

Jun 1992

REG 462 - Rekabentuk Konkrit

Masa : 3 Jam

Sila pastikan bahawa kertas peperiksaan ini mengandungi **LIMABELAS** muka surat tercetak sebelum anda memulakan peperiksaan ini.

Jawab **LIMA** soalan sahaja.

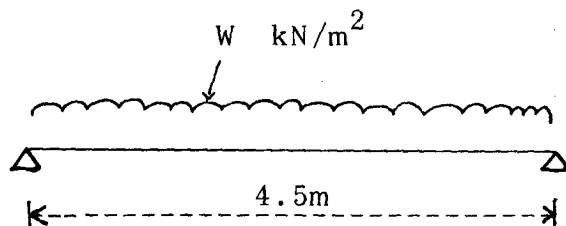
- (a) Apakah yang dimaksudkan dengan beban mati dan beban kenaan. Bagaimanakah beban reka bentuk diperolehi.
- (b) Papak konkrit disokong mudah dengan rentang sepanjang 4m dan memikul beban mati teragih bernilai 4.5 kN/m^2 , manakala beban hidup ialah 3.5 kN/m^2 .

Jika konkrit gred 25 digunakan ($f_{cu} = 25 \text{ N/mm}^2$) dan keluli lembut ($f_y = 250 \text{ N/mm}^2$) dipilih, tentukan tebal papak lantai dan tetulang keluli di dalamnya.

Lakarkan keratan papak dan tetulang yang ada padanya.

(20 markah)

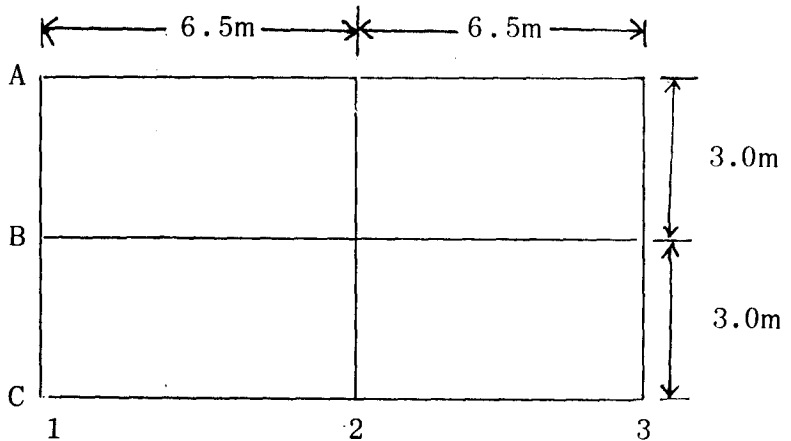
- Sebuah bumbung konkrit rata direka bentuk bagi memikul beban mati 4.5 kN/m^2 dan beban kenaan 4.0 kN/m^2 . Rentang bagi bumbung yang disokong mudah ialah 4.5m dan konkrit dari gred 25 digunakan.



Tentukan tebal bumbung konkrit dan tetulang yang diperlukan pada papak bumbung.

(20 markah)

3. Berdasarkan pelan lantai di dalam Rajah 1, tentukan momen, daya ricih dan seterusnya tetulang pada rasuk B/2-3. Beban reka bentuk daripada lantai ialah 10 kN/m^2 .



Rajah 1

(20 markah)

4. (a) Apakah fungsi tiang di dalam struktur bangunan. Bagaimanakah anda menakrifkan tiang pendek dan tiang langsing.
- (b) Jika piawaian BS 8110 menetapkan beban muktamad N_{muk} pada tiang konkrit yang dirembat dan dibebankan oleh beban paksian sebagai:-

$$N_{muk} = 0.4 f_{cu} A_c + 0.75 f_y A_{sc}$$

dan

$$A_c = \text{luas konkrit}$$

$$A_{sc} = \text{luas keratan keluli}$$

$$f_{cu} = \text{tegasan mampat kiub konkrit}$$

$$f_y = \text{tegasan alah keluli}$$

tentukan saiz tiang dan tetulang yang diperlukan bagi memikul beban bernilai 1800 kN. Andaikan konkrit dari gred 30 dan keluli lembut, $f_y = 250 \text{ N/mm}^2$. Tentukan saiz minimum rakap dan jarak di antara satu sama lain.

