Role Of Catalysts In The Decomposition Of Volatile Organic Compounds (VOCs) In Air Stream

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IRSTRACT: This article reviews the role of catalysts for catalytic decomposition of VOC in air. Major classes of catalyst immulations studied can be divided into four main categories vis supported metal catalysts, metal exchanged zeolites, perovskites immunicated catalyst. The most active metals are noble metals (Pt and Pd) and oxides of metals (Cr, Co, Cu, Fe, Mn and V) but immunicated with the type of VOC used. The high activity of a catalyst is commonly associated with high metal loading, high metal dispersion and the selection of suitable support. Chlorinated VOCs pose major challenge to the activity and viability of immunicated decomposition process. The decomposition of VOCs with low H/Cl ratio is relatively low and problems of catalyst immunication and formation of higher chlorinated species still remain unsatisfactorily solved. Thermal and hydrothermal stability immunicated much attention among researchers as the activity of the catalyst should be sustained in a prolonged high temperature of the product of the product

Lywords: VOCs, catalysts, oxidative decomposition, deactivation, chlorinated VOC, multicomponent VOCs, humid feed stream, product of incomplete combustion.

MTRODUCTION

Volatile organic compounds (VOCs) are an important class of air pellutants, emitted from many industrial processes (Kim and Ihn, 1999) and transportation activities (Becker and Forster, 1998; Niu et al., 1999). Catalytic combustion is one of the most promising technology for the decomposition of VOCs due to its definitive character and save of energy (Zhang et al., 1997). Catalytic oxidative decomposition is similar to thermal oxidation in that the gaseous impurities to be destroyed are reacted with oxygen at elevated temperature in form primarily carbon dioxide and water vapour. It differs in that the reactions are made to occur at a relatively low temperature by the use of a solid catalyst (Kohl and Nielsen, 1997). Typically, the reaction temperature is in the range of 150° to 480°C (Rafson, 1998), and is determined on the basis of the material being oxidized.

THE CATALYST

Many catalyst chemical formulations and geometric shapes are used to promote oxidation-reduction reactions (Rafson, 1998). Chemical types used for VOC oxidation include platinum, platinum alloys, copper chromate, copper oxide, cobalt oxide, chromium oxide, manganese oxide and nickel. The catalysts are often categorized as platinum metal group (PMG) and base metal (or metal oxide) types (Schneider et al., 2000). The active catalysts are often supported on an inert carrier such as γ -Al₂O₃. Catalyst forms include metal abbons, mesh and gauze, honeycomb monoliths and small

bends or particles that can be used in a fixed, fluidized or moving bed (Kohl and Nielson, 1997).

Noble metals (Pt and Pd) are among the most commonly used metal catalysts in investigations of VOC catalytic decomposition (Brink et al., 2000). Apart from the higher specific activity, they are favoured because of their resistance to sulfur poisoning (Niu et al., 1999) than oxide catalysts. In addition, highly dispersed Pt and Pd catalysts are easily prepared using a number of support materials (Zhang et al., 1997; Paulis et al., 2000).

The kinetics and mechanism of catalytic oxidation of hydrocarbons have been studied extensively. According to Zwinkels et al. (1993), there is correlation between the rate of hydrocarbon oxidation and metal-oxygen bond strength. Generally, this correlation can be presented as so-called volcano plot (Figure 1). A clear maximum in the plot is observed for platinum-group metals.

Metal (Group V_B to II_B) oxides are, in general, less active than the noble metals but are more resistant to poisoning (Sinquin et al., 2000). The most active oxides have a psemiconductor nature and the most frequently used ones are the oxides of V, Cr, Mn, Fe, Co, Ni and Cu. Chromium oxide is claimed to be one of the most active catalysts in chlorinated VOC destruction (Padilla et al., 1999), but the authors reported the formation of highly toxic by-products such as chromium oxychloride (Cr₂O₂Cl₂) and phosgene (COCl₂).

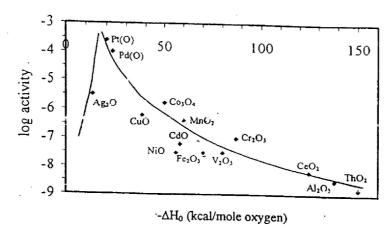


Figure 1: Volcano-type plot indicating specific activity in hydrocarbon oxidation as a function of the metal-oxygen bond streng (Zwinkels et al., 1993).

