difference                                  | Pa                       |
| q                | Volumetric flow rate                                 | cm <sup>3</sup> /s       |
| R                | Radius of the cylindrical pore                       | cm                       |
| R                | Gas constant   | J/mol.K                  |
| $R^2$            | Regression coefficient                               | -                        |
| $r_g$            | Gas kinetic radius                                   | cm                       |
| Гp               | Pore radius  | cm                       |
| t                | Actual flow path of gas molecule through the         | cm                       |
|                  | membrane   |                          |
| Т                | Temperature  | °C or K                  |
| $t_m$            | Membrane thickness                                   | cm                       |
| x                | Mole fraction of gas species in the retentate stream | -                        |

| У  | Mole fraction of gas species in the permeate stream | - |
|----|---|---|
| Z. | Compressibility factor                              | - |

### Greek letters

| α | Selectivity            | - |
|---|------------------------|---|
| β | Regression coefficient | - |
| 3 | Membrane porosity      | - |
| μ | Gas viscosity          | - |
| τ | Membrane tortuosity    | - |

## Subscripts

| F    | Feed  | - |
|------|---|---|
| i, j | Component gas $CO_2$ , $H_2$ , $N_2$ or $H_2$ | - |
| т    | membrane                                      | - |
| р    | Permeate stream                               | - |
| R    | Retentate                                     | - |

## Superscripts

| com | composition            | - |
|-----|------------------------|---|
| mix | Mixture                | - |
| S   | Single                 | - |
| sep | Separation selectivity | - |

## LIST OF ABBREVIATION

| Symbol                                   | Description                |  |  |
|--|----------------------------|--|--|
| AA                                       | Acetic acid                |  |  |
| Al                                       | Aluminum                   |  |  |
| $Al(OC_4H_9)_3$                          | Aluminum tri-sec-butoxide  |  |  |
| Al(OH) <sub>3</sub>                      | Aluminum hydroxide         |  |  |
| Al <sub>2</sub> O <sub>3</sub>           | Alumina                    |  |  |
| $\alpha$ -Al <sub>2</sub> O <sub>3</sub> | Alpha alumina              |  |  |
| $\gamma$ -Al <sub>2</sub> O <sub>3</sub> | Gamma alumina              |  |  |
| ANOVA                                    | Analysis of variance       |  |  |
| Ar                                       | Argon                      |  |  |
| ATB                                      | Aluminum tri-sec-butoxide  |  |  |
| BET                                      | Brunauer-Emmett-Teller     |  |  |
| BIH                                      | Barret-Joyner-Halenda      |  |  |
| BRB                                      | Back pressure regulater    |  |  |
| CCD                                      | Central composite design   |  |  |
| CMS                                      | Carbon molecular sieve     |  |  |
| CV                                       | Check valve                |  |  |
| CVD                                      | Chemical vapor deposition  |  |  |
| Dev                                      | Standard Deviation         |  |  |
| DF                                       | Degree of Freedom          |  |  |
| DI                                       | Deionized                  |  |  |
| DoE                                      | Design of experiment       |  |  |
| DTG                                      | Thermogravimetric Analysis |  |  |

| EDX              | Energy dispersive X-ray          |
|------------------|----------------------------------|
| ER               | Eksperimen rekabentuk            |
| EtOH             | Ethanol                          |
| FTIR             | Fourier transform infrared       |
| GC               | Gas chromatography               |
| GHG              | Greenhouse gases                 |
| KBr              | Potassium bromide                |
| LDH              | Layered double hydroxide         |
| MEA              | Monoethanolamine                 |
| MFC              | Mass flow controller             |
| MPR              | Metodologi permukaan respon      |
| NV               | Needle valve                     |
| O <sub>3</sub>   | Ozone                            |
| PG               | Pressure gauge                   |
| "Prob>F"         | Probability                      |
| PSA              | Pressure swing adsorption        |
| PVA              | Polyvinyl alcohol                |
| RSM              | Response surface methodology     |
| SEM              | Scanning Electron Microscopy     |
| SiO <sub>2</sub> | Silicon dioxide                  |
| TEOS             | Tetraethylorthosilicate          |
| TGA              | Temperature Gravimetric Analysis |
| TiO <sub>2</sub> | Titanium dioxide                 |
| TSA              | Temperature swing adsorption     |

- TWV Three way valve
- XRD X-ray differaction
- ZrO<sub>2</sub> Zirconium dioxide

## PEMBANGUNAN DAN ANALISIS HIDROTAISIT-MEMBRAN-MEMBRAN BERLIANG TERUBAHSUAI UNTUK PEMISAHAN KARBON DIOKSIDA

#### ABSTRAK

Pembebasan karbon dioksida (CO<sub>2</sub>) telah menjadi salah satu daripada masalah persekitaran yang paling serius semenjak revolusi perindustrian. Hari ini, pengurangan pelepasan CO<sub>2</sub> dianggap amat penting demi mengelak perubahan iklim global dan pemanasan global. Untuk ini, pemisahan CO<sub>2</sub> daripada campuran gas sedang giat dilaksanakan. Objektif utama penyelidikan ini ialah pemisahan  $CO_2$ daripada aliran gas sintetik yang terdiri daripada campuran gas binari dengan menggunakan teknologi membran tak-organik. Penyelidikan difokuskan kepada sintesis dan pembangunan membran tak-organik berliang yang terubahsuai dengan hidrotalsit bagi membantu pemisahan CO<sub>2</sub>. Bahan hidrotalsit telah digabung bagi memperbaiki afiniti CO<sub>2</sub> dan penstabilan terma membran tak-organik untuk permisahan gas  $CO_2$ . Membran berliang meso HT-alumina (~10 µm) yang bebas daripada rekahan dan berliang mikro HT-silika (~200 nm) telah berjaya disintesis di atas lapisan  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> yang disokong oleh penyokong cakera  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> menggunakan teknik sol-gel dan balut-rendam. Kesan pembolehubah ke atas prestasi membran, struktur dan kaitan ciri telapan dan mekanisma pengangkutan dipelajari dengan cara mengubah komposisi hidrotalsit dan suhu penyinteran. Membran yang tidak disokong diciri untuk mengetahui kehadiran HT, kumpulan berfungsi permukaan, topografi permukaan dan morfologi, kawasan permukaan, saiz liang, penjerapan CO<sub>2</sub> dan kapasiti penyah-jerapan.