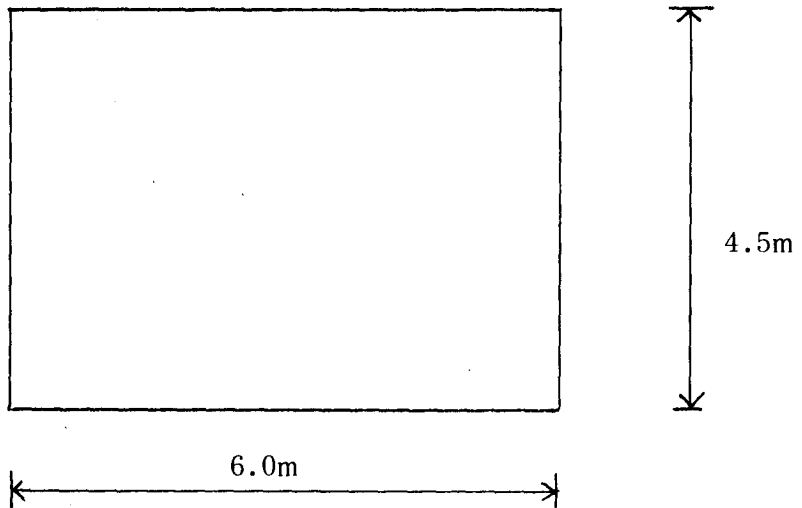
(20 markah)

...3/-

5. (a) Terangkan perbezaan di antara konkrit tetulang dengan ferosimen.
- (b) Bincangkan kegunaan utama ferosimen di dalam struktur bangunan, struktur marin dan juga pertanian.
- (c) Selain dari kadar campuran, kualiti struktur ferosimen bergantung juga pada kaedah memplaster. Terangkan kadar campuran yang sesuai untuk struktur marin serta langkah tambahan yang sangat diperlukan untuk menjamin ketahanan ferosimen.

(20 markah)

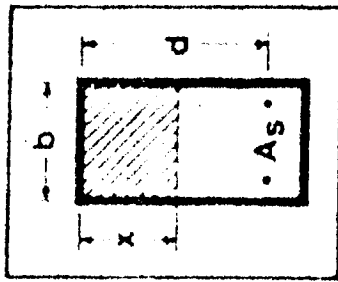
6. Sebuah lantai konkrit setebal 125mm disokong mudah di kedua-dua hujung. Papak lantai ini diperbuat dari konkrit gred 25 dan berukuran 4.5m lebar dan 6.0m panjang seperti di Rajah 2. Sekiranya beban kenaan untuk lantai ialah 3.5 kN/m^2 , tentukan momen lentur M_{sx} , M_{sy} dan tetulang yang diperlukan untuknya.