Supported Metal Catalyst

Piral₂O₃ catalysts as well as Pt and Pd on various supports (TiO₂, SiO₇, ZrO₂ etc) have been extensively studied (Brink et al., 2000). However, it seems that these catalysts are deactivated more or less depending on the oxidation system. Sinquin et al. (2000) claimed that after a slight initial deactivation, the activity is normally stabilized over a long period. Several authors point to deactivation particularly at low temperature (T<350° - 400°C) and on small metal particles (Tajima et al., 1997; Amores et al., 1999). The life time of these catalysts seems, therefore to depend on the reaction conditions and the preparation method.

Table 1 summarizes typical preparation method of suppor catalysts. As can be seen, most of the researchers empeither the incipient wetness or impregnation method to introduce the active metal catalysts into the support. Paulis al. (2000) introduced a new method of impregnation via a impregnation using citric acid solution. However, distinctive characteristics of the resulting final catalyst was demonstrated. In most of the recent researches, it is a catalyst compositions and not the preparation method the received more emphasis.

Refe	rence	Catalyst	supported catalysts	composition for VOC decomposition.
	a et al.	Pd, Fe, Co, Ni,	Support	Preparation/remarks
(1997		Cr, Mn, Mo, V	TiO_2 - ZrO_2	TiO ₂ -ZrO ₂ support was prepared by sol-get metho
	,	& W		wicklis wife infroduced through impregnation mathe
		OC VV		Aqueous solutions were added stirred dried calcing
Zhang	et al	Pt		(050 C, 2 hrs in air), grained and sieved (10-20 mesh)
(1997)		11	Fluorinated	infriegration with Ho-CH ₂ OH solution containing
			carbon powder	$1.0(1013)4(1003)_2$, dried (105°C, 16 hrs) H ₂ reduction
				(250 C, 10 nrs). Specific surface area=150m ² /g r
Ng et a	al.	Cr,Ni, Mn & Co	" A1 O 8 C'O	dispersion=9%.
(1998)		(chloride salts)	γ-Al ₂ O ₃ & SiO ₂ -	Incipient wetness method. Chloride salts were dissolved i
		(saits)	Al_2O_3	delonized H ₂ O, mixed and dried overnight at 120°C 11a.
Amore	s et	Mn	TiO ₂ (anatase)	101 hydrolytic decomposition of CFC-12
al. (199	99)		1102 (anatase)	Wet impregnation method. Adding salt precursor, stirring
 -				(100 C), myllig (100°C, 3 hrs) & calcination (60000)
Patters		Rh	δ-Al ₂ O ₃	143). Specific surface area=77-85 m²/g
al., (19	99)		5 1 11 203	Impregnation of δ-Al ₂ O ₃ containing 22% wt. CeO ₂ with
				Rh solution in HCl, calcination in air at 500°C. Specific surface area=27m ² /g.

Metal-Exchanged Zeolites

Zeolites can be formulated to carry active metals catalysts. The merit of zeolite-based catalysts is the active metal components are actually exchanged with the existing cations in the zeolites. Consequently, better metal dispersion down to nearly molecular level is expected. This property, coupled

with the size and shape features of the zeolites, allow the materials to be used as an effective catalyst in extremely selective reactions (Marcus and Cormier, 1999).

The presence of multivalent cations within the zeolite matrix has been found to increase its activity by creating highly acidic centres through hydrolysis of charged cations (Becker and Förster, 1998). The following systems have been myestigated: Cu-Y and Pd-Y/benzene (Becker and Förster, 1998), Pd-HFAU/o-xylene (Dégé et al., 2000) and Cr-ZSM-MTCE (Chintawar and Greene, 1997) and the results are very promising. However, problems regarding catalyst deactivation due to poisoning by chlorinated VOCs still remain unresolved (Brink et al., 1998; Kirn and Ihm, 1999).

