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UNIVERSITI SAINS MALAYSIA

1<sup>st</sup>. Semester Examination  
2004/2005 Academic Session  
*Peperiksaan Semester 1*  
*Sidang Akademik 2004/2005*

October 2004

**EAS 663/4 – Dynamics and Stability of Structures**  
***EAS 663/4 – Dinamik dan Kestabilan Struktur***

Duration: 3 hours  
*Masa : 3 jam*

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**Instructions to candidates:**

1. Ensure that this paper contains **TEN (10)** printed pages included appendices.  
*Sila pastikan kertas peperiksaan ini mengandungi **SEPULUH (10)** muka surat bercetak termasuk lampiran sebelum anda memulakan peperiksaan ini.*
2. This paper contains **FIVE (5)** questions. Answer **ALL (5)** questions.  
*Kertas ini mengandungi **FIVE (5)** soalan. Jawab **KESEMUA LIMA (5)** soalan..*
3. All questions **CAN BE** answered in English or Bahasa Malaysia or combination of both languages.  
*Semua soalan boleh dijawab dalam Bahasa Inggeris atau Bahasa Malaysia ataupun kombinasi kedua-dua bahasa.*
4. Each question carry equal marks.  
*Tiap-tiap soalan mempunyai markah yang sama.*
5. All question **MUST BE** answered on a new sheet.  
*Semua jawapan **MESTILAH** dijawab pada muka surat yang baru.*
6. Write the answered question numbers on the cover sheet of the answer script.  
*Tuliskan nombor soalan yang dijawab di luar kulit buku jawapan anda.*

1. (a) List two characteristics that distinguish structural dynamic problems from static ones.

(a) *Senaraikan dua ciri yang membezakan masalah struktur dinamik daripada masalah statik.*

(4 marks)

(b) Define viscous damping. Sketch the displacement response, (v) versus (t) of undamped and damped SDOF systems for free vibration. Does the natural period of vibration, T, change with the present of damping?

(b) *Takrifkan redaman likat. Lakarkan sambutan anjakan, v, melawan masa (t) untuk sistem Kebebasan Satu Darjah yang tanpa redaman dan dengan redaman. Adakah kala getaran, T, berubah dengan kehadiran redaman?*

(6 marks)

(c) Figure 1.0 shows a model of spring-mass SDOF system that is subjected to a harmonic excitation,  $p(t) = 50 \cos 10t$  N. The weight of the mass block is 150 kN and the spring stiffness,  $k = 7000$  N/m. Assume the damping of the system is equal to 5% of the critical damping. Determine the total displacement response of the system which is given by the following equation:

$$v(t) = V \cos(\Omega t - \alpha) + e^{-\zeta\omega t} (A_1 \cos \omega_d t + A_2 \sin \omega_d t)$$

$$V = \frac{v_r}{\sqrt{(1-r^2)^2 + (2\zeta r)^2}}$$

where  $\omega$ : natural circular frequency of the system and  $v_0$  : static displacement due to  $p_o$ .

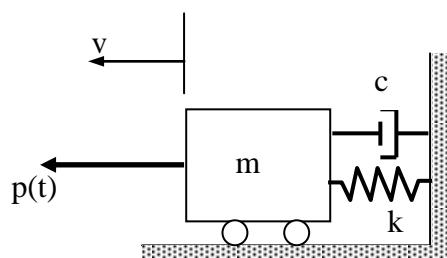
(c) *Rajah 1.0 menunjukkan satu sistem jisim- pegas dengan Kebebasan Satu Darjah yang dikenakan satu getaran harmonik ,  $p(t) = 50 \cos 10t$  N. Berat jisim blok ialah 150 kN dan kekuahan pegas,  $k = 7000$  N/m. Anggap bahawa redaman dalam sistem bersamaan 5% daripada redaman kritikal. Kira nilai sambutan anjakan sistem tersebut yang diberi dalam persamaan berikut :*

$$v(t) = V \cos(\Omega t - \alpha) + e^{-\zeta\omega t} (A_1 \cos \omega_d t + A_2 \sin \omega_d t)$$

$$V = \frac{v_r}{\sqrt{(1-r^2)^2 + (2\zeta r)^2}}$$

*iaitu  $\omega$  ialah frekuensi bulatan tabii sistem dan  $v_0$  ialah anjakan statik disebabkan oleh  $p_o$ .*