Pencirian ini dilakukan dengan menggunakan kaedah penyerakan sinar-x (XRD), FTIR, SEM, EDX, BET, TGA. Pengubahsuaian membran berliang dengan

HT meningkatkan prestasi pemisahan CO<sub>2</sub>. Membran komposit HT-silika yang mengandungi 15 isipadu% HT dan disinter pada suhu 500 °C memberikan peningkatan tertinggi dalam kepilihan telapan CO2/CH4, CO2/N2 dan CO2/H2 masing-masing 42.65, 37.78 dan 6.34, dengan penelapan  $CO_2$  tertinggi sebanyak 4.8×10<sup>-7</sup> mol.m<sup>-2</sup>.s<sup>-1</sup>.Pa<sup>-1</sup> berbanding membran HT-alumina di dalam kajian penelapan gas tulen. Membran komposit HT-silika yang mengandungi 15 isipadu % HT diuji untuk kajian penyerapan gas tulen CO<sub>2</sub>, H<sub>2</sub>, N<sub>2</sub> dan CH<sub>4</sub> pada suhu operasi berlainan dan perbezaan tekanan. Penelapan gas campuran dan pemisahan CO<sub>2</sub>/CH<sub>4</sub>, CO<sub>2</sub>/N<sub>2</sub> dan CO<sub>2</sub>/H<sub>2</sub> juga dikaji disekitar suhu (30-190°C), perbezaan tekanan (100-500 kPa) dan kepekatan suapan CO<sub>2</sub> (10-50 %). Membran komposit HT-silika yang mengandungi 15 isipadu % HT memberikan peningkatan tertinggi kepemilihan dalam CO<sub>2</sub>/CH<sub>4</sub>, CO<sub>2</sub>/N<sub>2</sub> dan CO<sub>2</sub>/H<sub>2</sub> masing-masing sebanyak 104.4, 68.2 and 9.3, berbanding kepilihan telapan. Eksperimen rekabentuk (ER) telah digunapakai untuk mengoptimumkan dan membangunkan model impirikal bagi penelapan CO<sub>2</sub> kajian kepemilihan campuran gas CO<sub>2</sub>/CH<sub>4</sub>, CO<sub>2</sub>/N<sub>2</sub> dan CO<sub>2</sub>/H<sub>2</sub> pada julat suhu (30-190°C), perbezaan tekanan (100-500 kPa) dan kepekatan suapan CO<sub>2</sub> (10-50 %). Perisian ER dengan metodologi permukaan respon (MPR) memberikan persamaan impirikal dengan keboleh-ramalan yang baik dan keboleh-percayaan yang cukup bagi pemodelan dan ramalan prestasi membran HT-silika.

## DEVELOPMENT AND ANALYSIS OF HYDROTALCITE-MODIFIED POROUS MEMBRANES FOR CARBON DIOXIDE SEPARATION

#### ABSTRACT

The emission of carbon dioxide  $(CO_2)$  has become one of the most serious environmental problems since the industrial revolution. Today, reducing CO<sub>2</sub> emissions is considered extremely important in order to abate the global climate change and global warming. For this purpose, CO<sub>2</sub> separations from gas mixtures have been actively researched. The main objective of this research is to separate  $CO_2$ from the synthetically produced gas stream containing binary gas mixtures using inorganic membrane technology. The research focused on the synthesis and development of different porous inorganic membranes modified with hydrotalcite (HT) to facilitate the separation of  $CO_2$ . Hydrotalcite material was incorporated to improve the CO<sub>2</sub> affinity and the thermal stability of the inorganic membranes for  $CO_2$  gas separation. The crack free mesoporous HT-alumina (~10 µm) and microporous HT-silica (~200 nm) porous membranes were successfully synthesized on top of  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> layer supported by a  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> disc support using the sol-gel and dip-coating techniques. The effect of different parameters on the membrane performance, the structure and permeation properties relationships and the transport mechanism were studied by varying hydrotalcite compositions and sintering temperatures. The unsupported membranes were characterized for the presence of HT, surface functional groups, surface topography and morphology, surface area, pore size, CO<sub>2</sub> adsorption and desorption capacity.

These characterizations were done using X-ray diffraction (XRD), Fourier Transform Infrared (FTIR) spectrometry, scanning electron microscopy (SEM), Energy-Dispersive X-ray spectroscope, Brunauer-Emmett-Teller method (BET) and Thermo gravimetric analyzer (TGA) techniques. The modification of porous membranes with HT enhanced CO<sub>2</sub> separation performance. The HT-silica composite membrane containing 15 vol.% HT and sintering temperature of 500 °C gave the highest increase in  $CO_2/CH_4$ ,  $CO_2/N_2$  and  $CO_2/H_2$  permselectivity of 42.65, 37.78 and 6.34, respectively, with the highest  $CO_2$  permeance of  $4.8 \times 10^{-7}$ mol.m<sup>-2</sup>.s<sup>-1</sup>.Pa<sup>-1</sup> compared to HT-alumina membranes in preliminary pure gas permeation studies. The HT-silica composite membrane containing 15 vol.% HT was tested for pure gas permeation studies of CO<sub>2</sub>, H<sub>2</sub>, N<sub>2</sub> and CH<sub>4</sub> at different operating temperatures and pressure differences. The mixed gas permeation and separation of CO<sub>2</sub>/CH<sub>4</sub>, CO<sub>2</sub>/N<sub>2</sub> and CO<sub>2</sub>/H<sub>2</sub> was also studied for wide range of temperature (30-190°C), pressure difference (100-500 kPa) and CO<sub>2</sub> feed concentration (10-50 %). The HT-silica composite membrane containing 15 vol.% HT provided the highest increase in CO<sub>2</sub>/CH<sub>4</sub>, CO<sub>2</sub>/N<sub>2</sub> and CO<sub>2</sub>/H<sub>2</sub> separation selectivity of 104.4, 68.2 and 9.3, respectively, compared to permselectivity. The design of experiments (DoE) was used to optimize and build up an empirical model for the CO<sub>2</sub> permeance and separation selectivity studies of CO<sub>2</sub>/CH<sub>4</sub>, CO<sub>2</sub>/N<sub>2</sub> and CO<sub>2</sub>/H<sub>2</sub> mixed gases at wide range of temperature (30-190°C), pressure difference (100-500 kPa) and CO<sub>2</sub> feed concentration (10-50 %). The DoE software with response surface methodology (RSM) produced empirical equations with good predictability and sufficient reliability for the modeling and predicting the HT-silica membrane performance.

