
UNIVERSITI SAINS MALAYSIA

Second Semester Examination
Academic Session 2006/2007
*Peperiksaan Semester Kedua
Sidang Akademik 2006/2007*

April 2007

EBB 409/3 – Fluid Power and Machinery ***EBB 409/3 – Kuasa Bendalir & Mesin Turbo***

Time: 3 hours
Masa: 3 jam

Please ensure that this paper consists of THIRTY THREE printed pages before you proceed with the examination.

Sila pastikan bahawa kertas peperiksaan ini mengandungi TIGA PULUH TIGA muka surat yang bercetak sebelum anda memulakan peperiksaan.

This paper contains TWENTY questions from PART A, THIRTY questions from PART B and SIX questions from PART C.

Kertas soalan ini mengandungi DUA PULUH soalan dari BAHAGIAN A, TIGA PULUH soalan dari BAHAGIAN B dan ENAM soalan dari BAHAGIAN C.

Answer ALL question from PART A, ALL question from PART B and FOUR question from PART C. If a candidate answers more than four questions only the first four questions answered in the answer script would be examined.

Jawab SEMUA soalan dari BAHAGIAN A, SEMUA soalan dari BAHAGIAN B dan EMPAT soalan dari BAHAGIAN C. Jika calon menjawab lebih daripada empat soalan hanya empat soalan pertama mengikut susunan dalam skrip jawapan akan diberi markah.

Answer to each and every question must start on a new page.

Mulakan jawapan anda untuk setiap soalan pada muka surat yang baru.

All questions must be answered in English.

Jawab semua soalan dalam Bahasa Inggeris.

PART A:

BAHAGIAN A:

Answer whether the 1- 20 statements True or false:

Jawab samada betul atau salah bagi kenyataan 1-20:

1. Fluid power is the technology which deals with the generation, control and transmission of power using pressurized fluids.
Kuasa bendalir adalah teknologi yang berhubung dengan penjanaan, kawalan dan penghantaran kuasa menggunakan bendalir di bawah tekanan.
2. Hydraulic cylinder creates a torque that can rotate a shaft.
Silinder hidraulik akan menghasilkan kilasan yang boleh memutarkan aci.
3. Hydraulic motor creates a force that can push or pull a load.
Motor hidraulik menghasilkan daya yang boleh menolak atau menarik beban.
4. Prime mover is an electric motor or other power source to drive the pump or compressor.
Pengerak primier adalah motor elektrik atau sumber kuasa lain yang memacu pam atau kompressor.
5. Liquids provide a very rigid medium for transmitting power.
Cecair memberikan medium yang tegar untuk menghantar kuasa.
6. Liquid cannot provide huge forces to move loads with utmost accuracy and precision.
Cecair tidak boleh memberikan daya yang besar untuk mengerakkan beban dengan kejituuan yang tinggi.

7. One of Pneumatic application is aircraft landing gear.

Salah satu kegunaan Penumatik ialah gear pendaratan kapal terbang.

8. One of Hydraulic application is artificial heart.

Salah satu kegunaan hidraulik ialah jantung tiruan.

9. One of Hydraulic application is automobile power steering.

Salah satu kegunaan hidraulik ialah stering kuasa kendaraan.

10. One of Pneumatic applications is robotic materials handling devices.

Salah satu kegunaan Penumatik ialah peranti pengendalian bahan robotik.

11. One of hydraulic fluid primary functions is dissipate heat.

Salah satu kegunaan utama bendalir hidrolik ialah untuk pelepasan haba.

12. A hydraulic fluid should not have high degree of incompressibility.

Bendalir hidraulik tidak sepatutnya mempunyai darjah ketidakbolehmampatan yang tinggi.

13. Absolute pressure-gage pressure relationship is $P_{abs} = p_{gage} + P_{atm}$.

Tolok-tekanan mutlak mutlak mempunyai hubungan tekanan bersamaan dengan $P_{abs} = P_{gauge} + P_{atm}$.

14. -40° temperatures are the Fahrenheit and Celsius values are equal.

Suhu -40° dalam Ferenhite dan Celsius adalah sama.

15. Efficiency is defined as input power divided by output power.

Kecekapan didefinisikan sebagai kuasa input dibahagikan kepada kuasa output.

16. The weight flow rate is the same for all cross-sections of a pipe, thus the smaller the pipe diameter the greater the velocity and vice versa.

Berat kadar alir adalah sama dengan keratan rentas paip, oleh itu, semakin kecil diameter paip, semakin besar kelajuan bendalir dan sebaliknya.

17. Ideally the velocity of a free jet of fluid is not equal to the square root of the product of two times the acceleration of gravity times the head producing the jet.

Secara ideal, kelajuan jet bebas bendalir tidak sama dengan punca kuasa dua hasil pendaraban dua kali pecutan gravity dengan kepala yang menghasilkan jet.

18. In the External Gear Pump the volumetric displacement can be represented by

$$V_D = [\pi/4] (D_o^2 + D_i^2) L.$$

Di dalam Pam Gear Dalaman, peralihan volumetrik boleh diberikan sebagai
 $V_D = [\pi/4](D_o^2 + D_i^2)L.$

19. The actual volumetric displacement in vane pump can be represented by

$$V_{Dmax} = (\pi/4)(D_C + D_R)2eL.$$

Peralihan volumetrik sebenar pada penunjuk pam boleh diberikan sebagai:

$$V_{Dmax} = [\pi/4](D_C + D_R)2eL.$$

20. The overall efficiency of pumps considers all energy losses and hence is equals to [actual power delivered by pump]/ [actual power delivered to pump].

Kecekapan keseluruhan pam mengambil kira semua tenaga yang terhilang oleh itu adalah bersamaan dengan [kuasa sebenar yang dibawa oleh pam]/[kuasa sebenar yang di bawa ke pam].