Hydrophobicity and thermal resistance are found to increase with an increase in SiO₂/Al₂O₃ ratio of zeolites (Marcus and Cormier. 1999) Hydrophobic zeolites have recently gained much attention due to their ability to selectively remove one or more organic pollutants from humid air streams (Dégé et al, 2000). More hydrophobic zeolites such as ZSM-5 types, dealuminated faujasites and silicalite are found to be effective in removing VOCs from dilute or humid air streams (Marcus and Cormier. 1999). This property is expected to eliminate some of the problems associated with catalyst deactivation in the presence of high humidity (Becker and Poister, 1998).

Perovs! ites

Perovskites can be used given their ability to stabilized the brides on the catalytic system (Singuin et al., 2000). They are well known for their performances in total oxidation of hydrocarbons and/or CO as reviewed by Zwinkels et al. (1993) and Tofan et al. (2000). Among the mixed metal mide catalysts, perovskites-type oxides with the general formula ABO; ('A' represents a lanthanoide and/or alkaline earth metal ion and 'B' a transition metal ion) have been found to be effective catalysts for the total oxidation of hydrocarbons and exygenated compounds as well as chlorinated hydrocarbons (Schneider et al., 2000); Sinquin et al., 2000).

New and efficient methods of preparation using low cost precursors assures production of fine high specific surface area perovskite powders. Some research groups have reported their success of developing perovskite compositions which can conserve high activity even after calcination at temperatures above 1300K as reviewed by Tofan et al. (2000). Most of the research works on perovskites development for VOC decomposition include manganese and cobalt (Schneider et al., 2000; Sinquin et al., 2000) as an active element. Other compositions involve the use of strontium in addition to manganese and cobalt (Tofan et al., 2000). These materials were found to be equally promising and satisfactory for high temperature VOC catalytic combustion.

Structured Catalysts

Monolithic or honeycomb materials are unitary structures composed of inorganic oxides or metals in the structure of a boneycomb with equally sized and parallel channels which may be square, sinusoidal, triangular, hexagonal and round (Rafson, 1998). Monoliths are often washcoated with catalytically active high surface area materials such as γ -

Al₂O₃ (Barresi and Baldi, 1994), zeolite (Chatterjee and Greene, 1991) or perovskite (Schneider et al., 2000).

From the technical point of view, monolithic catalysts have several advantages compared with catalysts in pellet form e.g. the faster mass and heat transfer in the thin catalyst layer (Schneider et al., 2000) and the lower pressure drop in the reactor (Kohl and Nielsen, 1997). These materials can otter high thermal shock resistance, high mechanical strength and high melting point (Rafson, 1998). Other advantages are excellent attrition resistance, good mechanical properties, compact and freedom in reactor orientation as summarized by Heck and Farrauto (1995).

The washcoat influences the thermal shock resistance of the monolith (especially during rapid temperature changes) because it expands more than the monolith (Rafson, 1998). These differences must be factored into design of the finished catalysts to maintain good adherent coating without substantially weakening the monolith. There is also a limit to how much washcoat can be deposited on the monolith. Too much deposition results in a decrease of the effective channel diameter, thereby increasing the pressure drop to an unacceptable level (Kohl and Nielsen, 1997).

DECOMPOSITION OF CHLORINATED VOCS

Until recently, the use of catalytic oxidizers was restricted to nonhalogenated streams because halogen, especially chlorine, would poison the catalysts used. Brink et al. (2000) reported that noble metals were powerful oxidation catalysts, but can easily form inorganic chlorides with deactivation as a likely consequence. Reportedly the problem lies more with the catalyst carrier or washcoat rather than the catalyst (Cohl and Nielsen, 1997). Al₂O₃ support, for example, can react with chlorinated species to give AlCl₃ that subsequently can vaporize above 178°C (Velasco et al., 2000).

The quest for ideal catalysts for chlorinated VOC decomposition has received much attention among researchers. Chromia-alumina catalysts have been studied extensively as one of the most promising catalysts among commercially available materials (Kim and Ihm, 1999; Pradier et al., 2000). Brink et al. (2000) reported unsatisfactory result of their experiments on oxidative decomposition of chlorobenzene over Pt/γ-Al₂O₃. A study by Ng et al. (1998) concluded that metal chloride promoted γ-Al₂O₃ is an active catalyst for the hydrolytic decomposition of CFC-12 but the presence of water can depress the activity. Tajima et al. (1997) reported the excellent activity of WO₃/TiO₂-ZrO₂ supported catalysts for the decomposition of CFC113 but undesirable product CO in an amount equimolar to CO₂ was also detected.