(10 marks)



**Figure 1.0**

2. (a) Duhamel Integral is normally used for the evaluation of a linear SDOF system subjected to arbitrary time varying force. Define the underlined term with the help of a graph Force, (P) versus (t).

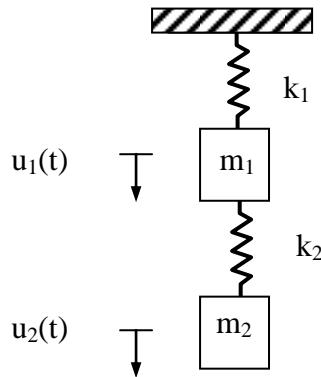
(a) Kamilan Duhamel biasanya digunakan untuk penilaian sistem Kebebasan Satu Darjah yang dikenakan daya ubah waktu sembarang. Takrifkan perkataan yang bergaris dengan bantuan rajah daya, (P)v, melawan masa (t).

(5 marks)

- (b) Figure 2.0 shows a spring-mass model for 2DOF system under free vibration. Derive the equations of motion for the system.

(b) Rajah 2.0 menunjukkan satu model jisim-pegs dengan Kebebasan Dua Darjah yang dikenakan getaran bebas. Terbitkan persamaan gerakan untuk sistem tersebut.

(5 marks)



**Figure 2.0 (a)**

- (c) The water tower as shown in Figure 2.0 (b) weighs 700kN when filled with water is subjected to step force with rise time [Figure 2.0 (c)]. It is observed that a horizontal jack force of 30kN is required to displace the tower top by a distance of 20mm. Estimate the maximum lateral displacement response due to dynamic forces. The constant phase is given by the following equation:

$$v(t) = v_0 \left\{ 1 + \frac{1}{\omega t_r} [A \sin(\omega(t - t_r) + \alpha)] \right\}$$

$$A = \sqrt{(1 - \cos \omega t_r)^2 + (\sin \omega t_r)^2}, \quad \tan \alpha = -\frac{\sin \omega t_r}{(1 - \cos \omega t_r)}$$

where  $\omega$  : natural circular frequency of the system ,  $v_0$  : static displacement due to  $p_0$  ,  $v_{max}$  : maximum response and  $T_n$  : natural period of vibration. A plot of  $R_d (= v_{max}/v_0)$  versus  $t_r/T_n$  is shown in Figure 2.0 (d). Comment on the effect of ratio  $t_r/T_n$  on  $R_d$  , without carrying out any “exact” dynamic analysis.

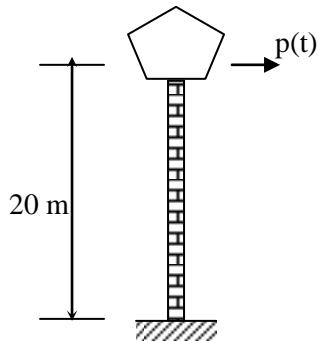
(c) Menara air yang ditunjukkan dalam Rajah 2.0 (b) mempunyai berat 700kN apabila penuh dengan air yang dikenakan daya langkah dengan masa kenaikan yang terhingga [Rajah 2.0 (c)]. Diberi bahawa satu daya ufuk sebesar 30kN diperlukan untuk menganjukkan bahagian atas menara air sebanyak 20mm. Anggarkan sambutan anjakan maksima yang disebabkan oleh satu daya dinamik. Persamaan sambutan anjakan semasa fasa malar adalah seperti berikut:

$$v(t) = v_0 \left\{ 1 + \frac{1}{\omega t_r} [A \sin(\omega(t - t_r) + \alpha)] \right\}$$