(40 marks)

Part B:

BAHAGIAN B:

The following questions 21 to 40, chose the correct answer.

Soalan berikutnya (21-40) mesti dijawab dengan memilih jawapan yang betul.

21. Fluid Power Systems normally

- [a] Hindered by geometry or machine.
- [b] Provides no remote control.
- [c] Complex mechanical linkages are eliminated.
- [d] Instantly irreversible motion.

Sistem Kuasa Bendalir selalunya

- [a] Dihalang oleh geometri atau mesin.
- [b] Tidak boleh di kawal jauh.
- [c] Menghapuskan hubungan mekanikal yang kompleks.
- [d] Menghasilkan pergerakkan berbalik serta merta.

22. Mechanical System normally

- [a] A mess due to oil leakage problems.
- [b] No danger of bursting of hydraulic lines.
- [c] Fire hazard due to oil leaks.
- [d] Infinitely variable speed control

Sistem mekanikal selalunya

- [a] adalah kotor kerana masalah dengan kebocoran minyak.
- [b] tidak berbahaya kerana talian hidrolik.
- [c] Adalah bahaya api kerana kebocoran minyak.
- [d] Mempunyai kawalan kelajuan bolehubah yang kecil.

23. The pressure on a skin diver that has descended to a depth of 60 ft in fresh water with its density of 0.0361 lb/in³ is
- [a] 20 psi
 - [b] 30 psi
 - [c] 60psi
 - [d] 26psi.

Tekanan pada kulit penyelam yang telah menyelam pada kedalaman 60 kaki di dalam air tawar yang mempunyai ketumpatan [0.0361lb/in³] ialah:

- [a] 20 psi
- [b] 30 psi
- [c] 60psi
- [d] 26psi.

24. Viscosity index (VI) is equal to

- [a] $[L-U]/[L+H] \times 100$
- [b] $[L-U]/[L-H] \times 100$
- [c] $[L+U]/[L+H] \times 100$
- [d] $[L+U]/[L-H] \times 100$

where L = viscosity in SUS of 0-VI oil at 100°F, U = viscosity in SUS of unknown-VI oil at 100°F and H = viscosity in SUS of 100-VI oil at 100°F.

Indeks kelikatan (VI) adalah bersamaan dengan

- [a] $[L-U]/[L+H] \times 100$
- [b] $[L-U]/[L-H] \times 100$
- [c] $[L+U]/[L+H] \times 100$
- [d] $[L+U]/[L-H] \times 100$

di mana L = kelikatan di dalam SUS minyak 0-VI pada 100°F, U = kelikatan di dalam SUS minyak 0-VI yang tidak diketahui pada 100°F dan H = kelikatan di dalam SUS untuk minyak 100-VI pada 100°F.

25. Conversion of – 34 000 Pa pressure to an absolute pressure is equal to:

- [a] 70 000 Pa abs
- [b] 68 000 Pa abs
- [c] 67 000 Pa abs
- [d] 87 000 Pa abs

Pertukaran pada tekanan ~ 34 000 Pa ke tekanan mutlak adalah bersamaan dengan:

- [a] 70 000 Pa abs
- [b] 68 000 Pa abs
- [c] 67 000 Pa abs
- [d] 87 000 Pa abs

26. The continuity Equation is

- [a] $\gamma_1 A_1 v_1 = \gamma_2 A_2 v_2$
- [b] $\gamma_1 A_1 v_1 = \gamma_2 A_2 v_1$
- [c] $\gamma_1 A_1 v_2 = \gamma_2 A_2 v_1$
- [d] $\gamma_2 A_1 v_1 = \gamma_1 A_2 v_2$

where γ = specific weight of fluid (lb/ft^3),

A = cross-sectional area of pipe (ft),

v = velocity of fluid (ft/s).

Persamaan keterusan adalah

- [a] $\gamma_1 A_1 v_1 = \gamma_2 A_2 v_2$
- [b] $\gamma_1 A_1 v_1 = \gamma_2 A_2 v_2$
- [c] $\gamma_1 A_1 v_2 = \gamma_2 A_2 v_1$
- [d] $\gamma_2 A_1 v_1 = \gamma_1 A_2 v_2$

di mana γ = berat tentu bendalir (lb/ft^3)

A = keratan ringkas kawasan paip (ft)

V = kelajuan bendalir (ft/s)

27. Pump head is

- [a] $H_p \text{ (m)} = \text{pump hydraulic power (W)} \times Q(m^3/s) \times \gamma(N/m^3)$
- [b] $H_p \text{ (m)} = \text{pump hydraulic power (W)} / Q(m^3/s) / \gamma(N/m^3)$
- [c] $H_p \text{ (m)} = \text{pump hydraulic power (W)} / Q(m^3/s) \times \gamma(N/m^3)$
- [d] $H_p \text{ (m)} = \text{pump hydraulic power (W)}^2 / Q(m^3/s) \times \gamma(N/m^3)$

Kepala pam adalah

- [a] $H_p \text{ (m)} \text{ kuasa pam hidraulik (W)} \times Q(m^3/s) \times \gamma(N/m^3)$
- [b] $H_p \text{ (m)} = \text{kuasa pam hidraulik (W)} / Q(m^3/s) / \gamma(N/m^3)$
- [c] $H_p \text{ (m)} = \text{kuasa pam hidraulik (W)} / Q(m^3/s) \times \gamma(N/m^3)$
- [d] $H_p \text{ (m)} = \text{kuasa pam hidraulik (W)}^2 / Q(m^3/s) \times \gamma(N/m^3)$

28. The velocity of oil is flowing through a 30 mm diameter pipe at 60 liters per min (Lpm) is:

- [a] 1.20m/s
- [b] 1.65m/s
- [c] 1.90m/s
- [d] 1.41m/s

Kelajuan minyak mengalir di dalam paip yang berdiameter 30mm pada 60 litre per min (Lpm) ialah:

- [a] 1.20m/s
- [b] 1.65m/s
- [c] 1.90m/s
- [d] 1.41m/s

29. Reynolds number is:

- [a] $N_R = vD\rho\mu$
- [b] $N_R = vD\rho/\mu$
- [c] $N_R = vD/\rho\mu$
- [d] $N_R = v/D\rho\mu$

where; v velocity, D diameter, ρ density and μ absolute viscosity.

