

UNIVERSITI SAINS MALAYSIA

First Semester Examination 2013/2014 Academic Session

December 2013/January 2014

ESA461/2 – Flight Stability and Control II
[Kawalan dan Kestabilan Pesawat II]

Duration : 2 hours
Masa : 2 jam

Please check that this paper contains **THIRTEEN (13)** printed pages, **THREE (3)** pages appendix and **FIVE(5)** questions before you begin the examination.

[Sila pastikan bahawa kertas soalan ini mengandungi **TIGA BELAS (13)** mukasurat bercetak, **TIGA (3)** mukasurat lampiran dan **LIMA (5)** soalan sebelum anda memulakan peperiksaan].

Instructions : Part A : Choose **ONE (1)** question **ONLY**. **Part B:** Answer **ALL** questions.

Arahan : BAHAGIAN A : Pilih SATU (1) soalan SAHAJA.

BAHAGIAN B : Jawab SEMUA soalan

1. **Appendix A/Lampiran A[FORMULA]:** [1 page/mukasurat]
 2. **Appendix B/Lampiran B** [2 pages/mukasurat]

Answer all questions in **English** OR **Bahasa Malaysia**.

[Menjawab semua soalan dalam **Bahasa Inggeris ATAU Bahasa Malaysia**].

Answer to each question must begin from a new page.

[Jawapan untuk setiap soalan mestilah dimulakan pada mukasurat yang baru].

In the event of any discrepancies, the English version shall be used.

[Sekiranya terdapat sebarang peranggahan pada soalan peperiksaan, versi Bahasa Inggeris hendaklah diguna pakai].

PART A: Choose ONE (1) question **ONLY**
BAHAGIAN A : Pilih SATU (1) soalan SAHAJA

1. [a] Briefly explain about directional stability and state the conditions required for an aircraft to remain stable in this motion.

(6 marks)

- [b] Vertical tail is one of the most influential components in directional stability. Its contribution to the aircraft's directional stability can be calculated from the following equation

$$C_{n_{\beta_v}} = V_v \eta_v C_{L_{av}} \left(1 + \frac{d\sigma}{d\beta} \right)$$

Where,

$$\eta_v \left(1 + \frac{d\sigma}{d\beta} \right) = 0.724 + 3.06 \frac{S_v/S}{1 + \cos A_{a/4w}} + 0.4 \frac{z_w}{d} + 0.009 AR_w$$

Let say a model of an airplane is tested in a wind tunnel with vertical tail off. Contributions of various components give $C_{n_g} = -0.001 \text{ deg}^{-1}$. If the vertical tail is to be positioned at a point on the aft end of the fuselage giving a tail length of 4.8 m , estimate the required vertical tail area to give an overall $C_{n_g} = 0.001 \text{ deg}^{-1}$? Given $C_{L_{av}} = 0.0454$, $A_{a/4w} = 0$, $S = 18 \text{ m}^2$, $b = 10.6 \text{ m}$ and the wing is set at the middle of the fuselage.

(14 marks)

- [c] Explain why deflecting the ailerons produce a yawing moment.

(5 marks)

- [a] Terangkan dengan ringkas tentang kestabilan berarah dan nyatakan keadaan yang diperlukan untuk sebuah kapal terbang kekal stabil dalam pergerakan ini.

(6 markah)

- [b] Ekor menegak merupakan salah satu komponen yang berpengaruh dalam kestabilan berarah. Sumbangannya kepada kestabilan berarah pesawat boleh dikira dengan menggunakan formula berikut

$$C_{n_{\beta_v}} = V_v \eta_v C_{L_{n_v}} \left(1 + \frac{d\sigma}{d\beta} \right)$$

Di mana

$$\eta_v \left(1 + \frac{d\sigma}{d\beta} \right) = 0.724 + 3.06 \frac{S_v/S}{1 + \cos A_{c/4w}} + 0.4 \frac{z_w}{d} + 0.009 AR_w$$