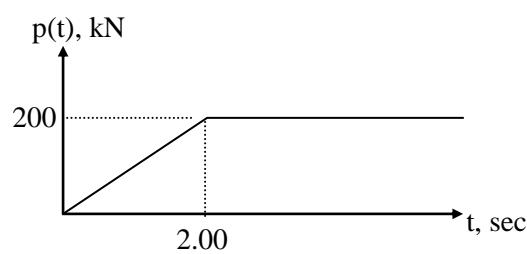
$$A = \sqrt{(1 - \cos \omega t_r)^2 + (\sin \omega t_r)^2}, \quad \tan \alpha = -\frac{\sin \omega t_r}{(1 - \cos \omega t_r)}$$

iaitu  $\omega$  : frekuensi bulatan tabii sistem,  $v_0$  : anjakan statik disebabkan oleh  $p_o$ ,  $v_{max}$  : sambutan maksimum dan  $T_n$  : kala tabii getaran. Satu plot  $R_d (= v_{max} / v_0)$  lawan nisbah  $t_r / T_n$  ditunjukkan dalam Rajah 2.0 (d). Beri ulasan tentang kesan nisbah  $t_r / T_n$  ke atas  $R_d$  tanpa menjalankan sebarang analisis dinamik "sebenar".

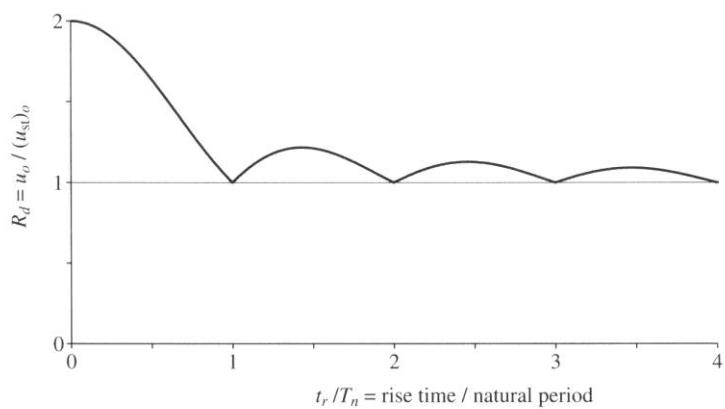
(10 marks)



**Figure 2.0 (b)**



**Figure 2.0 (c)**



**Figure 2.0 (d)**

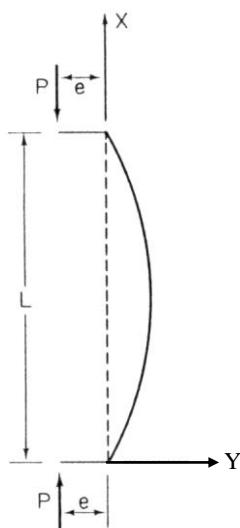
3. (a) By using an axially loaded and perfectly straight column with both ends pinned, explain the concepts of stable, unstable and neutral equilibrium.

(6 marks)

- (b) Figure 3.0 shows an initially straight column subjected to an axial load  $P$  which acts at an eccentricity  $e$  from the centroidal axis of the column. Obtain the following relation between mid-height deflection  $\delta$  and ratio  $P/P_E$  where  $P_E$  : Euler buckling load  $= \pi^2 EI/L^2$ :

$$\delta = e \left[ \sec \left( \frac{\pi}{2} \sqrt{\frac{P}{P_E}} \right) - 1 \right]$$

Sketch a plot of  $P/P_E$  versus  $\delta$  for three different values of  $e$ .



**Figure 3.0**

Sketch also on the same plot the graph representing the behaviour of an initially straight column with  $e=0$ . Based on the graph, discuss the effect of imperfection of load on the behaviour of an axially loaded column.