#### CHAPTER 1

#### **INTRODUCTION**

#### 1.1 Global issues of carbon dioxide as greenhouse gas

Several greenhouse gases (GHG) exist in the earth's atmosphere such as carbon dioxide ( $CO_2$ ), water vapor ( $H_2O$ ), methane ( $CH_4$ ), nitrous oxide ( $N_2O$ ) and ozone (O<sub>3</sub>) (Mondal et al., 2012). These gases allow direct sunlight (relative shortwave energy) to enter the atmosphere and reach the earth's surface unimpeded. When the shortwave energy strikes the earth's surface, some of it (longer-wave (infrared) energy) is reradiated back towards the atmosphere as infrared radiation (heat). Greenhouse gases absorb this infrared radiation and trap the heat in the lower atmosphere (Carpenter et al., 2013). GHG results in an increase of the average earth temperature above what it would be in the absence these gases (Rohde et al., 2012). The rise in the average earth temperature may, in turn, leads to change of the weather, rising sea levels due to melting of iceberg at the pole, changes in ecosystems, loss of biodiversity and reduction of crop yield, usually referred to as "climate change" (Houghton et al., 2001; Hunter et al., 2013). The anthropogenic carbon dioxide has been known to cause irreversible change in ocean chemistry that could endanger marine life populations on a huge scale (Pires et al., 2011; Crim et al., 2011). In addition, increasing GHG concentrations affect the composition of the atmosphere and lead to the depletion of the stratospheric ozone layer.

The first measurements made in the second half of the twentieth century show that  $CO_2$  concentration in atmosphere had increased. The concentrations of  $CO_2$  in the atmosphere were only slightly changed before the industrial revolution from 280 ppmv in 1000 to 295 ppmv in 1900 based on antarctica ice core data. It increased to 315 ppmv in 1958 and further to 377 ppmv in 2004 based on actual data logged in Hawaii (Yang *et al.*, 2008; Humlum *et al.*, 2013). At present, there are around 390.5 ppmv (Humlum *et al.*, 2013), an increase of over 39 percent. International Panel on Climate Change (IPCC) forecasts that, the concentration of  $CO_2$  in the atmosphere may go up to reach 570 ppmv by the year 2100, causing a rise of average earth temperature of around 1.9°C and an increase in mean sea level of 38 cm (Stewart and Hessami, 2005). The ever increasing anthropogenic  $CO_2$  emissions (i.e., emissions produced by human activities) since the beginning of the industrial age, has been due to the burning of huge amounts of fossil fuels, such as coal or natural gas to produce electricity, and petroleum or diesel for transportation. Hence,  $CO_2$  is of utmost concern compared to other GHGs, and its emission has always been the subject of interest in research discussion about global issues.

Several options can be applied to reduce  $CO_2$  emissions from fossil fuel such as improving the efficiency of fossil fuel combustion, replacing of fossil fuel with renewable one and sequestrating of  $CO_2$  from its large emission sources. Separation and capture of  $CO_2$  from its emission sources are promising options but they remained as great challenges due to some technological and political issues (Mondal *et al.*, 2012). In industrial settings, the separation of  $CO_2$  is an essential step in many industrial processing such as the natural gas purification. The final natural gas used as fuel in the industry or vehicles is consists almost entirely of methane. Removal of  $CO_2$  increases the calorific capacity, yields better transportation conditions and prevents pipeline corrosions. Carbon dioxide content in the natural gas obtained from gas or oil well can vary from 4 to 50% (Datta and Sen, 2006). On the other hand, purged gas from a gas-reinjected EOR (enhanced oil recovery) well can contain as much as 90% carbon dioxide. Before a natural gas rich in carbon dioxide can be transported, it must be pre-processed so as to meet the typical specification of 2–5% carbon dioxide (Datta and Sen, 2006).

#### **1.2** Conventional technologies for CO<sub>2</sub> separation and capture

Several conventional technologies are available for separation and capture of  $CO_2$  such as; cryogenic distillation, absorption using liquid solvents and pressuretemperature swing adsorption using various solid sorbents. Cryogenic distillation technology has been used for decades for  $CO_2$  removal on the basis of fractional condensation and distillation at low temperature. This technology is a commercial process to produce a large volume of  $CO_2$  with high purity from streams that already have relatively high  $CO_2$  concentrations (>90 %). However, the cost of this technology is very high due to the requirement of extremely low temperature (lower than -73°C for liquefaction of  $CO_2$ ) and high pressure (Leo *et al.*, 2009; Burt *et al.*, 2009; Olajire, 2010), which leads to high cost.

The absorption process is the commercial technology used for  $CO_2$  separation and capture for more than few decades. Absorption of  $CO_2$  can be either physical or chemical process. In a chemical absorption process,  $CO_2$  is chemically captured from gaseous streams through acid-base neutralization reactions using basic solvents such as monoethanolamine (MEA) to form a weakly bonded intermediate compound. The  $CO_2$ -rich solution is pumped to a stripper column for thermal regeneration where the  $CO_2$  is stripped from the solution and the original solvent pumped back for a new cyclic use. The pure  $CO_2$  released from the stripper

is compressed for the subsequent transportation and storage (Yu et al., 2012). High CO<sub>2</sub> recovery rate is about 98% can be achieved with MEA solutions due to fast kinetics and strong chemical reaction (Yang et al., 2008). However, there are many drawbacks of using liquid solvent absorption such as flow problems (flooding and loading) caused by viscosity increases with fast-reacting solvent, equipment corrosion, and high energy consumption for solvent regeneration (Zheng et al., 2005; Gray et al., 2005). For physical absorption process, CO<sub>2</sub> is selectively absorbed in a solvent according to Henry's Law, which means that they are temperature and pressure dependent. Higher CO<sub>2</sub> partial pressure and lower temperature favor the solubility of  $CO_2$  in the solvents. Different physical solvents for CO<sub>2</sub> absorption are commercially available such as dimethylether of polyethylene glycol (Selexol process), propylene carbonate (FLUOR process), cold methanol (Rectisol process) and ionic liquid. Lower energy is required for solvents regeneration due to the weakly interacting between CO<sub>2</sub> and the solvent compared to that of chemical solvents. However, physical absorption has drawbacks due to high capital cost of constructing Selexol and FLUOR plants. In addition, the high viscosity of ionic liquid limits the mass transfer and hence low absorption rates (Olajire, 2010; Yu et al., 2012).