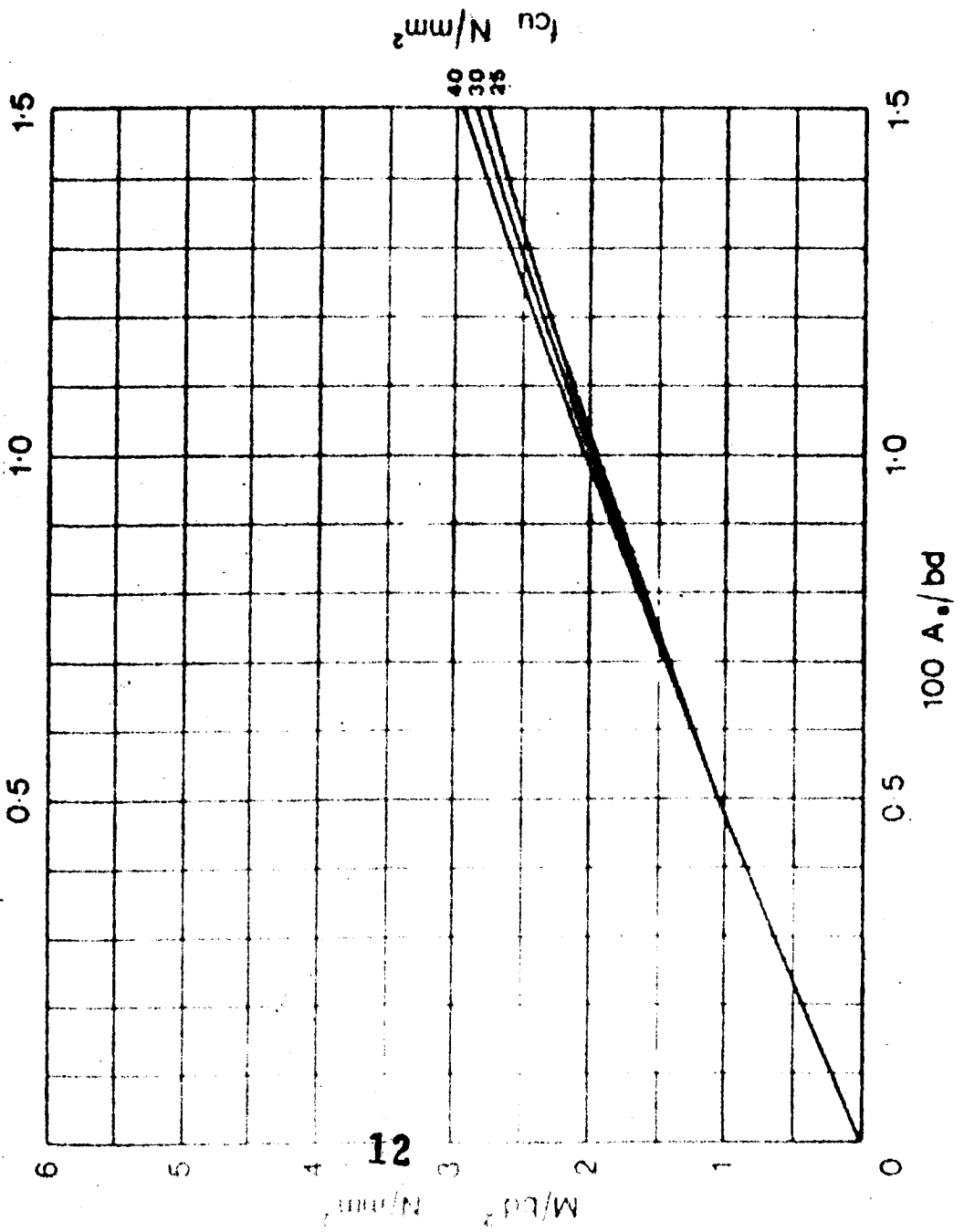
(20 markah)