Nombor Reynold ialah:

- [a] $N_R = vD\rho\mu$
- [b] $N_R = vD\rho/\mu$
- [c] $N_R = vD/\rho\mu$
- [d] $N_R = v/D\rho\mu$

di mana v = kelajuan, D = diameter, ρ = ketumpatan dan μ kelikatan mutlak

30. The Reynolds number of hydraulic oil having the kinematic viscosity $0.0001 \text{ m}^2/\text{s}$ flowing in a 30-mm diameter pipe at a velocity of 6 m/s is:

- [a] 4000
- [b] 3500
- [c] 2000
- [d] 1800

Nombor Reynold pada minyak hidrolik yang mempunyai kelikatan kinematik $0.0001 \text{ m}^2/\text{s}$ mengalir di dalam paip yang berdiameter 30 mm pada kelajuan 6m/s ialah:

- [a] 4000
- [b] 3500
- [c] 2000
- [d] 1800

31. Head loss in valves and fittings is:

- [a] $H_L = K(2v^2g)$
- [b] $H_L = K/(v^2/2g)$
- [c] $H_L = K/(2v^2g)$
- [d] $H_L = K(v^2/2g)$

Kehilangan pada kepala injap dan pemasangan ialah:

- [a] $H_L = K(2v^2g)$
- [b] $H_L = K/(v^2/2g)$
- [c] $H_L = K/(2v^2g)$
- [d] $H_L = K(v^2/2g)$

32. The volumetric displacement of a vane pump has a rotor diameter of 50mm, a cam ring diameter of 75 mm, a vane width of 50 mm and the eccentricity is 8 mm is

- [a] 0.785 litters
- [b] 0.0785 litters
- [c] 0.00785 litters
- [d] 78.5 litters

Anjakan volumetrik pada pam ram yang mempunyai diameter rotor 50mm, diameter sesondol 75mm, lebar ram 50mm dan esentrivity 8mm ialah B bersamaan dengan

- [a] 0.785 litters
- [b] 0.0785 litters
- [c] 0.00785 litters
- [d] 78.5 litters

33. In Piston pumps Maximum piston stork can be obtained at:

- [a] less angle θ
- [b] angle $\theta = 0$
- [c] maximum angle θ
- [d] none of above

Di dalam pam omboh, maksimum lejang omboh boleh dicapai pada

- [a] kurang daripada sudut θ
- [b] sudut $\theta=0$
- [c] sudut maksimum θ
- [d] tiada yang di atas

34. In Piston pump the Volumetric displacement is:

- [a] $V_D = YAD \tan^2 (\theta)$
- [b] $V_D = YAD \tan (2\theta)$
- [c] $V_D = YAD/ \tan (\theta)$
- [d] $V_D = YAD \tan (\theta)$

where Y = number of pistons, A = piston area (in^2, m^2), D = piston circle diameter (in, m), θ = offset angle ($^\circ$)

Di dalam pam piston, anjakan volumetrik ialah:

- [a] $V_D = YAD \tan^2 (\theta)$
- [b] $V_D = YAD \tan (2\theta)$
- [c] $V_D = YAD/ \tan (\theta)$
- [d] $V_D = YAD \tan (\theta)$

di mana Y = bilangan piston, A = kawasan piston (in^2, m^2), D = diameter bulatan piston (in, m), θ = sudut offset ($^\circ$)

35. In Piston Pump the mechanical efficiency can be measured by:

- [a] $\eta_m = [p \text{ (Pa)} \times Q_T(m^3/s)]/[T_A(N.m) \times N(rad/s)]$
- [b] $\eta_m = [2p \text{ (Pa)} \times Q_T(m^3/s)]/[T_A(N.m) \times N(rad/s)]$
- [c] $\eta_m = [p \text{ (Pa)} \times Q_T(m^3/s)]/[2T_A(N.m) \times N(rad/s)]$
- [d] $\eta_m = [p \text{ (Pa)} \times Q_T(m^3/s)]/[T_A(N.m) \times N^2(rad/s)]$

where p = pump discharge pressure (psi, Pa), Q_T = pump theoretical flow-rate (gpm, m^3/s) T_A = actual torque delivered to pump (in .lb, N .m) N = pump speed (rpm, rad/s).

Di dalam pam piston, kecekapan mekanikal boleh diukur dengan

- [a] $\eta_m = [p \text{ (Pa)} \times Q_T(m^3/s)]/[T_A(N.m) \times N(rad/s)]$
- [b] $\eta_m = [2p \text{ (Pa)} \times Q_T(m^3/s)]/[T_A(N.m) \times N(rad/s)]$
- [c] $\eta_m = [p \text{ (Pa)} \times Q_T(m^3/s)]/[2T_A(N.m) \times N(rad/s)]$
- [d] $\eta_m = [p \text{ (Pa)} \times Q_T(m^3/s)]/[T_A(N.m) \times N^2(rad/s)]$

di mana p = tekanan nyahcas pam (psi, Pa), Q_T = kadar aliran pam theoritikal ($gpm, m^3/s$), T_A = tork sebenar yang dihantar ke pa, (in lb, N.m), N = kelajuan pam (rpm, rad/s).

36. The Pump overall efficiency can be expressed as:

- [a] $\eta_o = \eta_v \times \eta_m$
- [b] $\eta_o = \eta_v / \eta_m$
- [c] $\eta_o = \eta_m / \eta_v$
- [d] $\eta_o = [\eta_v \times \eta_m]^2$

where η_o = overall efficiency, η_v = volumetric efficiency and η_m = mechanical efficiency.