(14 marks)

4. (a) Derive the following fourth order differential equation for beam-column :

$$y^{iv} + k^2 y'' = 0, \quad k^2 = \frac{P}{EI}$$

where  $y$  : lateral displacement of beam-column,  $P$  : axial force acting at both ends of beam-column,  $EI$  : flexural rigidity and  $(\dots)' = d(\dots)/dx$ . Next, explain how the above fourth order differential equation is used to determine the critical load of beam-column with different end conditions. You are required to specifically point out in your explanation how starting from the fourth order differential equation, one can arrive at the eigenvalue problem which can be used to solve for the critical load of beam-column with different end conditions.

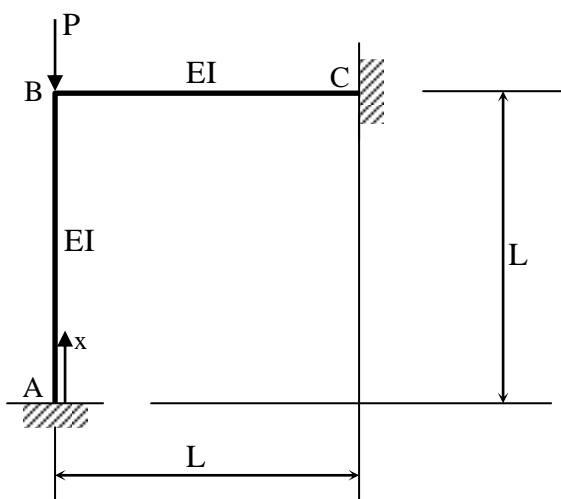
(10 marks)  
...6/-

- (b) A simple two-bar frame is shown in Figure 3.0. A load  $P$  acts at end B of vertical member AB. Both supports A and C are fixed. Obtain the effective length  $L_e$  for the two-bar frame by using the following equation for an elastically restrained column:

$$(1 - \lambda_1 - \lambda_2 - \lambda_1 \lambda_2 \Phi^2) \Phi \sin \Phi + (2 + \lambda_1 \Phi^2 + \lambda_2 \Phi^2) \cos \Phi - 2 = 0$$

where  $\lambda_1 = EI/(\alpha_1 L)$ ,  $\lambda_2 = EI/(\alpha_2 L)$ ,  $\Phi = kL$ ,  $k^2 = P/EI$ ,  $EI$  : flexural rigidity ,  $L$  : length of column,  $\alpha_1, \alpha_2$  : rotational stiffness of end 1 and 2 of column being studied, respectively. Justify your solution for the effective length obtained by using information provided in Table 1.0 (see Appendix 1).

(10 marks)



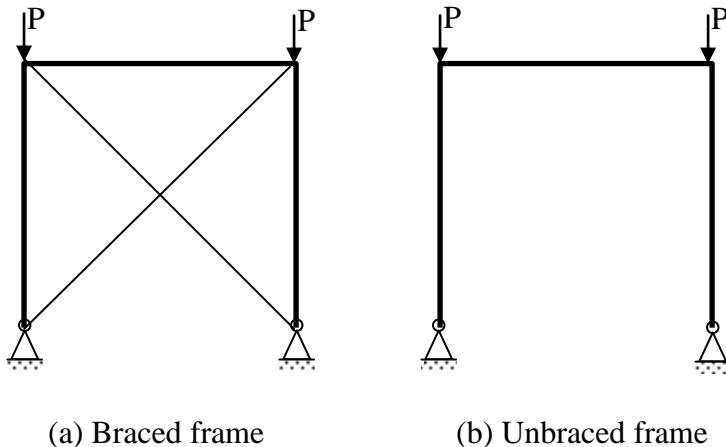
**Figure 3.0**

5. (a) Figure 4.0 (a) and (b) show braced and unbraced frames, respectively. For each frame, sketch the buckling mode corresponding to the lowest critical load. Using suitable eigenvalue analysis, it can be shown that effective length factor K for

- i. column in braced frame is  $K < 1.0$  and
- ii. column in unbraced frame is  $K > 1.0$

Justify the above conclusions by referring to behavior of columns with other standard end conditions.