Rajah 2

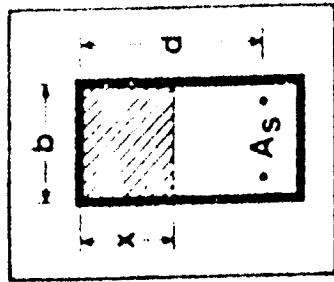
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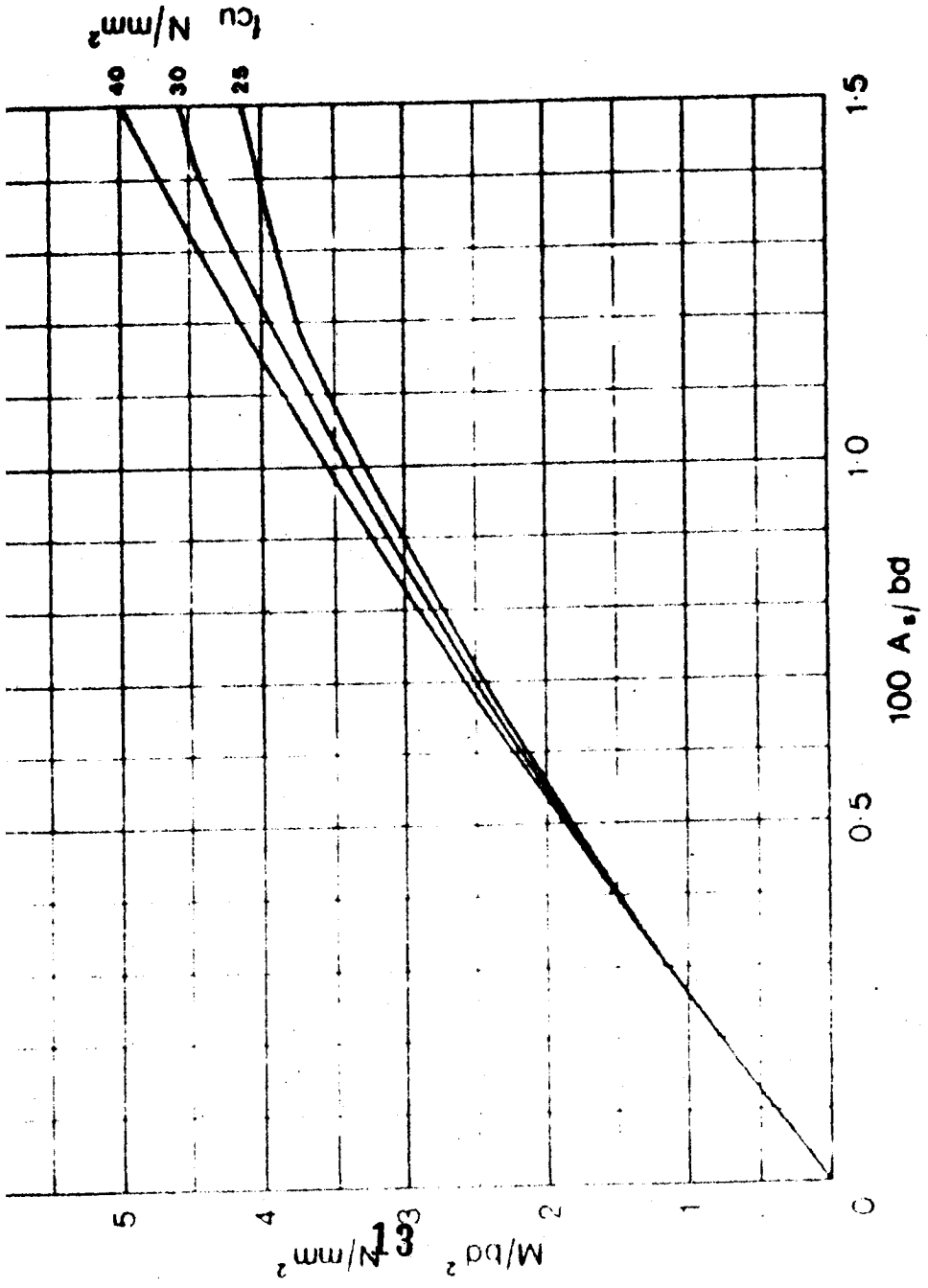
f_y 250