Kecekapan keseluruhan pam boleh diberikan sebagai:

- [a] $\eta_o = \eta_v \times \eta_m$
- [b] $\eta_o = \eta_v / \eta_m$
- [c] $\eta_o = \eta_m / \eta_v$
- [d] $\eta_o = [\eta_v \times \eta_m]^2$

di mana η_o = kecekapan keseluruhan, η_v = kecekapan volumetrik and η_m = kecekapan mekanikal.

37. The Equivalent length of valves and fittings can be shown as:

- [a] $Le = KfD$
- [b] $Le = fK/D$
- [c] $Le = KD/f^2$
- [d] $Le = KD/f$

where K factor (called loss coefficient), D = pipe inside diameter (ft, m), ,f = friction factor (dimensionless).

Persamaan panjang injap dan pengetat boleh ditunjukkan sebagai:

- [a] $Le = KfD$
- [b] $Le = fK/D$
- [c] $Le = KD/f^2$
- [d] $Le = KD/f$

di mana faktor K (dipanggil pekali kehilangan), D = diameter dalaman paip (ft, m), f = faktor geseran (tidak berdimensi)

38. Hydraulic horsepower is:

- [a] $HHP = [P(\text{psi}) \times Q(\text{gpm})]/9550$
- [b] $HHP = [P(\text{psi}) \times Q(\text{gpm})]/1714$
- [c] $HHP = [P(\text{psi}) \times Q(\text{gpm})]$
- [d] $HHP = [P(\text{psi}) \times Q(\text{gpm})]/3950$

where P pressure, Q flow rate

Kuasakuda hiraolik ialah:

- [a] $HHP = [P(\text{psi}) \times Q(\text{gpm})]/9550$
- [b] $HHP = [P(\text{psi}) \times Q(\text{gpm})]/1714$
- [c] $HHP = [P(\text{psi}) \times Q(\text{gpm})]$
- [d] $HHP = [P(\text{psi}) \times Q(\text{gpm})]/3950$

di mana P = tekanan dan Q = kadar aliran

39. Energy equation is:

- [a] $Z_1 + P_1/\gamma + v^2_1/2g + H_p - H_m - H_L = Z_2 - P_2/\gamma - v^2_2/2g$
- [b] $Z_1 + P_1/\gamma + v^2_2/2g + H_p - H_m - H_L = Z_2 + P_1/\gamma + v^2_2/2g$
- [c] $Z_1 + P_1/\gamma + v^2_1/2g + H_p - H_m - H_L = Z_2 + P_2/\gamma + v^2_2/2g$
- [d] $Z_1 + P_1/\gamma + v^2_1/2g + H_p + H_m + H_L = Z_2 + P_2/\gamma + v^2_2/2g$

where H_p Pump head, H_m motor head, H_L loss head.

Persamaan tenaga ialah:

- [a] $Z_1 + P_1/\gamma + v^2_1/2g + H_p - H_m - H_L = Z_2 - P_2/\gamma - v^2_2/2g$
- [b] $Z_1 + P_1/\gamma + v^2_2/2g + H_p - H_m - H_L = Z_2 + P_1/\gamma + v^2_2/2g$
- [c] $Z_1 + P_1/\gamma + v^2_1/2g + H_p - H_m - H_L = Z_2 + P_2/\gamma + v^2_2/2g$
- [d] $Z_1 + P_1/\gamma + v^2_1/2g + H_p + H_m + H_L = Z_2 + P_2/\gamma + v^2_2/2g$

di mana H_p = kepala pam, H_m = kepala motor dan H_L = kehilangan kepala.

40. Fluid velocities can be expressed by:

- [a] $v = Q/A$
- [b] $v = QA$
- [c] $v = A/Q$
- [d] $v = QA^2$

where Q is the flow rate and A is the cross section area of the pipe.

Kelajuan bendalir boleh diberikan sebagai:

- [a] $v = Q/A$
- [b] $v = QA$
- [c] $v = A/Q$
- [d] $v = QA^2$

di mana Q adalah kadar aliran dan A ialah keratan rentas kawasan paip.

41. Weight-mass relationship is:

- [a] $F = w = m/g$
- [b] $F = w = m/2g$
- [c] $F = w = mg$
- [d] $D. F = w = m^2g$

where m is the mass and g acceleration of gravity.

Persamaan berat-jisim ialah:

- [a] $F = w = m/g$
- [b] $F = w = m/2g$
- [c] $F = w = mg$
- [d] $D. F = w = m^2g$

di mana m ialah jisim dan g pecutan graviti.

48. Power required to drive a compressor:

- [a] Theoretical power (kW) = $[P_{in}] [(P_{out}/P_{in})^{0.286} - 1]]$
- [b] Theoretical power (kW) = $[17.1P_{in}] [(P_{out}/P_{in})^{0.286} - 1]]$
- [c] Theoretical power (kW) = $[P_{in}/17.1] [(P_{out}/P_{in}) - 1]]$
- [d] Theoretical power (kW) = $[P_{in}/17.1] [(P_{out}/P_{in})^{0.286} - 1]]$

P is the pressure.

Kuasa yang diperlukan untuk memandu kompresor ialah:

- [a] Kuasa teori (kW) = $[P_{in}] [(P_{out}/P_{in})^{0.286} - 1]]$
- [b] Kuasa teori (kW) = $[17.1P_{in}] [(P_{out}/P_{in})^{0.286} - 1]]$
- [c] Kuasa teori (kW) = $[P_{in}/17.1] [(P_{out}/P_{in}) - 1]]$
- [d] Kuasa teori (kW) = $[P_{in}/17.1] [(P_{out}/P_{in})^{0.286} - 1]]$

P ialah tekanan.