Katakan sebuah model pesawat tanpa ekor menegak diuji dalam sebuah terowong angin. Sumbangan pelbagai komponen pesawat tersebut memberikan $C_{n_{\beta}} = -0.001 \text{ deg}^{-1}$. Jika ekor menegak diletakkan pada bahagian belakang pesawat iaitu di hujung fiuslaj dengan panjang ekor adalah 4.8 m, anggarkan luas permukaan ekor menegak yang diperlukan untuk memberi kestabilan keseluruhan $C_{n_{\beta}} = 0.001 \text{ deg}^{-1}$. Diberi $C_{L_{n_v}} = 0.0454$, $A_{c/4w} = 0$, $S = 18 \text{ m}^2$, $b = 10.6 \text{ m}$ dan pesawat diletakkan pada pertengahan fiuslaj.

(14 markah)

- [c] Terangkan mengapa dengan memesongkan aileron menghasilkan momen rewang.

(5 markah)

2. [a] Briefly explain about asymmetric power and state the conditions required for an aircraft to remain stable in this motion.

(4 marks)

- [b] For the twin engine airplane shown in **Figure 1**, determine the rudder size to control the airplane if one engine needs to be shut down. Use the following flight information and **Figure 2** to solve this problem.

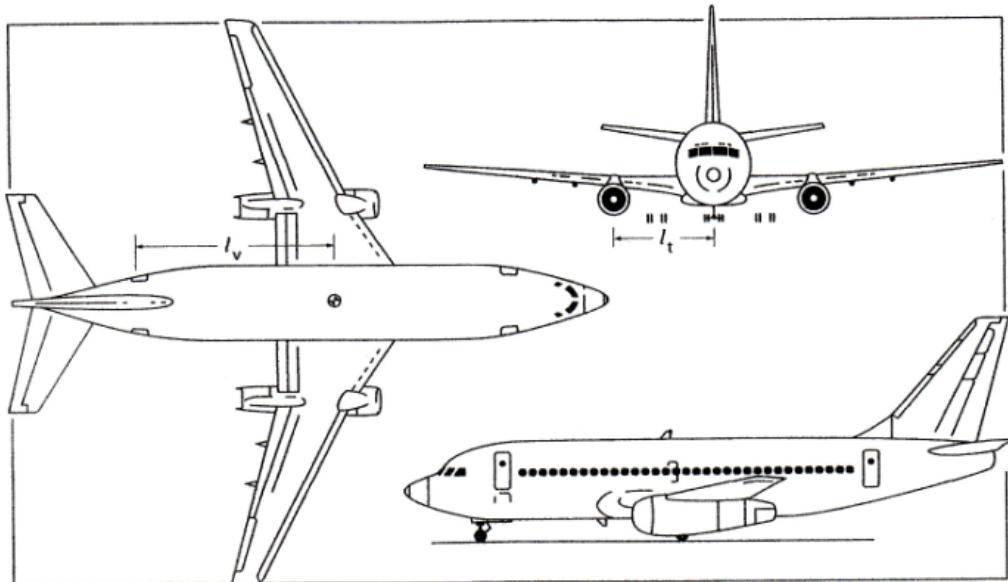
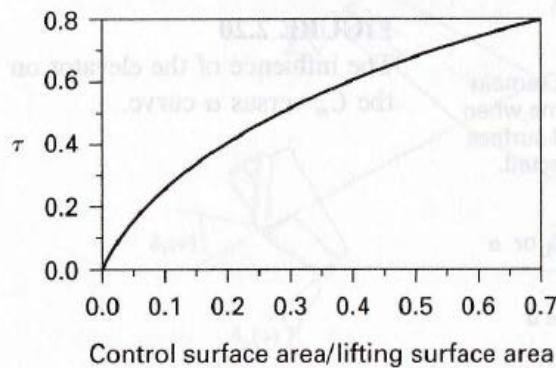
**Figure 1**