(6 marks)



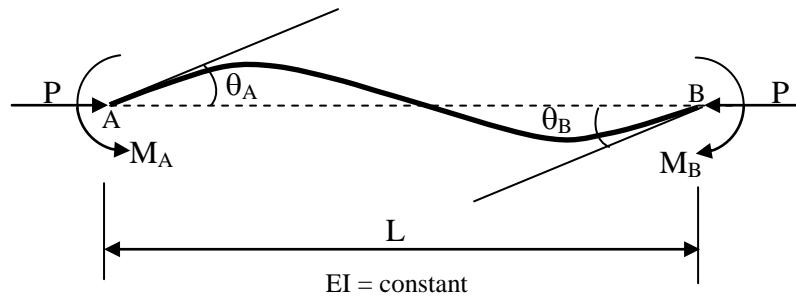
**Figure 4.0**

- (b) Slope deflection equations for a beam-column are given as follows :

$$M_A = \frac{EI}{L} (s_{ii}\theta_A + s_{ij}\theta_B)$$

$$M_B = \frac{EI}{L} (s_{ji}\theta_A + s_{jj}\theta_B)$$

where  $s_{ii}$ ,  $s_{ij}$  ( $= s_{ji}$ ),  $s_{jj}$  are stability functions and  $M_A$ ,  $M_B$ ,  $\theta_A$  and  $\theta_B$  are as shown in Figure 5.0.



**Figure 5.0**

Making use of the previous set of slope-deflection equations and the following assumptions for a member in a braced frame:

- i. All members are prismatic and behave elastically
- ii. The axial forces in the beam are negligible
- iii. All columns in a storey buckle simultaneously
- iv. At a joint, the restraining moment provided by the beams is distributed among the columns in proportion to their stiffness
- v. At buckling, the rotations at the near and far ends of the beams are equal and opposite

show the process of deriving the following eigenvalue problem for the determination of effective length of a column in a braced frame :

$$\begin{bmatrix} s_{ii} + \frac{2}{G_A} & s_{ij} \\ s_{ij} & s_{jj} + \frac{2}{G_B} \end{bmatrix} \begin{Bmatrix} \theta_A \\ \theta_B \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix}$$

where  $G_A$ ,  $G_B$  are defined as follows :

$$G_A = \frac{\sum_A (I/L)_{column}}{\sum_A (I/L)_{beam}} = \frac{\sum \text{of column stiffness meeting at end A}}{\sum \text{of beam stiffness meeting at end A}}$$

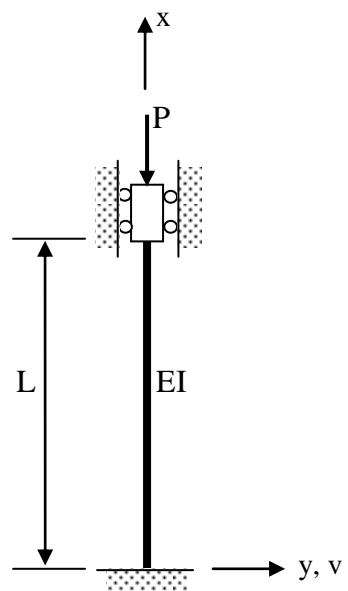
$$G_B = \frac{\sum_B (I/L)_{column}}{\sum_B (I/L)_{beam}} = \frac{\sum \text{of column stiffness meeting at end B}}{\sum \text{of beam stiffness meeting at end B}}$$

You are required:

- i. to show the equations involved in arriving at the eigenvalue problem
- ii. to show a suitable sketch showing the column in a braced frame
- iii. to state how the assumptions listed above are used in the derivation

(14 marks)

Supplements :



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