Adsorption is another well-established technology for  $CO_2$  separation and capture. Various regenerable solid sorbents are often used such as activated carbons, metal oxide, hydrotalcite, zeolites, mesoporous silica functionalized with amines and activated alumina.  $CO_2$  molecules are attracted and trapped by the solid sorbents through physisorptions (van der Waals) or chemisorptions (covalent bonding), followed by regeneration (desorption) of the solid sorbents which can be achieved either by increasing the temperature (Temperature Swing Adsorption, or TSA), or by reducing pressure (Pressure-Swing Adsorption, or PSA) (Olajire, 2010). Physical adsorbents based on carbons and zeolites can adsorb large amounts of CO<sub>2</sub> at room temperature (Hao *et al.*, 2013; Cheung *et al.*, 2013). The rate-limiting step in the adsorption is the diffusion of CO<sub>2</sub> from gas mixture to the inside pore of the adsorbent which is three times higher than the magnitude of CO<sub>2</sub> transfer across the gas-liquid interface in aqueous amine absorption (Khatri *et al.*, 2005). However, these physical adsorbents have many disadvantages due to reduced CO<sub>2</sub> adsorption capacity at high temperature (Zheng *et al.*, 2005; Gray *et al.*, 2005), high temperature requirement for regeneration, poor tolerance to water (Franchi *et al.*, 2005) and unsuitable for high CO<sub>2</sub> concentration streams (> 3%) since it needs frequent regeneration of solid bed.

#### **1.3** Membrane technology for CO<sub>2</sub> separation

Membrane technology is a novel method to facilitate  $CO_2$  separation from a gas mixture. Membranes act as filters that enable continuous separation of one or more gases from a feed mixture based on the differences in physical properties of the gases and/or chemical interplays between the membrane material and the gas (Olajire, 2010). The separation of  $CO_2$  using membrane technologies provides many advantages over the other conventional separation technologies (Zhang *et al.*, 2013). First, the membrane process is a viable energy-saving alternative for  $CO_2$  separation, since it does not require any phase transformation. Second, the necessary process equipment is very simple with no moving parts, compact, relatively easy to operate and control, and also easy to scale-up (Ismail *et al.*, 2009; Zhang *et al.*, 2013). Membrane materials are classified into organic (polymeric) and inorganic (carbon, zeolite, ceramic or metallic) which can be porous or dense.

There have been several studies of polymeric membranes for gas separation due to its low energy cost, ease in fabrication and scalability (Ismail et al., 2009; Basu et al., 2010). Polymeric membranes can be categorized into two groups; rubbery or glassy; based on operating temperature relative to the glass transition; Rubbery membranes can be operated above the glass transition temperature (Approximate midpoint of the temperature range over which a material undergoes a phase change from brittle to rubbery), while glassy membranes operate below the glass transition temperature (Olajire, 2010; Adewole et al., 2013). However, the loss in permeance stability of polymer membranes at high temperature, high pressure, and highly acidic or alkaline environment has limited its application (Koros and Mahajan, 2000). Furthermore, polymeric membranes show inverse behavior for the permeability/selectivity; in other words, the gas selectivity decreases as the gas permeability through the membrane increases (Zhang et al., 2013). It has been reported that presence of CO<sub>2</sub> even in low concentration induces plasticization problem in polymeric membrane, specially the glassy polymers, due to its condensability at certain pressures. It is supposed that a plasticization phenomenon happens when the polymer matrix absorbs  $CO_2$  present in the feed to an extent that it increases the free volume of the polymer matrix. The swelling of polymer matrix during the absorption of CO<sub>2</sub> enhances the permanent enlargement of interchain spacing in the polymer matrix, which in turn, increases the permeability of gas and decreases the separation performance (Pandey et al., 2002; Baker, 2002; Basu et al., 2010).

Inorganic membranes are gaining intense research efforts for use in CO<sub>2</sub> separation that are difficult to achieve by polymeric membranes with respect to their higher thermal, chemical and mechanical stability (Yeo et al., 2012). Inorganic membranes can be categorized based on their physical structures; either dense or porous. Dense inorganic membranes such as palladium and perovskite are usually used in selective separation of hydrogen and oxygen, respectively (Schiestel et al., 2005; Burkhanov et al., 2011). Porous inorganic membranes are generally consist of a porous thin top layer supported on a porous metal or ceramic support which provides mechanical strength to the system and offers minimum mass-transfer resistance. Porous inorganic membranes that are mainly used include alumina, titania, zerconia, hydrotalcite, silicon carbide, glass, amorphous silica, carbon and zeolites (De Vos and Verweij, 1998; Shekhawat et al., 2003; Kim et al., 2009b; Yeo et al., 2012). These membranes vary in properties such as pore size, surface area, thermal and chemical stability. The porous inorganic membrane can be categorized based on their pore size into microporous (pore diameter <2 nm), mesoporous (2 nm > pore diameter <50 nm) and macroporous (pore diameter >50 nm) (Shekhawat et al., 2003). The microporous inorganic membranes consists essentially of either amorphous silica, carbon molecular sieve or zeolites (Yeo et al., 2012).

Carbon molecular sieve (CMS) membranes are typically prepared through carbonization (at high temperature in an inert atmosphere) of polymeric precursors already processed in the form of membranes (Sim *et al.*, 2013). In spite of higher production cost of CMS membranes which is greater than polymeric membranes by 1 to 3 orders of magnitude per unit area, they provide higher permeance and separation factor compare to polymeric membranes. However, the major disadvantage of CMS membranes that hinder their commercialization is their brittleness (Brunetti *et al.*, 2010). The zeolite materials are aluminosilicates with uniform pore structures. Zeolite membranes are usually prepared by in-situ hydrothermal synthesis on porous stainless steel,  $\alpha$ -alumina, or  $\gamma$ -alumina support tubes or disks for the gas permeation studies (Yang *et al.*, 2008). Despite the success of zeolite membranes in the separation of CO<sub>2</sub> from different gaseous systems, they have two main disadvantages: Firstly, high cost and difficult to produce; Secondly, low gas permeability compared to other inorganic membranes. This is due to the fact that relatively thick zeolite layers are necessary to get a pinhole-free and crack-free zeolite layer (De Beer, 2000).