FIGURE 2.19

Figure 2

Wing: $S = 980 \text{ ft}^2$, $b = 93 \text{ ft}$

Vertical tail: $S_v = 330 \text{ ft}^2$, $AR_v = 4.3$, $l_v = 37 \text{ ft}$, $\eta_v = 1.0$, $C_{L_{av}} = 0.1/\text{deg}$

Rudder: $\delta_r = \pm 15^\circ$

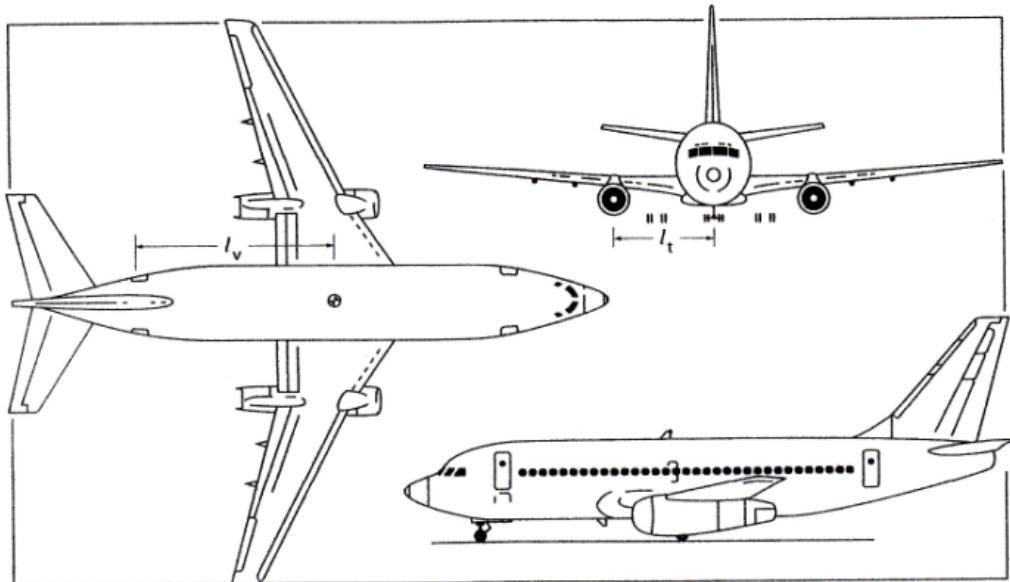
Propulsion: $T = 14,000 \text{ lb}$ each $y_T = 16 \text{ ft}$

Flight condition: $V = 250 \text{ ft/s}$, $\rho = 0.002378 \text{ slug}/\text{ft}^3$

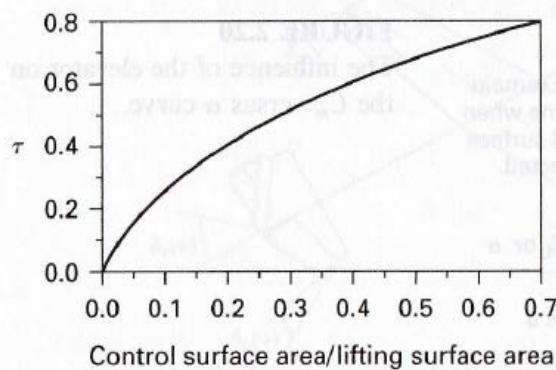
(21 marks)

- [a] Terangkan dengan ringkas tentang kuasa asimetri dan nyatakan keadaan yang diperlukan untuk sebuah kapal terbang kekal stabil dalam pergerakan ini. (4 markah)

- [b] Untuk kapal terbang dengan enjin berkembar seperti dalam **Rajah 1**, tentukan saiz kemudi untuk mengawal kapal terbang jika salah satu daripada enjin tersebut perlu dimatikan. Gunakan informasi penerbangan berikut dengan **Rajah 2** untuk menyelesaikan masalah ini.