49. General Gas Law:

- [a] $P_1V_1T_1 = P_2V_2T_2$
- [b] $P_1V_1/T_1 = P_2V_2/T_2$
- [c] $P_1V_2/T_1 = P_2V_1/T_2$
- [d] $P_1/[V_1T_1] = P_2/[V_2T_2]$

where P is the pressure, V is the volume and T is the temperature

Hukum gas umum:

- [a] $P_1V_1T_1 = P_2V_2T_2$
- [b] $P_1V_1/T_1 = P_2V_2/T_2$
- [c] $P_1V_2/T_1 = P_2V_1/T_2$
- [d] $P_1/[V_1T_1] = P_2/[V_2T_2]$

di mana P ialah tekanan, V ialah isipadu dan T ialah suhu.

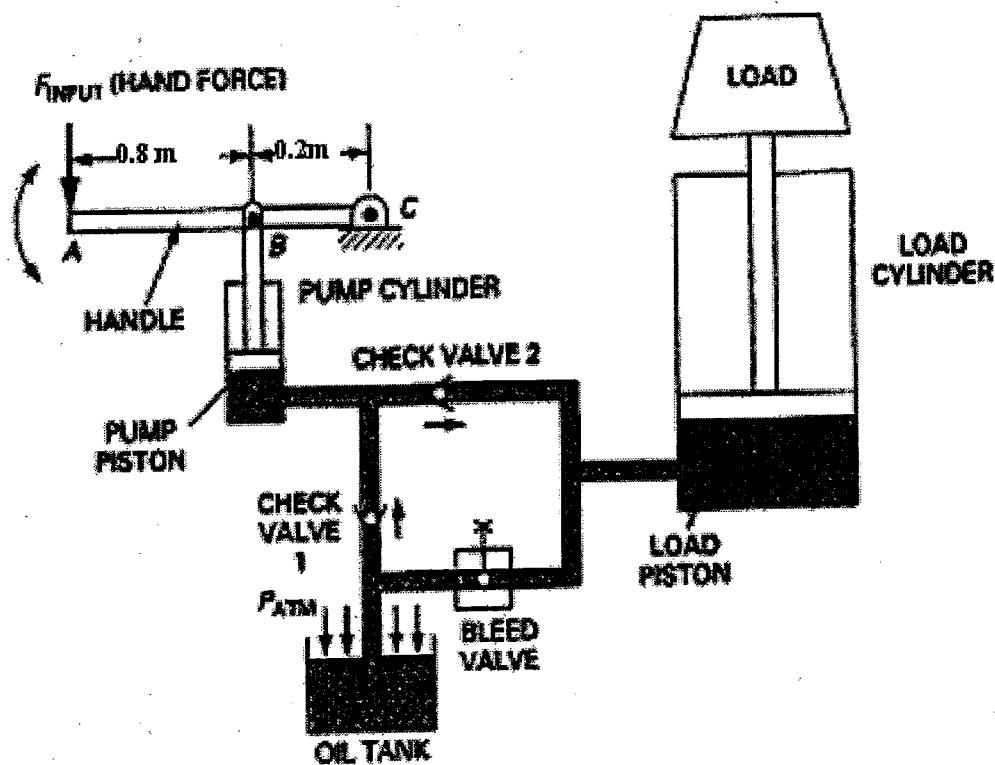
PART C:

BAHAGIAN C:

1. [a] An operator makes 20 complete cycles during a 15-sec interval using the hand pump of Figure 1A. Each complete cycle consists of two pump strokes (intake and power). The pump has a 5.08 cm diameter piston and the load cylinder has a 10.16cm diameter piston. The average hand force is 88.6 N during each power stroke.
 - (i) How much load can be lifted?
 - (ii) Through what distance will the load be moved during the 15-sec interval assuming no oil leakage? The pump piston has a 7.62 cm stroke.
 - (iii) What is the output HP assuming 90% efficiency?

Seorang operator membuat 20 putaran lengkap di dalam masa 15 saat menggunakan pam tangan seperti yang ditunjukkan pada Rajah 1A. Setiap kitaran yang lengkap mempunyai dua pukulan pam (pengambilan dan kuasa). Pam mempunyai 5.08 cm diameter piston dan beban pada silinder ialah 10.16cm diameter piston. Purata daya tangan ialah 88.6N pada setiap pukulan kuasa.

- (i) *Berapa banyak beban yang boleh diangkat*
- (ii) *Berapa jauhkan jarak beban itu boleh digerakkan pada sela masa 15 saat dengan menganggapkan tiada kebocoran minyak? Piston pam mempunyai pukulan 7.62cm.*
- (iii) *Apakah output HP dengan menganggapkan kecekapan 90%?*



Rajah 1A (Figure 1A)

(50 markah)

- [b] For the hydraulic system of Figure 1B the following data are given:
- (i) the pump is adding 3.73 kW [pump hydraulic power =3.73 kW] to the fluid.
 - (ii) pump flow is $0.001896\text{m}^3/\text{s}$.
 - (iii) the pipe has a 0.0254 m inside diameter.
 - (iv) the specific gravity of the oil 0.9
 - (v) the elevation difference between station 1 and 2 is 6.096 m.

Find the pressure available at the inlet to the hydraulic motor [station 2]. The pressure at station 1 in the hydraulic tank is atmospheric [0 Pa, or 0 N/m^2]. The head loss H_L due to friction between station 1 and 2 is 9.144 m of oil.

Untuk sistem hidraulik pada Rajah 1B, data yang berikut diberikan:

- (i) Pam menambahkan 3.73kW [kuasa hidrolik pam = 3.73kW] kepada bendalir
- (ii) Aliran pam ialah $0.00189 \text{ m}^3/\text{s}$
- (iii) Paip mempunyai 0.0254 diameter dalaman
- (iv) Graviti spesifik minyak ialah 0.9
- (v) Perbezaan dongakan diantara stesen 1 dan 2 ialah 6.090m

Cari tekanan yang sesuai pada inlet kepada motor hidrolik [stesen 2]. Tekanan pada stesen 1 di dalam tank hidrolik ialah atmosferik [0 Pa, atau 0 N/m^2]. Kehilangan pada kepala, H_L kerana geseran di antara stesen 1 dan 2 ialah 9.144m daripada minyak.