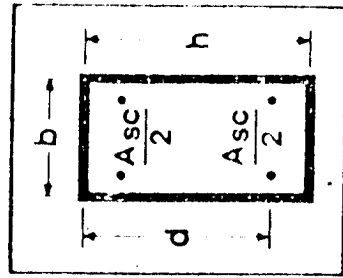
Singly reinforced beams



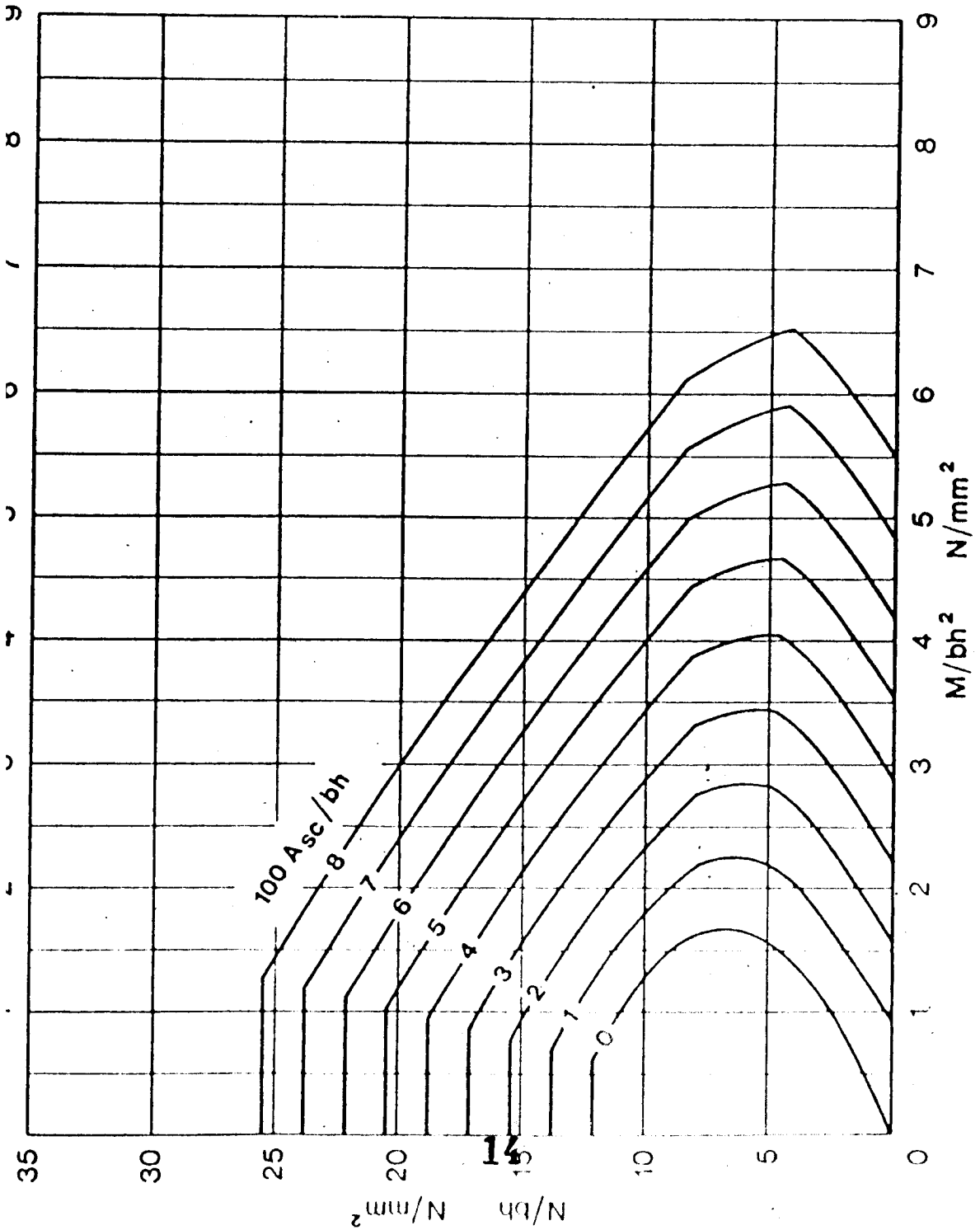
f_y 460



Singly reinforced beams

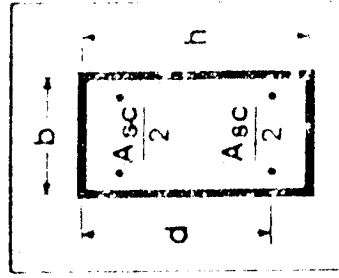