In the decomposition of high CVH ratio VOCs, the addition of water in the feed stream is actually needed to improve the conversion (Velasco et al., 2000). Typically, water as hydrogen-supplying reactant is added to generate HCl by suppressing the formation of Cl₂ because HCl could be readily scrubbed downstream of the catalytic oxidizer (Kim

and Ihm, 1999; Padilla et al., 1999). Beside water, hexane, toluene (Velasco et al., 2000) methane and propane (Schneider et al., 2000) have also been studied for the same positive role. Brink et al. (2000) have extended the scope of the study to the removal of chlorine from catalyst surface. They came to the conclusion that removal of Cl from the surface (mainly in the form of HCl) by hydrocarbons is responsible for reducing the formation of by-products.

THERMAL AND HYDROTHERMAL STABILITY

In order to develop various heat-resistant or steam resistant alumina materials, many research works have been done recently, such as modifying transition alumina with additives of rare earth metal oxides (Ng et al., 1998), alkalıne earth metal oxides (Zwinkels et al., 1993), silica and other oxides such cerium oxide (Patterson et al., 1999). High temperature operation can cause conversion of catalyst supports to a new crystal structure. For example, when γ -Al₂O₃ convert to α -Al₂O₃, there is significant stepwise decrease in the internal urface area from about 150 to < 50 m²/g. Similarly, the nigher surface area (60 m²/g) TiO₂ anatase structure converts to rutile (< 10 m²/g) at about 550°C. The conversion versus temperature curve will usually undergo a loss in activity (Heck and Farrauto, 1995).

Reaction of the active catalytic component with the carrier can be a source of deactivation if the product is less active than the initial dispersed species. Pradier et al. (2000) reported a formation of chromium silicate and chromium aluminate from interaction between chromia and alumina and silicate respectively. Rh₂O₃ is reported to react with a high surface area Al₂O₃ to form an inactive compound during high-temperature operation (Heck and Farrauto, 1995). The reaction is believed to be occurring is conceptually shown below;

$$Rh_2O_3 + Al_2O_3 \longrightarrow Rh_2Al_2O_4 -----(1)$$

Becker and Förster (1998) claimed that compared to alumina supporting Pd catalysts, zeolite exchanging Pd catalysts have ther and more durable activity in low-temperature catalytic combustion of benzene. Unfortunately, the catalysts are very unstable and lose their activity easily in steam because the

hydrothermal treatment results in sharp dealumination of zeolites framework and ultimately leads to the collapse of the structure. Luckily, an increase in SiO₂/Al₂O₃ of the zeolites has been demonstrated to significantly improve their hydrothermal stability (Chintawar and Greene, 1997).

DECOMPOSITION OF MULTICOMPONENT VOCS

The presence of mixtures of VOCs which is usual for 'endof-pipe' air pollution control may affect the design criteria,
operation control and performance characteristics of a
catalytic incinerators (Dangi and Abraham, 1997). Sharma et
al. (1995) and Barresi and Baldi (1994) reported that it is
often not possible to predict what effect one component
might have on the rate of oxidation of the other. Thus, it is
very difficult to evaluate the performance characteristic of a
given catalytic incinerator as applied to a specific VOC
mixture, based on the behaviour of individual components.

Earlier studies have found that a mixture effect exists in the oxidation of hydrocarbons, mostly in the form of inhibition of oxidation of one hydrocarbon in the presence of others. Therefore, when inhibition effect is encountered, a higher temperature is usually needed to achieve a similar destruction level. It should also be noted that in some systems, promoting effect do occur (Table 2). However, no report has so far been made on inter-promoting effect between VOC components. Often, the promotional effect on the conversion of one. component is at the expense of the others. Various reasons for this phenomenon can be put forward, ranging from simple competitive-reactions rationale (Barresi and Baldi, 1994) to additional heat production (Valasco et al., 2000) or the formation of specific intermediates in the conversion of the additive (Sharma et al., 1995) but none of them satisfactorily explains the result.