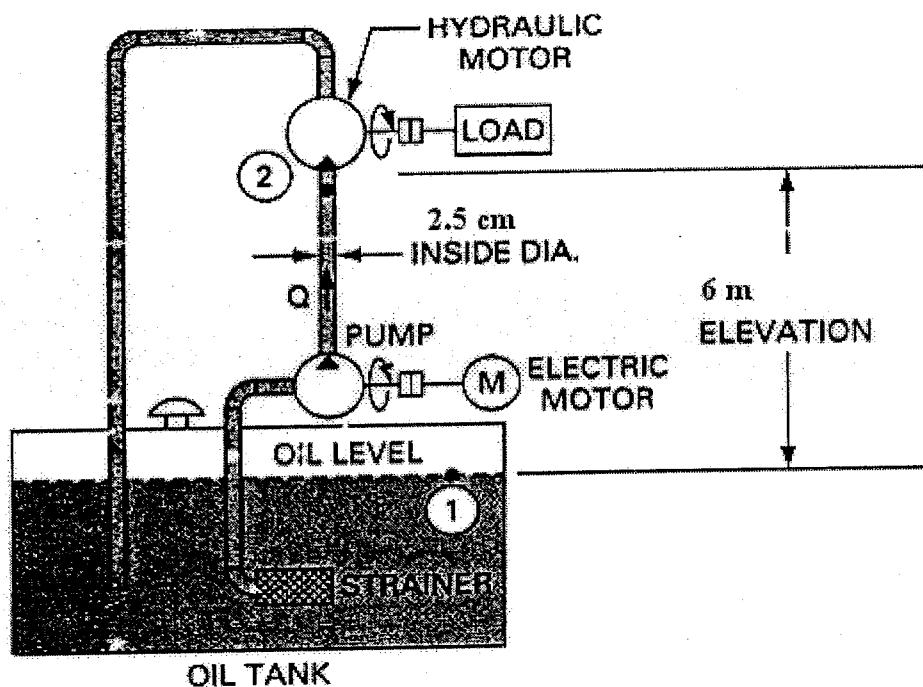


Figure 1B (*Rajah 1B*)

(50 markah)

2. [a] The oil tank for the hydraulic system of Figure 2A is air-pressurized at 10 psi. The inlet line to the pump is 10 ft below the oil level. The pump flow rate is 30 gpm. Find the pressure at station 2. The specific gravity of the oil is 0.90, and the kinematic viscosity of the oil is 100 cS. Assume that the pressure drop across the strainer is 1 psi. (1 in = 2.5cm and 1ft = 30cm), K factor for steel elbow = 0.9, water density = 62.4lb/ft³.

$$\text{Hint } N_R = [7740v \text{ ft.s}^{-1} \times D \text{ in}] / v \text{ (cS)}$$

Tangki minyak untuk sistem hidrolik pada Rajah 2A telah di bertekanan-udara pada 10 psi. Inlet pada talian kepada pam ialah 10 ft di bawah aras minyak. Kadar aliran pam ialah 30 gpm. Cari tekanan pada stesen 2. Graviti spesifik pada minyak ialah 0.90 dan kelikatan viskositi untuk minyak ialah 100cS. Andaikan penurunan tekanan pada penahan ialah 1 psi (1 in = 2.5cm and 1ft = 30cm), faktor K pada lengan keluli = 0.9, ketumpatan air 62.4lb/ft³.

$$\text{Panduan } N_R = (7740v \text{ ft.s}^{-1} \times D \text{ in}) / v \text{ (cS)}$$

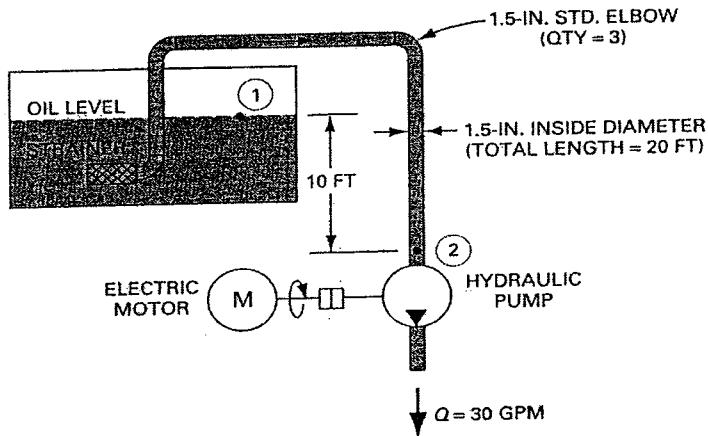


Figure 2A (Rajah 2A)

(50 markah)

... 26/-

- [b] A pump has a displacement volume of 100cm^2 . it delivers $0.0015\text{m}^3/\text{s}$ and 1000 rpm and 70 bars. If the prime mover input torque is 120N.m.
- what is the overall efficiency of the pump?
 - what is the theoretical torque required to operate the pump?

Pam mempunyai peralihan isipadu sebanyak 100cm^2 . Pam memngabantar $0.0015\text{m}^3/\text{s}$ dan 1000rpm dan 70 bars. Jika penggerak primier input kilasan ialah 120N.m.