| | |
|----------|------|
| f_{cu} | 30 |
| f_y | 250 |
| d/h | 0.80 |

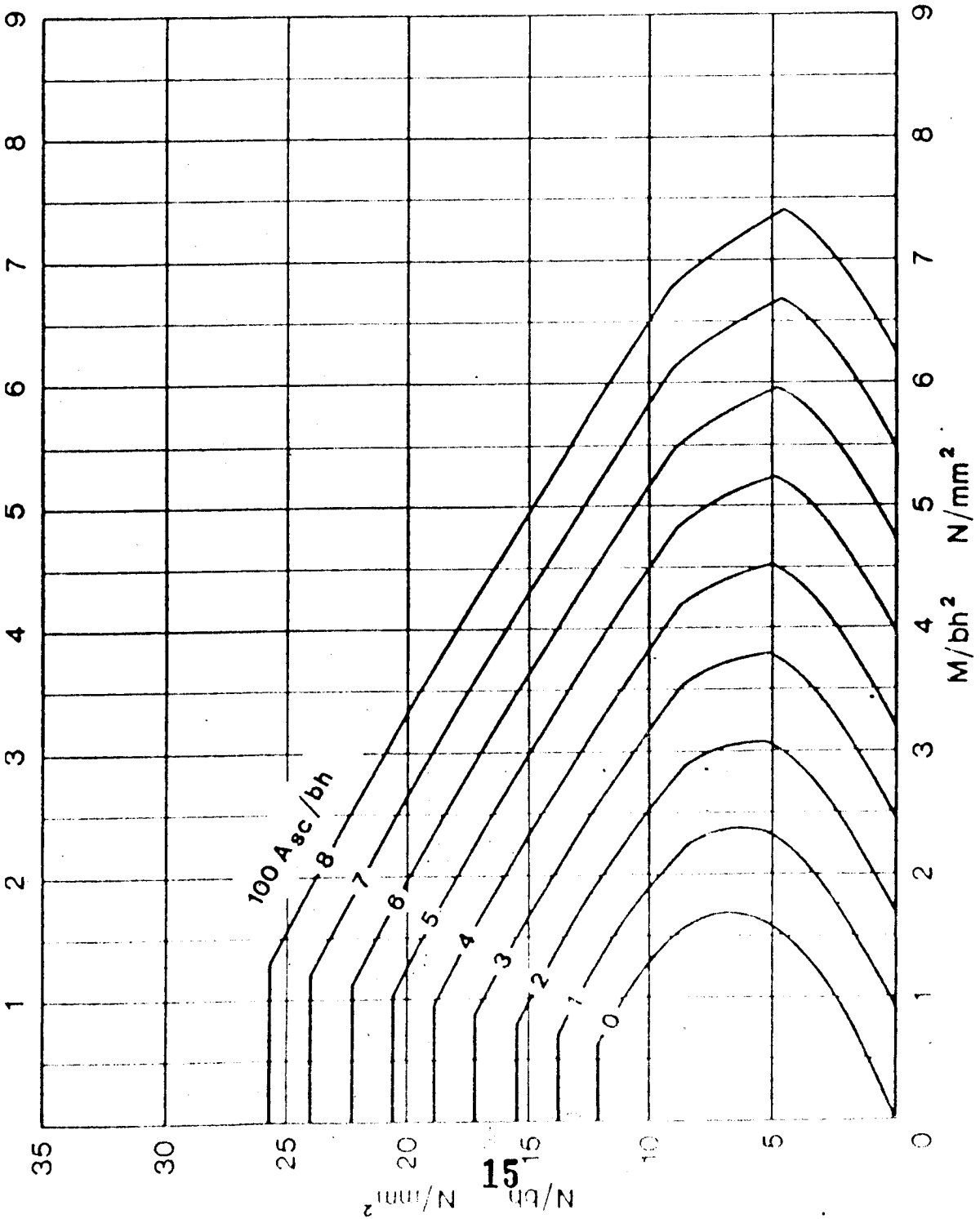


Rectangular columns

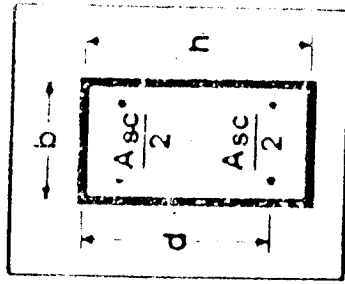
CP 110, Part 2, 1972