Mixed matrix membranes (MMMs) are a well-known solution to improve the thermal and mechanical properties of polymeric membranes. MMMS are formed by homogenous incorporation of an inorganic material in the form of micro- or nano-particles (discrete phase) into a polymeric matrix (continuous phase). The combination of the two different materials provides high selectivity of inorganic phase and low cost of polymer phase that give better design for CO<sub>2</sub>-selective membrane. However, the performance of MMMs suffers from defects caused by poor interaction at the molecular sieves/polymer interface which forms non-selective void spaces. Additionally, MMMs encounter plasticization problem caused by CO<sub>2</sub> adsorption (Yang *et al.*, 2008; Ismail *et al.*, 2009; Brunetti *et al.*, 2010).

#### **1.4** Hydrotalcite compound for CO<sub>2</sub> separation

Hydrotalcite (HT) is a class of anionic clays called layered double hydroxide (LDH) or hydrotalcite-like compounds. The general chemical formula of hydrotalcite

is  $[M_{1-x}^{2+}M_x^{3+}(OH)_2](A^{n-})_{x/n}$  .mH<sub>2</sub>O], where M<sup>2+</sup> the divalent cation (e.g., Mg<sup>2+</sup>,  $Ni^{2+}$ ,  $Co^{2+}$ ,  $Zn^{2+}$ ,  $Cu^{2+}$ );  $M^{3+}$  is the trivalent cation (e.g.,  $Al^{3+}$ ,  $Fe^{3+}$ ,  $Cr^{3+}$ );  $A^{n-}$  is the anion (e.g.,  $CO_3^{2^-}$ ,  $SO_4^{2^-}$ ,  $NO_3^-$ ,  $CI^-$ ) and x is the ratio of  $(M^{3^+}/M^{2^+} + M^{3^+})$  with values range from 0.2 to 0.33. These materials exist with positively charged layers of brucite  $[Mg(OH)_2]$ , and aluminum hydroxide  $[Al(OH)_3]$ , which are balanced by anions and water molecules in the interlayer region as shown in Figure 1.1 (Reichle, 1985; Cavani et al., 1991; Salomão et al., 2011). HT compounds have attracted much attention worldwide since they find a wide range of applications. Various important applications include catalysis in dehydrochlorination and recovery of hydrochloric acid (Kameda et al., 2007) and decomposition of urea (Vial et al., 2006). HT has already found use in pharmaceutical industries as a drug carrier (Lee and Chen, 2006). HT can also be applied in the purification of wastewater as sorbent to remove phosphates or heavy metals (Li et al., 2009). In particular, HT has been intensively investigated in recent years as adsorbents for CO<sub>2</sub> at high temperature to reduce the greenhouse emission into atmosphere. HT has adequate mechanical strength when it is exposed to high pressure, it exhibits high capacity and selectivity to adsorb CO<sub>2</sub> at high temperature, adequate CO<sub>2</sub> adsorption/desorption kinetics for CO<sub>2</sub> at operating after conditions, and stable adsorption capacity of  $CO_2$ repeated adsorption/desorption cycles (Yong et al., 2002). The CO<sub>2</sub> adsorption capacity of HT is influenced by many factors such as aluminum content, anion type, water content as well as the heat treatment temperature. The effect of these factors on CO<sub>2</sub> adsorption at high temperatures was investigated on several commercially supplied HTs at higher temperatures (300 °C). Their results revealed that the capacity for CO<sub>2</sub> increases when the amount of aluminum was decreased and that there is an optimum aluminum content in the HTs for adsorption of CO<sub>2</sub>. The presence of small amount of

water in the HTs also favors the adsorption capacity. Similarly, under dry and wet feed condition, the capacity for the wet feed conditions was found to be approximately 10% higher than for the dry feed condition. Adsorption capacities of HTs having  $CO_3^{2-}$  and OH anion reveal that the HTs containing  $CO_3^{2-}$  show higher adsorption capacities than those containing OH<sup>-</sup> (Baba *et al.*, 2010). However, researches on the fabrication of HT material as a  $CO_2$  selective membrane has been rarely conducted (Othman, 2009; Kim *et al.*, 2009a).



Figure 1.1: Schematic representation of the HT structure (Salomão et al., 2011)

#### **1.5 Problem statement**

The inorganic membrane has been widely studied for preparation and modification of  $CO_2$ -selective membranes because of its high resistance against heat and chemicals (Yeo *et al.*, 2012). However, the attempt to prepare uniform and thin inorganic membrane is a very challenging work. Many factors affect the production of high quality inorganic membrane. These include: the right choice of synthesis method and suitability of preparation conditions. The most important features of the

good CO<sub>2</sub>-selective membrane are high CO<sub>2</sub> permeation flux and selectivity for CO<sub>2</sub> from the gaseous mixture. High CO<sub>2</sub> permeation flux reduces the required membrane area and high CO<sub>2</sub> separation selectivity under low driving force is important to confirm the high separation efficiency of the prepared membrane, therefore the capital separation cost will be reduced (Lu *et al.*, 2007). However, the membrane performances have to balance between CO<sub>2</sub> permeation flux and CO<sub>2</sub> separation selectivity. Generally, the increasing membrane thickness decreases the gas permeation flux, but at the same time increases the gas separation selectivity. The synthesis of a defect free and thin membrane layer is desirable for both high gas separation selectivity and gas permeation flux. This is one of critical issue along with the challenges to prepare a membrane with the desired characteristics.

The inorganic molecular sieve membranes made from zeolite, carbon and silica currently suffer problems such as brittleness and low permeability. In this work, a molecular sieve hydrotalcite membrane is prepared and characterized for the first time in order to investigate its potential to solve some of the issues faced by the membranes described earlier. Its separation performance with the other molecular sieve membrane namely pure silica membrane is also compared. Hydrotalcites are very attractive materials for  $CO_2$  adsorption at elevated temperature in the presence of water. Therefore, in this research the fabrication of new membrane from HT material modified porous alumina and silica membranes to increase the separation selectivity of  $CO_2$  from different gaseous mixtures is a subject of this study. Modification of the internal pore surface of alumina membrane with HT increases the amount of adsorbed  $CO_2$  resulting in increase of HT-alumina is expected to

provide high gas permeation flux due to the bigger pore size of alumina (mesoporous) and adequate separation factor.

Separation of gas using membranes follows a few mechanisms. In molecular sieve mechanism, the separation is based on the kinetic diameter of the gas molecules. The gas with small kinetic diameter penetrates through the pores, whereas the larger kinetic diameter cannot pass through these pores. High gas selectivity and permeation flux for the small gas molecules in a gas mixture can be achieved from molecular sieve membranes. However, the separation selectivity and gas permeation flux can further improve the interaction between gas molecules and pore wall, resulting in an additional transport along the surface. The second mechanism called surface affinity for porous materials can also drastically decrease or eliminate the transport of weakly adsorbed molecules through the pore by reducing the size of pore mouth by the adsorbed molecules (Moon et al., 2004). Separation layers can be chemically modified in order to change the surface affinity of the membranes. In this way the pore size can be changed and/or the chemical character of the surface can be modified (Keizer et al., 1988). With smaller pore size it is expected that the gas-solid interaction and surface affinity play a bigger role than the other gas diffusion phenomena.