- Apakah kecekapan keseluruhan pam?*
- Apakah pukulan theoritikal yang diperlukan untuk mengoperasi pam?*

(50 markah)

3. [a] For the fluid power system of Figure 3A, the following data are given:
- Cylinder piston diameter = 0.203m
Cylinder rod diameter = 0.102m
Extending speed of cylinder = 0.0762m/s
External load on cylinder = 178000N
Pump volumetric efficiency = 92%
Pump mechanical efficiency = 90%
Pump speed = 1800 rpm
Pump inlet pressure = - 27600Pa
- The total pressure drop in the line from the pump discharge port to the blank end of the cylinder is 517000Pa. The total pressure drop in the return line from the rod end of the cylinder is 345 000 Pa
- Determine the
- Volumetric displacement of the pump
 - Input HP required to drive the pump
 - Input torque required to drive the pump
 - Percentage of pump input power delivered to the load

...27/-

3. [a] Untuk sistem fluid pada Rajah 3A, data-data yang di bawah diberikan:

Diameter silinder piston = 0.203m

Diameter silinder rod = 0.102m

Kelajuan tambahan silinder = 0.0762m/s

Beban luaran pada silinder = 178000N

Kecekapan volumetrik pam = 92%

Kecekapan mekanikal pam = 90%

Kelajuan pam = 1800 rpm

Tekanan inlet pam = -27600 Pa

Jumlah kejatuhan tekanan di dalam talian daripada tempat pengeluaran ke hujung silinder yang kosong ialah 517000 Pa. Jumlah kejatuhan di dalam talian kembali daripada hujung rod silinder ialah 345 000 Pa.

Tentukan:

- (i) pengalihan volumetrik di dalam pam
- (ii) Input HP yang diperlukan untuk memacu pam
- (iii) Input kilasan yang diperlukan untuk memacu pam
- (iv) Peratusan kuasa input pam yang diberikan kepada beban

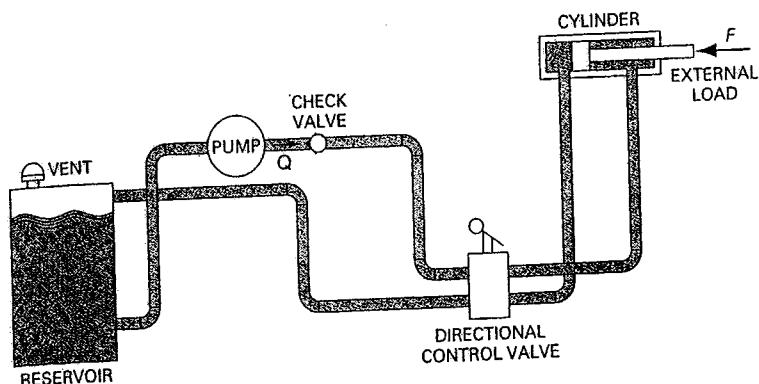


Figure 3A (Rajah 3A)

(50 markah)

...28/-

- [b] Determine the output pressure of a compressor operating with the following data:
- (i) Actual power required to drive the compressor is 20 kW.
 - (ii) Overall efficiency of the compressor is 75%.
 - (iii) Compressor delivers four standard m^3/min .
 - (iv) Compressor inlet pressure is 100 kPa abs.

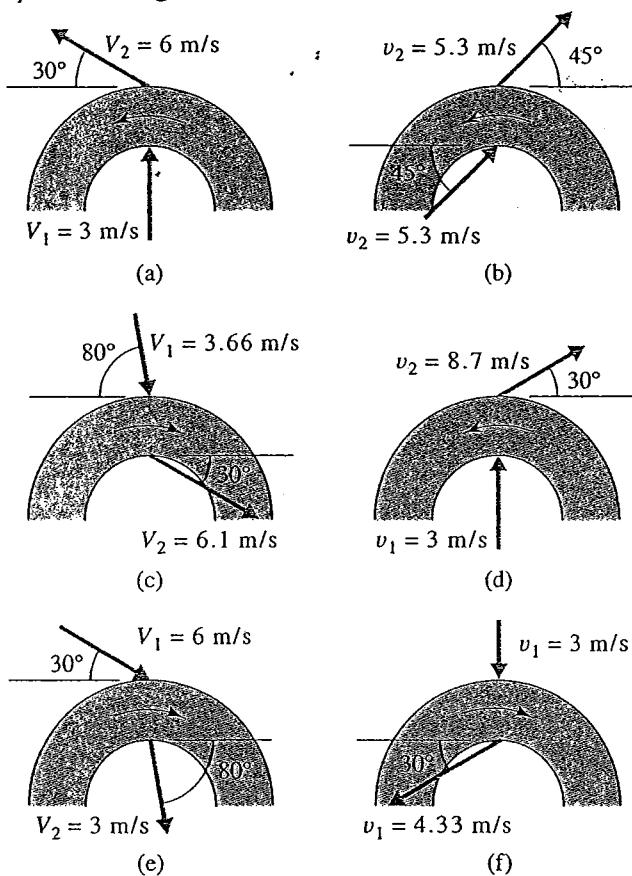
Tentukan tekanan output pada kompressor yang beroperasi dengan data-data berikut:

- (i) *Kuasa sebenar yang diperlukan untuk memacu kompresor pada 20kW*
- (ii) *Kecekapan keseluruhan kompresor ialah 75%*
- (iii) *Kompresor memberikan 4 standard m^3/min*
- (iv) *Tekanan inlet kompresor ialah 100 kPa abs.*

(50 markah)

4. Determine the torque, power and head input or output for each turbomachine shown below. Is a pump or turbine implied? The following data are in common: outer radius 300 mm, inner radius 150 mm, $Q = 0.057 \text{ m}^3/\text{s}$, $\rho = 1000 \text{ kg/m}^3$, and $\omega = 25 \text{ rad/s}$.

Tentukan kilasan, kuasa dan masukan atau keluaran turus untuk setiap mesin turbo yang ditunjukkan di bawah. Apakah yang dibayangkan itu pam atau turbin? Data berikut adalah umum: jejari luas 300 mm, jejari dalam 150 mm, $Q = 0.057 \text{ m}^3/\text{s}$, $\rho = 1000 \text{ kg/m}^3$ dan $\omega = 25 \text{ rad/s}$.