Rajah 1



Rajah 2

Sayap: $S = 980 \text{ ft}^2$, $b = 93 \text{ ft}$

Ekor Tegak: $S_v = 330 \text{ ft}^2$, $AR_v = 4.3$, $l_v = 37 \text{ ft}$, $\eta_v = 1.0$, $C_{L_{av}} = 0.1/\text{deg}$

Kemudi: $\delta_r = \pm 15^\circ$

Pendorongan: $T = 14\,000 \text{ lb}$ each $y_T = 16 \text{ ft}$

Keadaan penerbangan: $V = 250 \text{ ft/s}$, $\rho = 0.002378 \text{ slug}/\text{ft}^3$

(21 markah)

PART B: Answer ALL questions.
BAHAGIAN B : Jawab SEMUA soalan.

3. [a] The stability coefficient C_{L_y} is the change in roll moment due to the yawing rate. What cause this effect and how does the vertical tail contribute to the C_{L_y} ? A simple discussion with appropriate sketches is required for this problem. **(4 marks)**
- [b] The stability coefficient $C_{L_{\delta_r}}$ is the change in roll moment coefficient due to rudder deflection. Again, explain how this effect occurs. **(1 marks)**
- [c] Using the geometric data given below and in **Figure 3**, estimate C_{L_p} and C_{n_r} . The roll moment coefficient due to rolling rate, C_{L_p} and yaw moment coefficient due to yawing rate, C_{n_r} can be formulated from the following equations respectively.

$$C_{L_p} = -\frac{C_{L_w}}{12} \frac{1+3\lambda}{1+\lambda}$$

$$C_{n_r} = -2\eta_v V_v \left(\frac{l_v}{b}\right) C_{L_{av}}$$

(20 marks)

Wing: $S = 232 \text{ ft}^2$, $b = 36 \text{ ft}$, $C_{L_{av}} = 0.1/\text{deg}$

Vertical tail: $S_v = 37.4 \text{ ft}^2$, $l_v = 18.5 \text{ ft}$, $C_{L_{av}} = 0.1/\text{deg}$, $\eta_v = 1$

Wing: $C_{L\alpha_w} = 0.1/\text{deg}$ $C_{m\text{ac}_w} = -0.02/\text{deg}$
 $\alpha_{Lo} = -1.0^\circ$

Tail: $C_{L\alpha_w} = 0.1/\text{deg}$ $C_{m\text{ac}_w} = 0.00$
 $\alpha_{Lo} = 0^\circ$

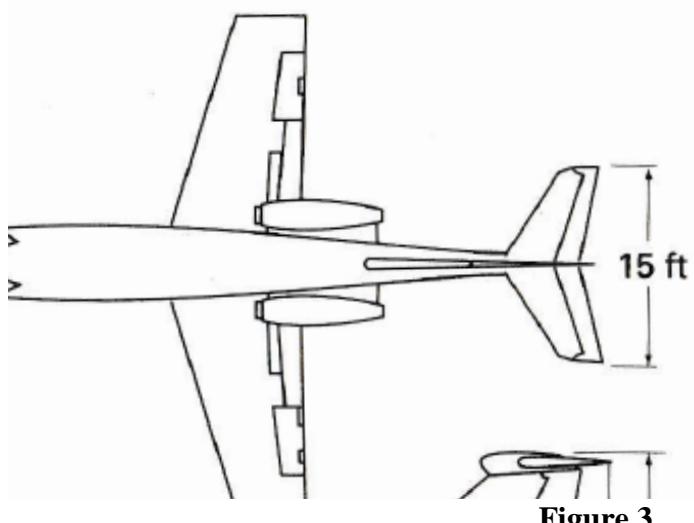


Figure 3

- [a] Kestabilan pekali C_{L_y} adalah perubahan dalam masa roll disebabkan oleh kadar rewang. Apa yang menyebabkan kesan ini dan bagaimana ekor menegak menyumbang kepada pekali C_{L_y} ? Satu perbincangan ringkas dengan lakaran yang sesuai diperlukan untuk masalah ini.