#### **1.6** Research objectives

This research is aimed at developing a novel porous HT membranes with molecular sieve characteristics for  $CO_2$  separation from natural gas, flue gas and fuel streams. The present research study has the following objectives:

- To develop and synthesize HT-modified porous membranes by sol-gel method at different HT vol. % and sintering temperature.
- To characterize and analyze the physical and chemical properties of HTmodified porous membrane.
- 3. To evaluate and study the performance of HT-modified porous membranes for single gas CO<sub>2</sub>, H<sub>2</sub>, N<sub>2</sub>, and CH<sub>4</sub> permeances and permselectivities over wide range of pressure differences and operating temperatures.
- 4. To study the performance of HT-modified porous membrane for  $CO_2$ permeation and separation from different binary gaseous mixtures contains  $CO_2/CH_4$ ,  $CO_2/N_2$  and  $CO_2/H_2$  over different range of operating parameters (operating temperature, pressure difference across the membrane and  $CO_2$ feed concentration).
- 5. To optimize and build up an empirical model for  $CO_2$  permeance and  $CO_2$  separation selectivity for different mixed gas mixtures contains  $CO_2/CH_4$ ,  $CO_2/N_2$  and  $CO_2/H_2$ .

#### **1.7** Research scope

This research focuses on the synthesis, development and characterization of porous membranes modified with HT as a  $CO_2$  affinity membrane. For this purpose, different HT vol. % in the composite membrane and different sintering temperatures are to be investigated carefully. The synthesized membranes are characterized in order to understand its chemical structure, surface morphology,  $CO_2$  adsorption capacity, porosity and pore size distribution. The steps outlined below leads to the accomplishment of the research objectives. These are:

# 1.7.1 Synthesis of unmodified alumina and silica membranes via sol-gel method

The alumina membrane is synthesized from sol-gel method following the documented work in (Ahmad *et al.*, 2005; Ahmad *et al.*, 2006b). In this research 2 vol.% of PVA solution containing 4 g of PVA in 100 mL of water is used as a binder, as reported previously that this ratio of binder is adequate to achieve an appropriate porosity level to avoid cracks on the gel layer. Whereas, the silica membrane is synthesized from sol-gel method following the procedures reported by (De Vos and Verweij, 1998; Peters *et al.*, 2005). The polymeric silica sol was prepared by hydrolysis and condensation of tetraethylorthosilicate (TEOS) in ethanol with nitric acid (HNO<sub>3</sub>) as catalyst. The standard molar ratios of TEOS-ethanol-water-HNO<sub>3</sub> are used.

## **1.7.2** Development of alumina and silica membranes with HT material via solgel method

HT sol was prepared from sol-gel technique by controlling hydrolysis and condensation of aluminum tri-sec butoxide and magnesium methoxide following the documented work (Valente *et al.*, 2007; Prince *et al.*, 2009). The HT-alumina membrane was prepared by mixing together the freshly prepared alumina sol with HT sol at different volume ratio followed by dip coating the support in this mixed sol. Whereas, the HT-silica membrane was prepared by mixing together the freshly prepared by mixing together the freshly prepared silica sol with HT sol at different volume ratio followed by dip coating the support in this mixed sol and sintering it at different temperature.

#### 1.7.3 Characterization of unmodified and the modified porous membranes

The synthesis membrane samples will be characterized and re-evaluated using the following equipment:

- X-ray diffraction (XRD) technique will be used to characterize the membrane internal structures and compositions of the membrane. The XRD patterns should suggest the presence of HT in the porous membrane sample.
- Fourier Transform Infrared spectrometry (FTIR) test will be used for the determination of surface functional groups. These functional groups govern the activity of the membrane.
- Brunauer-Emmett-Teller method (BET) method will be used to determine the surface area, pore size, volume and pore size distribution for the suggested membrane. These physical properties of the membrane govern the permeability and selectivity of the membrane because they indicate whether that the CO<sub>2</sub> gases can penetrate through the membrane pore or not. That permeability determines the amount of CO<sub>2</sub> that can permeate through the membrane and the separation factor from other gases.
- Thermo gravimetric analyzer (TGA) technique will be used to determine the changes in membrane weight in relation to the change in temperature. Also, TGA analysis will be used to determine the CO<sub>2</sub> adsorption and desorption of the adsorbent through the change membrane in membrane weight when CO<sub>2</sub> gas is fed instead of N<sub>2</sub>.
- Since it is of importance to characterize the surface topography and morphology of the membranes, scanning electron microscopy (SEM) will be employed for this purpose.

# 1.7.4 Study of the permeation of single gas and mixed gas mixtures using modified HT porous membrane

All the unmodified and modified membranes with HT are subjected to preliminary single gas permeations of CO<sub>2</sub>, H<sub>2</sub>, N<sub>2</sub> and CH<sub>4</sub> at 30 °C and 100 kPa. The modified HT membrane that has highest permselectivity performances of CO<sub>2</sub>/CH<sub>4</sub>, CO<sub>2</sub>/N<sub>2</sub> and CO<sub>2</sub>/H<sub>2</sub> will be selected for single gas and mixed gas permeation studies over operating temperature range 30-190 °C and pressure difference across the membrane of 100-500 kPa. In the mixed gas permeation and separation studies, three binary gas mixture were carried out CO<sub>2</sub>/CH<sub>4</sub>, CO<sub>2</sub>/N<sub>2</sub> and CO<sub>2</sub>/H<sub>2</sub> using the selected modified membrane over operating temperature of 30-190 °C and pressure difference across the membrane of 100-500 kPa and CO<sub>2</sub> feed concentration of 10-50%.

# **1.7.5** Modeling, optimization for CO<sub>2</sub> permeance and separation selectivity from mixed gas mixture and surface affinity study

Design of experiments (DoE) was chosen to optimize and find out empirical equations for  $CO_2$  permeances and separation selectivities of the three binary gas systems of  $CO_2/CH_4$   $CO_2/N_2$  and  $CO_2/H_2$  using Design Expert software version 6.0.6. The optimization of the process parameters was determined by using response surface methodology (RSM) coupled with center composite design (CCD). Whereas the statistical model equations are determined using quantitative data from the set of experimental runs.