Figure

(100 markah)

...30/-

5. The following performance data were obtained from a test on a 216-mm double-entry centrifugal pump moving water at a constant speed of 1350 rev/min:

Data perlakuan berikut diperolehi dari ujian ke atas 216 mm pam empar masuk berkembar menggerakkan air pada kelajuan malar 1350 pusingan/min:

Q (m^3/min)	H (m)	η_p
0	12.2	0
0.454	12.8	0.26
0.905	13.1	0.46
1.36	13.4	0.59
1.81	13.4	0.70
2.27	13.1	0.78
2.72	12.2	0.78
3.80	11.0	0.74

Plot H versus Q , η_p versus Q , and W_p versus Q . If the pump operates in a system whose demand curve is given by $5 + Q^2$, find the discharge, head, and power required. In the demand curve, Q is given in cubic meters per minute.

Plotkan H melawan Q , η_p melawan Q dan W_p melawan Q . Jika pam beroperasi di dalam sistem di mana lengkung permintaan diberi sebagai $5 + Q^2$, tentukan discas, turus dan kuasa yang diperlukan. Pada lengkung permintaan Q diberi di dalam meter padu per minit.

6. Prepare dimensionless performance curves for the 205-mm-diameter radial flow pump of Figure 6.1. Compare these with the curves shown in Figure 6.2. Can you explain why there may be differences between the two sets of curves?

Sediakan lengkung perlakuan tanpa dimensi pam aliran jejarian bergaris pusat 205 mm bagi Rajah 6.1. Bandingkan lengkungan ini dengan lengkungan yang ditunjukkan dalam Rajah 6.2. Terangkan kenapa terdapat banyak perbezaan di antara kedua-dua set lengkung ini.

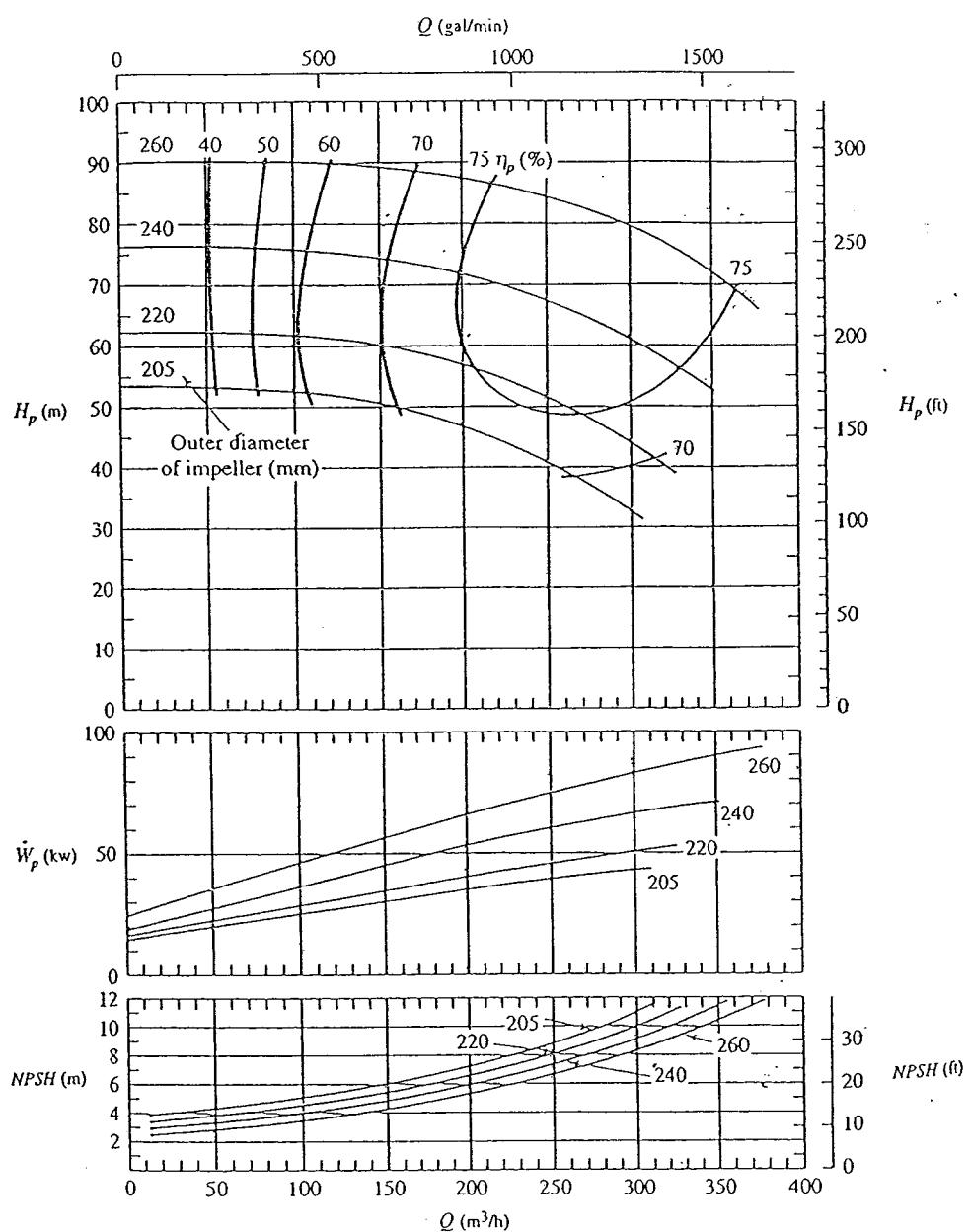


Figure 6.1 Radial-flow pump and performance curves for four different impellers with $N = 2900$ rpm, $\omega = 304$ rad/s. Water at 20°C is the pumped liquid.
(Courtesy of Sulzer Pumps Ltd.)