(4 markah)

- [b] Pekali kestabilan C_{L_y} adalah perubahan pekali momen roll yang disebabkan oleh kemudi pesongan. Sekali lagi, menjelaskan bagaimana kesan ini berlaku.

(1 markah)

- [c] Menggunakan data geometri yang diberikan di bawah dan di dalam **Rajah 3**, anggaran C_{L_p} and C_{n_r} . Pekali momen roll yang disebabkan oleh kadar roll, C_{L_p} dan pekali momen rewang yang disebabkan oleh kadar rewang, C_{n_r} boleh dirumuskan daripada persamaan berikut.

$$C_{L_p} = -\frac{C_{L_w}}{12} \frac{1+3\lambda}{1+\lambda}$$

$$C_{n_r} = -2\eta_v V_v \left(\frac{l_v}{b}\right) C_{L_{av}}$$

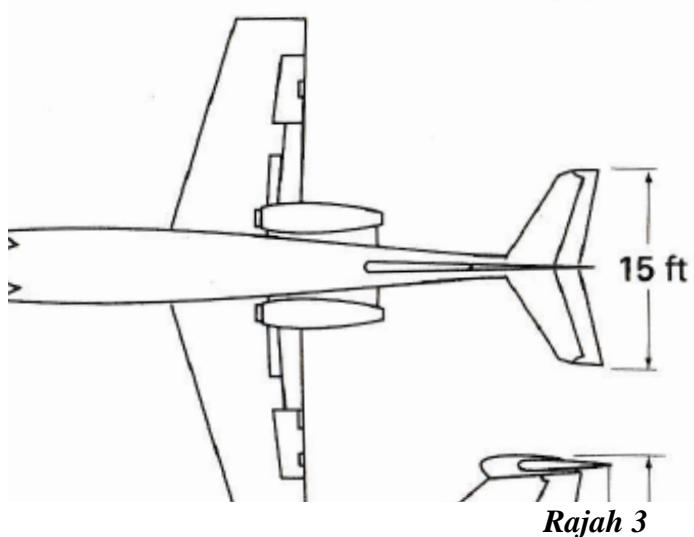
(20 markah)

Sayap: $S = 232 \text{ ft}^2$, $b = 36 \text{ ft}$, $C_{L_{av}} = 0.1/\text{deg}$

Ekor Tegak: $S_v = 37.4 \text{ ft}^2$, $l_v = 18.5 \text{ ft}$, $C_{L_{av}} = 0.1/\text{deg}$, $\eta_v = 1$

Wing: $C_{L\alpha_w} = 0.1/\text{deg}$ $C_{m_{ac_w}} = -0.02/\text{deg}$
 $\alpha_{Lo} = -1.0^\circ$

Tail: $C_{L\alpha_w} = 0.1/\text{deg}$ $C_{m_{ac_w}} = 0.00$
 $\alpha_{Lo} = 0^\circ$



4. Assuming the cruciform finned model in Figure 4 is mounted in a wind tunnel so that it is constrained to a pure yawing motion. The model is displaced from its trim position by 10^0 and then released. Neglect the fuselage and $\dot{\beta}$ contribution and assume $S = \pi D^2/4$.

[a] Find the time for the motion to damp to half its initial amplitude.

(15 marks)

[b] What is the period of the motion.