#### **1.8** Organization of thesis

The thesis consists of five chapters and each chapter gives specific information about this research project.

**Chapter 1 (Introduction)** presents a brief introductory of this research project. This chapter starts with the global issues and the importance of the  $CO_2$  separation. This chapter also gives brief overview of the conventional and membrane technologies for  $CO_2$  separation and the definition of HT compound and its application in  $CO_2$  separation. At the end of this chapter, problem statements that provide basis and rationale to justify the research direction in the present study are elaborated. Based on the problem statement; the specific objectives of the research followed by the research scope are stated clearly in this chapter.

**Chapter 2 (Literature review)** presents literature review on the background of the present research project. This chapter provides the literature review on the modification of  $\gamma$ -alumina membrane for CO<sub>2</sub> separation, in addition to the sol-gel method for synthesis of  $\gamma$ -alumina membrane. The methods used for synthesis and modification of silica membrane for CO<sub>2</sub> gas separation are also provided. Further in this chapter are reviews on the hydrotalcite compound for CO<sub>2</sub> adsorption, the sol-gel method used for preparation of hydrotalcite and the efforts on fabrication of hydrotalcite membrane. At the end of this chapter, the gas transport mechanisms through inorganic porous membrane are discussed.

Chapter 3 (Materials and Methods) describes the detail of materials and methodology used in this research project. The first part of this chapter presents the

list of all materials and chemicals used in present research project. The subsequent topics describe clearly the experimental procedures for synthesis method of membrane support, unmodified alumina and silica membranes, modified alumina and silica membranes with HT, characterization methods and analytical techniques. At the end of this chapter, details of experimental procedures of the gas permeation and separation test in measuring the gas permeation and separation and also gas sample analysis are elaborated.

**Chapter 4** (**Results and Discussion**) presents the experimental results and discussion of the present research project. The first section of this chapter presents the characterizations of unmodified and modified porous membranes with HT. The subsequent topic presents the preliminary single gas permeations comparison between the synthesized membranes. This is followed by single gas permeation of  $CO_2$ ,  $H_2$ ,  $N_2$  and  $CH_4$  and mixed gas permeation and separation studies of three systems  $CO_2/CH_4$ ,  $CO_2/N_2$  and  $CO_2/H_2$  through the selected modified membrane with HT. In the last part of this chapter, DoE approach was discussed to optimize the operating parameters and build up empirical equations to represent  $CO_2$  permeances and separation selectivity for the three systems of  $CO_2/CH_4$ ,  $CO_2/N_2$  and  $CO_2/H_2$ .

**Chapter 5** (**Conclusions and Recommendations**) gives the conclusive attainment of all the major finding obtained in this research project. Suggestions and recommendations for future work to improve the present research work are also presented.

#### CHAPTER 2

#### LITERATURE REVIEW

This chapter provides the literature review of application of  $\gamma$ -alumina in gas separation, the methods used to enhance the surface diffusion and the synthesis fundamentals of  $\gamma$ -alumina membrane by sol-gel method. Next, various methods used in the synthesis of silica membrane for gas application are reviewed. The following section also reviews the modifications of silica membrane by doping elements to enhance its properties. Further in this chapter are reviews on the synthesis methods of hydrotalcite compounds and the synthesis of hydrotalcite membrane. Finally, literature review on the gas transport mechanisms for inorganic membranes is also provided.

#### **2.1** *γ*-alumina membranes for gas separation

Although the synthesis of mesoporous  $\gamma$ -alumina membranes stalled in the early 1980's, many valuable experimental details were revealed. These details included type of metal-organic compound, temperature of hydrolysis, amount and type of acid used as a peptizing agent, amount of binder adding to create defect free membrane and permeability of gases (Leenaars *et al.*, 1984; Leenaars and Burggraaf, 1985b; Leenaars and Burggraaf, 1985a; Othman *et al.*, 2001; Kwon *et al.*, 2012). Inorganic mesoporous alumina material have been selected to prepare a membrane for CO<sub>2</sub> gas separation since it is thermally and chemically stable and has good mechanical strength (Kwon *et al.*, 2012). Generally, the mesoporous alumina membrane provides high gas permeance but low selectivity due to transport of the gases through the pores by Knudsen diffusion mechanism in which the light gases permeate faster than heavy gases (Mukhtar and Othman, 2004). A well-known example is Knudsen separation of uranium isotopes (Keizer *et al.*, 1988). Higher Knudsen separation values are obtained for light gases such as H<sub>2</sub>/CO<sub>2</sub> with a separation factor of 4.7. Moreover, mesoporous  $\gamma$ -alumina membranes had an essential function as intermediate layer on macroporous supports in order to provide a smooth pore size transition between the support and the more selective microporous silica membranes (Xomeritakis *et al.*, 2009). Therefore, to achieve high separation factors, different mechanisms for gas transport through  $\gamma$ -alumina have to be employed.

Separation factors can be enhanced by introducing an interaction between one of the gases in the mixture and the membrane pore surface. If the adsorbed gas is mobile along the surface of the pore wall, it will diffuse in the direction of decreasing driving forces. The additional diffusion enhanced the gas permeance and separation factor of the more adsorbed gas. The presence of this type of transport, called surface diffusion, is frequently described in porous materials (Othman, 2009).

A few efforts have been reported to improve  $\gamma$ -alumina membranes to facilitate CO<sub>2</sub> surface diffusion. Keirzer et al. (1988) and Uhlhorn et al. (1989b) modified the  $\gamma$ -alumina membrane with magnesia (MgO) by impregnating technique to improve CO<sub>2</sub> surface diffusion and conform an increase in CO<sub>2</sub> adsorption. However, the modified membrane showed CO<sub>2</sub>/N<sub>2</sub> separation factor of only unit nearly to the Knudsen separation factor value, 0.8. They suppose that strong adsorption of CO<sub>2</sub> occurred on the MgO sites, resulting in a decrease in CO<sub>2</sub> permeation rate. Cho et al. (1995) improved the  $CO_2$  surface diffusion by doping calcium oxide (CaO) into the  $\gamma$ -alumina membrane. The  $CO_2/N_2$  separation factor was enhanced to be 1.72 at 25 °C and decreased with increase in the temperature to reach 1.5 at 200 °C. It was concluded that the separation factor could be enhanced by applying surface diffusion mechanism when the membrane is microporous and the operating temperature is low.