Dangi and Abraham (1997) used the Mars-van Krevelen model to obtain the kinetic parameters needed to predict the mixture conversion over platinum catalyst. They tried to extend pure-component model to the two-component mixture of benzene and MTBE. Padilla et al. (1999) suggested that for destruction of chlorinated VOCs, the reaction rate, improves with an increase in H/Cl ratio brought about by addition of H supplying organic substances.

Reference	Experimenta	l conditions		g VOC mixtures decomposition. Finding/Conclusion
7	VOC	Catalyst	Temperature	_ tang conclusion
Baresi and Baldi (1994)	Toluene, xylene,	Pt/cordierite		Toluene and xylene conversion are inrhibited by benzene and ethylbenzene
	benzene ethlybenzene	&		and enlytoenzene
Sharma et al. (1995)	Methanol, acetone methylene chloride	Pt/ & & Pd/fluorinated carbon	50°-400°C	Methanol: promoting destruction of acetone and methylene chloride. Acetone: promoting destruction of methylene chloride while inhibiting destruction of methanol. Methylene chloride: inhibiting destruction of methanol and acetone.

Becker and Forster (1998)	Benzene & toluene	Cu - & Pd- zeolite Y	220°-350°C	Toluene promotes destruction of benzene only for Pd-Y catalyst.
Brink et al. (2000)	2-butene, toluene, heptane & chlorobenzene	Pt/γ-Al ₂ O ₃ .	100°-500°C	Chlorobenzene conversion is promoted by 2- butene, toluene and heptane. Chlorobenzene retards toluene and heptane
Velasco et al. (2000)	TCE, hexane & toluene	Pd/ & Pd/γ- Al ₂ O ₂	200°-550°C	conversion. Hexane and toluene promote TCE conversion over both catalysts.

THE EFFECT OF HUMIDITY IN FEED STREAM

Most of the industrial waste gases are often saturated with rater vapour (Ng et al., 1998). Moisture can cause musiderable problems with the practical application of malytic emission control in the sense that it generally inhibits a poisons the oxidation catalyst especially at low temperatures Becker and Förster, 1998). Thus the development of lowtemperature water-resistant catalysts is highly desirable (Zhang (al., 1997). The fact that the catalysts are more reactive in the absence of water shows that while water is a necessary reagent for the hydrolysis reaction (Sinquin et al., 2000), its presence

also has an inhibiting effect on the decomposition reaction (Ng et al., 1998).

Typically in a chlorinated VOC decomposition system, water is added to generate HCl by suppressing the formation of Cl2 because HCl could be readily scrubbed downstream of the catalytic oxidizer before exiting the stack (Kim and Ihm, 1999). The presence of water in feed stream is known to affect components in the product gas. Table 3 summarizes some of the effect observed by some recent research.

P.eference	Table 3 : Fffect of water on product gas co Operating conditions			Findings
	VOC/gas	Catalyst	Temperature	
Ng et al. (1993)	CFC-12	LaO ₂ / & SiO ₂ /γ-Al ₂ O ₃	350°-400°C	H ₂ O increases CO ₂ yield but suppresses CCl ₃ F and CCL formation.
Kim and Ihm (1999)	TCE	$CoCr_2O_4/$ and $ZnCr_2O_4/\gamma$ - Al_2O_3	330°C	H ₂ O suppresses Cl ₂ and tetrachlorcethylene by products'
Patterson et al. (1999)	Benzene/CO & toluene/CO	Rh/ & Rh/CeO ₂ /Al ₂ O ₃ with residual chlorine	100°-400°C	formation. H ₂ O reduces formation of chlcrobenzene from benzene/CO but increases yield of benzene from
Holmgren et d. (1999)	CO, ¹⁶ O ₂ & ¹⁸ O ₂	Pt/CeO ₂	45° & 140°C	toluene/CO. H ₂ O improves selectivity to C ¹⁶ O ₂ & C ¹⁶ O ¹⁸ O
Schneider et I. (2000)	dichloromethane	LaMnO ₃ coated monolith	500°-650°C	H ₂ O suppresses CCl ₄ , C ₂ HCl ₃ and C ₂ Cl ₄ formations but Cl ₂ formation is not influenced.