(10 marks)

$$D = \text{Characteristic length} = 5.0$$

Tail surfaces are flat plates: $I_z = 5.0 \times 10^{-2} \text{ kgm}^2$, $S = \pi D^2/4$

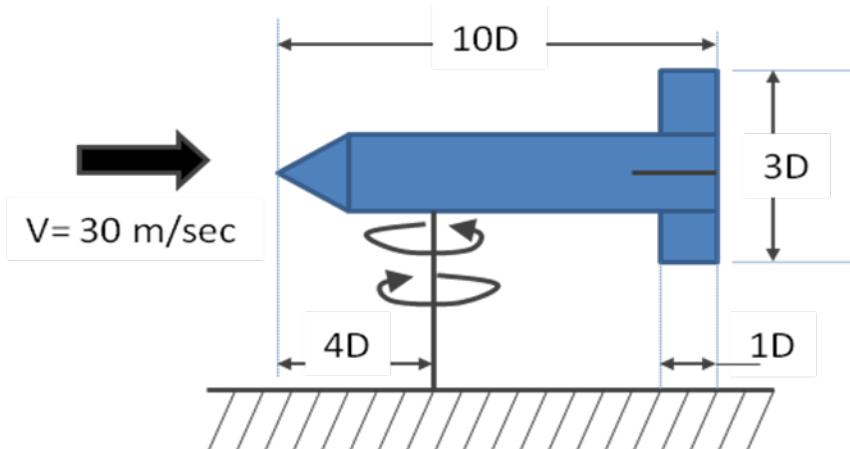


Figure 4

Dengan andaian model bersirip bentuk ‘Cruci’ seperti di **Rajah 4** yang dipasang di dalam terowong angin supaya ianya berlaku pergerakan rewang asli. Model yang disasarkan dari kedudukan cantas dengan 10° dan kemudian dibebaskan. Abaikan fusalj dan β sumbangan dan anggapkan $S = \pi D^2/4$.

- [a] Tentukan masa bagi pergerakan menjadi rendam untuk setengah amplitudo awal.

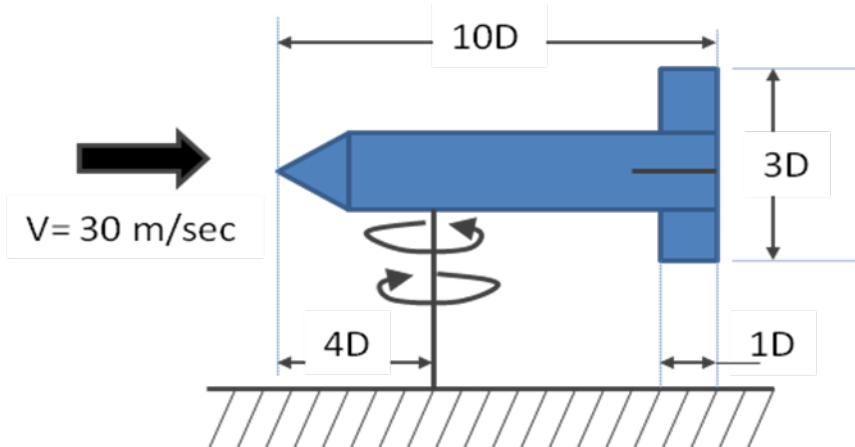
(15 markah)

- [b] Apakah tempoh pergerakan.

(10 markah)

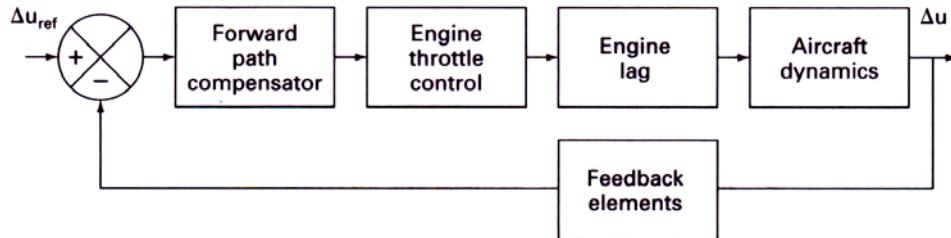
$$D = \text{Panjang Kriteria} = 5.0$$

Permukaan ekor adalah permukaan rata: $I_z = 5.0 \times 10^{-2} \text{ kgm}^2$, $S = \pi D^2/4$