Hyun et al. (1996) modified the top layer of  $\gamma$ -alumina composite membranes supported on  $\alpha$ -alumina and titania by silane coupling with phenyltriethoxysilane to improve the CO<sub>2</sub> affinity. It was found that the separation factor of the modified  $\gamma$ alumina membranes with silane coupling was strongly dependent on the hydroxylation tendency of the support materials and the amount of phenol radical. The CO<sub>2</sub>/N<sub>2</sub> separation factor through the  $\gamma$ -alumina-titania membrane modified with the 10 wt. % silane solution was 1.7 at 90 °C and pressure difference of 200 kPa for the equimolar binary gas mixture, whereas, there was no improvement of CO<sub>2</sub>/N<sub>2</sub> separation factors in the  $\alpha$ -alumina supported case.

Lee et al. (2005) and (2006) investigated the effect of adsorption capacities of different gas species He, N<sub>2</sub>, CH<sub>4</sub>, C<sub>2</sub>H<sub>6</sub> and CO<sub>2</sub> on the permeation properties of mesoporous  $\gamma$ -alumina supported on  $\alpha$ -alumina. It was observed that the permeation of the adsorbing gas species (C<sub>2</sub>H<sub>6</sub> and CO<sub>2</sub>) increased through preferential adsorption on the membrane pore surface. It was observed that the permeance of the adsorbing gas components (C<sub>2</sub>H<sub>6</sub> and CO<sub>2</sub>) in the single gas system increased through preferential adsorption on the membrane pore surface more than the predicted value by the Knudsen diffusion. While for binary gas systems, the adsorbing gas component limited the diffusion of the weakly adsorbing gas through the  $\gamma$ -alumina membrane. It was concluded that the improvement in the adsorption capacity of membrane could enhance the separation factor in the presence of the adsorbing gas component due to the surface diffusion mechanism.

#### **2.1.1** Synthesis of $\gamma$ -alumina membrane by sol-gel method

The sol-gel process is the most practical method for fabrication of micro or meso porous inorganic membranes. The process involves the transition of suspension colloidal particles in a liquid system called sol into a semi- rigid solid network linked together by surface forces called gel. Therefore the term "sol-gel" processing can be used to describe wet chemical synthesis of inorganic materials in which eventually a particulate gel is produced. The sol-gel process starting from transformation of inorganic molecular precursor (metal alkoxide) into a highly cross linked solid (inorganic polymer) by hydrolysis and condensation reactions. Metal alkoxides have the general formula M(OR)<sub>z</sub> where M is a metal of valence z and R is an alkyl group (Rahaman, 1995). Alumina alkoxides Al(OR)<sub>3</sub> where R = (C<sub>4</sub>H<sub>9</sub>) are commonly used as a metal precursor for synthesis of alumina membrane from sol-gel method due to easily hydrolyzed by water to form hydroxides. The hydrolysis step replaces an alkoxide with a hydroxide group from water and a free alcohol (butanol) is formed as follows:

$$Al(OR)_3 + H_2O \rightarrow Al(OR)_2(OH) + ROH$$
 (2.1)

Once hydrolysis has occurred the sol can react further and condensation (polymerization) occurs resulting in boehmite (AlOOH) sol.

$$Al(OR)_2(OH) + H_2O \rightarrow AlOOH + 2ROH$$
 (2.2)

The following reaction might also be possible, provided that the coordination number of alumina was satisfied to cause the nucleophilic attack which initiated and facilitated water condensation reaction, giving rise to the production of alumina after liberation of water (Teoh *et al.*, 2007; Othman and Kim, 2008b).

$$AlOOH + AlOOH \rightarrow Al_2O_3 + H_2O$$
(2.3)

During hydrolysis step hydrochloric or nitric acid can be added into the boehmite mixture to facilitate peptization of the solution to a clear sol so that highly dispersed metals in the solution can be obtained (Yoldas, 1975; Othman et al., 2001). Changrong et al. (1996) investigated the effect of acidity on the boehmite sol properties. Stable boehmite sol was prepared by hydrolysis of aluminum tri-sec butoxide in hot distilled water at temperature above 80 °C and nitric acid was used as a sol peptizer. It was found that the size and shape of the sol particles as well as the viscosity affected by its acidity. For low acidity the sol particles was needle or rod shaped with diameters of a few nanometers and length around a hundred nanometers. Whereas, the sol particles change to granular or spherical shaped with diameter of 10-20 nm at high acidity conditions. On the other hand, the sol viscosity increased sharply with increase the acidity resulted in more chain between the particles and finally a tendency for gelation at high acidic conditions. The optimum mole ratio of acid to alkoxide used to obtain stable boehmite sol useful for synthesis crack free alumina membranes was around 0.07 (Ahmad et al., 2008; Kwon et al., 2012).

The crack formation during gels drying is the biggest challenge in the synthesis of  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> membrane from sol-gel process. Normally, organic binders are

added to the boehmite sol to avoid cracking formation in the initial drying process and during heat treatment. Polyvinyl alcohol (PVA) and polyethylene glycol (PEG) were found to be the most effective binders in the preparation of crack free  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> membrane (Lambert and Gonzalez, 1999; Othman *et al.*, 2001; Ahmad *et al.*, 2008). Othman et al. (2001) investigated the effect of PVA content on the characteristics of the sintered  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> membrane. It was demonstrated that the increase in PVA addition caused essential increase in the boehmite sol viscosity. High-viscosity sols form  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> membranes developed cracks during drying and sintering. On the other hand, the pore size of the sintered membrane increased with the increased PVA content. It was concluded that defect free  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> membrane with small pore size was prepared using 2 vol. % of PVA solution containing 4 g PVA in 100 ml of water.

Mesoporous  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> membranes were prepared by dip coating of boehmite sol onto  $\alpha$ -alumina support and drying at room temperature for 24 h (Othman *et al.*, 2001; Ahmad *et al.*, 2006b). The dried membranes were then sintered to get the final membrane. The membrane thickness was found to depend on the sol viscosity, dipping time and on the support pore size (Leenaars *et al.*, 1984; Othman *et al.*, 2001). However, multiply coating of the  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> membrane on the support was applied to avoid crack formation.

#### 2.2 Silica membranes for gas separation

Silica is considered an interesting material in the fabrication of  $CO_2$  selective membranes due to its low cost, availability and unique properties. It shows exceptional thermal, chemical, and structural stability in both oxidizing and reducing