The weakly adsorbed water acts as an inhibitor of the raction. However, without water replenishing the surface hydroxyl groups (Patterson et al., 1999), the hydrolytic scivity is not sustainable. Water vapour can influence the ctivity of supported Pt catalysts in two ways. First, water molecules compete with reactant molecules for the surface Pt ities and therefore, affect the adsorption and activation of VOC and oxygen (Holmgren et al., 1999). Second, the accumulation of water on the support by adsorption and apillary condensation can affect the interaction between Pt and support, and can even deactivate some surface active siles (Zhang et al., 1997).

Hydrophobic catalysts have been intensively investigated for humid VOC decomposition applications (Chintawar and Greene, 1997; Niu et al., 2000). Hydrophobicity and thermal resistance are found to increase with an increase in \$i0₂/Al₂O₃ ratio of zeolites (Chintawar and Greene, 1997; Marcus and Cormier, 1999). More hydrophobic zeolites such s ZSM-5 types, dealuminated faujasites and silicalite are

found to be especially effective in removing VOCs from dilute or humid air streams (Marcus and Cormier, 1999). This property is expected to eliminate some of the problem associated with catalyst poisoning in the presence of high humidity (Becker and Förster, 1998).

PRODUCTS OF INCOMPLETE COMBUSTION (PICS)

In catalytic combustion processes for hydrocarbons and oxygenates, partial oxidation reactions must be avoided and CO2 and water being possibly the only products (Baldi et al., 1998; Zhang et al., 1997). According to the more strict limits for the emissions of some partially oxidized compounds, the presence of even small amounts of species e.g. aldehydes, can make the mixture resulting form catalytic combustion processes even more pollutant than the waste to be purified (Baldi et al., 1998).

Catalytic oxidation of chlorinated VOCs constitutes one of the most significant challenge as far as deep or complete oxidation is concerned. Ideally, there should be only HCl as the chlorine-containing species in the product gas. Chintawar and Greene (1997) have shown that among the first row transition metals, including Ni and Mn, only Cr has the ability to catalytically destroy TCE effectively. However, chromium residues are an environmental concern. Cr containing catalysts are also associated with the presence of elemental Cl_2 in the product gas due to well documented Deacon reaction (Brink et al., 2000); $2HCl + \frac{1}{2}O_2 \rightleftharpoons Cl_2 + H_2O$

Therefore, finding either an environmental friendly replacement or an active catalyst formulation containing very low levels of chromium would be worthwhile.

The addition of water as co-feed in the inlet gas has received considerable attention among researchers (Becker and Förster, 1998; Padilla et al., 1999; Velasco et al., 2000). Water can act as an H supplier to the decomposition of high CI/H ratio substances to improve selectivity toward HCl lasco et al., 2000) and to suppress Deacon reaction. It can also suppress the formation of PICs in many systems as what have been summarized in Table 4. Decomposition of CFC113 in the presence of water was studied over WO₃, MoO₃ and V₂O₅ supported on TiO₂-ZrO₂ and satisfactory conversion was achieved but the product gas contained considerable amount of C₂Cl₄F₂ and C₂Cl₂F₄ by-products (Tajima et al., 1997). Normally, selectivity toward deep exidation products deteriorates with time due to catalyst deactivation.

CONCLUSION

Supported metal catalysts, metal exchanged zeolites, perovekites and structured catalyst are main categories of catalyst systems currently being studied for VOC decomposition. The most active metals for this purpose are , noble metals (Pt and Pd) and metal oxides (Cr, Co, Cu, Fe, Mr. and V) but each metal has its own merits and weaknesses. Metal loading and dispersion as well as type of ort are the main determinant in the activity of a catalyst. Problems of catalyst deactivation and formation of higher chlorinated species still remain unsatisfactory resolved in atalytic abatement of chlorinated VOCs. Thermal and sydrothermal stability are another key factors in successful application of catalytic process and the development of stable catalysts is under way. Promotion or inhibition effect might ccur during the decomposition of mixture of VOCs and the haviour of the decomposition cannot be based on individual component. Competitive adsorption might occur the presence of water causing the retardation of the italyst activity. Water can suppress the formation of chlorinated by-products during high H/Cl ratio VOCs decomposition and favour HCl formation. Successful inversion of VOC should be evaluated with selectivity ward deep oxidation products (H2O, CO2 or HCl).

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