Rajah 4

5. Examine the performance characteristics of a speed control autopilot similar to the one shown in **Figure 5** for the STOL transport included in **Appendix A**. The transfer functions for the throttle servo, engine lag, forward path compensation, and the feedback elements follow:

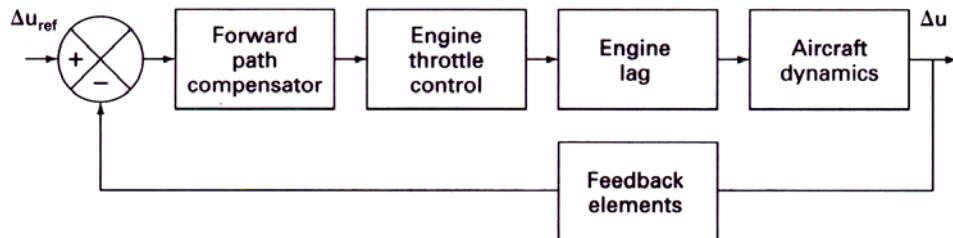
**Figure 5**

$$G_{Throttle}(s) = \frac{10}{s+10}, G_{enginelag}(s) = \frac{1}{s+0.1} ,$$

$$G_e(s) = 1 + \frac{0.1}{s} = \frac{k_a(s+0.1)}{s}, H = 10s + 1$$

- [a] Find the loop transfer function $G(s)H(s)$ (10 marks)
- [b] Using unit step response, determine the gains by sketch the graph time vs amplitude. (10 marks)
- [c] Discuss, how to improve the performance of this system. (5 marks)

Kaji ciri-ciri prestasi kelajuan kawalan autopilot yang sama seperti yang ditunjukkan dalam **Rajah 5** pengangkutan STOL yang disertakan dalam **Lampiran A**. Berikut adalah rangkap pindah bagi servo pendikit, lag enjin, kompensator laluan hadapan dan elemen suapbalik.



Rajah 5

$$G_{Throttle}(s) = \frac{10}{s+10}, G_{enginelag}(s) = \frac{1}{s+0.1}, \\ G_c(s) = 1 + \frac{0.1}{s} = \frac{k_a(s+0.1)}{s}, H = 10s + 1$$

- [a] Tentukan gelung rangkap pindah $G(s)H(s)$ (10 markah)
- [b] Tentukan gandar dengan memplot graf masa berlawanan dengan amplitud. (10 markah)
- [c] Bincangkan bagaimana untuk meningkatkan prestasi dalam sistem ini. (5 markah)

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APPENDIX A/ LAMPIRAN A

Geometric, Mass, and Aerodynamic Characteristic of Selected Airplanes

$$b \text{ Wing span} \quad C_{L_\alpha} = \frac{\partial C_L}{\partial \alpha} \text{ (rad}^{-1}\text{)}$$

$$\bar{c} \text{ Mean chord} \quad C_{L_\dot{\alpha}} = \frac{\partial C_L}{\partial \left(\frac{\dot{\alpha} \bar{c}}{2u_0} \right)} \text{ (rad}^{-1}\text{)}$$

$$C_L = \frac{L}{QS}$$

$$C_{L_M} = \frac{\partial C_L}{\partial M} \quad C_{l_{\delta_a}} = \frac{\partial C_l}{\partial \delta_r} \text{ (rad}^{-1}\text{)}$$

$$C_{L_{\delta_e}} = \frac{\partial C_L}{\partial \delta_e} \text{ (rad}^{-1}\text{)} \quad C_{l_{\delta_r}} = \frac{\partial C_l}{\partial \delta_r} \text{ (rad}^{-1}\text{)}$$

$$C_D = \frac{D}{QS} \quad C_n = \frac{N}{QSb}$$

$$C_{D_\alpha} = \frac{\partial C_D}{\partial \alpha} \text{ (rad}^{-1}\text{)} \quad C_{n_\beta} = \frac{\partial C_n}{\partial \beta} \text{ (rad}^{-1}\text{)}$$

$$C_{D_M} = \frac{\partial C_D}{\partial M} \quad C_{n_p} = \frac{\partial C_n}{\partial (pb/2u_0)} \text{ (rad}^{-1}\text{)}$$

$$C_{D_{\delta_e}} = \frac{\partial C_D}{\partial \delta_e} \text{ (rad}^{-1}\text{)} \quad C_{n_r} = \frac{\partial C_n}{\partial (rb/2u_0)} \text{ (rad}^{-1}\text{)}$$

$$C_m = \frac{M}{QS\bar{c}} \quad C_{m_\alpha} = \frac{\partial C_m}{\partial (\dot{\alpha} \bar{c}/2u_0)} \text{ (rad}^{-1}\text{)}$$

$$C_{m_\alpha} = \frac{\partial C_m}{\partial \alpha} \quad C_{m_M} = \frac{\partial C_m}{\partial M}$$

$$C_y = \frac{Y}{QS} \quad C_{m_q} = \frac{\partial C_m}{\partial (q\bar{c}/2u_0)} \text{ (rad}^{-1}\text{)}$$

$$C_{y_\beta} = \frac{\partial C_y}{\partial \beta} \text{ (rad}^{-1}\text{)} \quad C_{n_{\delta_a}} = \frac{\partial C_n}{\partial \delta_a} \text{ (rad}^{-1}\text{)}$$

$$C_{y_{\delta_r}} = \frac{\partial C_y}{\partial \delta_r} \text{ (rad}^{-1}\text{)} \quad C_{n_{\delta_r}} = \frac{\partial C_n}{\partial \delta_r} \text{ (rad}^{-1}\text{)}$$

$$C_l = \frac{L}{QSb}$$

I_x Rolling moment of inertia

$$C_{l_\beta} = \frac{\partial C_l}{\partial \beta} \text{ (rad}^{-1}\text{)}$$

I_y Pitching moment of inertia

$$C_{l_p} = \frac{\partial C_l}{\partial (pb/2u_0)} \text{ (rad}^{-1}\text{)}$$

I_z Yawing moment of inertia

$$C_{l_r} = \frac{\partial C_l}{\partial (rb/2u_0)} \text{ (rad}^{-1}\text{)}$$

I_{xz} Product of inertia about xz axis

M Mach number

Q Dynamic pressure

S Wing planform area

u_0 Reference flight speed

APPENDIX B /LAMPIRANB

STOL Transport Reference data

TABLE B.28
STOL Transport

	C_L	C_D	C_{L_0}	C_{D_0}	C_{m_0}	C_{L_d}	C_{m_d}	C_{L_r}	C_{m_r}	C_{L_w}	C_{m_w}	C_{D_w}	C_{m_b}	C_{L_b}	C_{m_b}
Longitudinal															
M = 0.14															
Sea level	1.5	0.127	5.24	0.67	-0.78	1.33	-6.05	7.83	-35.6	0	0	0	0	0.465	-2.12
M = 0.37															
10,000 ft	0.3	0.036	5.24	0.67	-0.78	1.33	-6.05	7.83	-35.6	0	0	0	0	0.465	-2.12
Lateral															
M = 0.14															
Sea level	-0.362	-0.125	0.101	-0.53	-0.283	0.410	-0.188	0.20	0	-0.233	-0.024	0.107			
M = 0.37															
10,000 ft	-0.362	-0.125	0.101	-0.53	-0.037	0.113	-0.171	0.20	0	-0.233	-0.024	0.107			

Note: All derivatives are per radian.