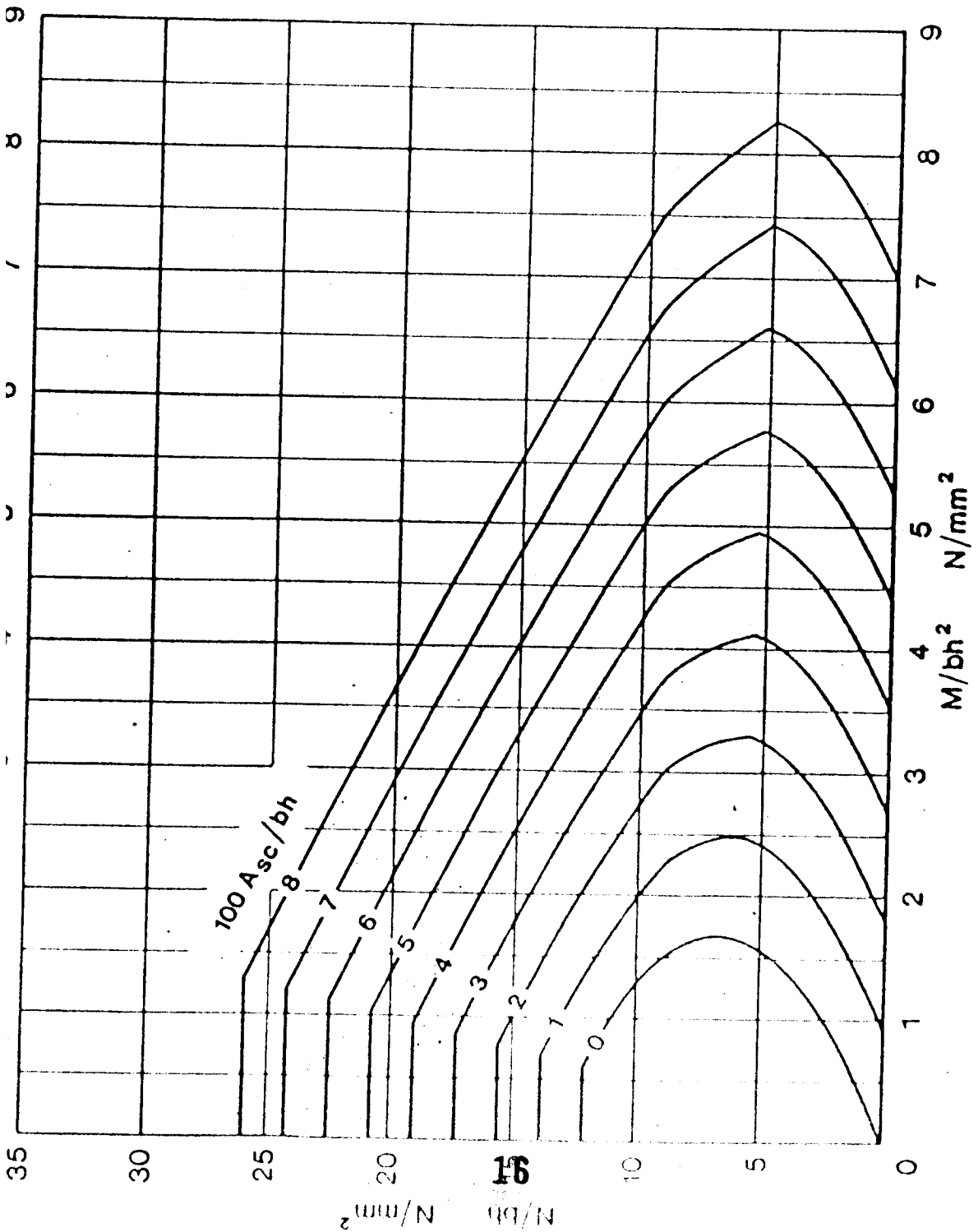
| | |
|----------|------|
| f_{cu} | 30 |
| f_y | 250 |
| d/h | 0.85 |



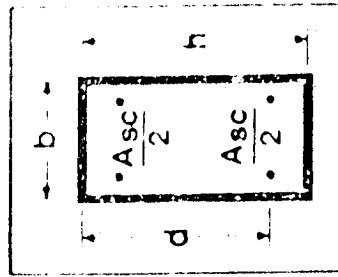
Rectangular columns



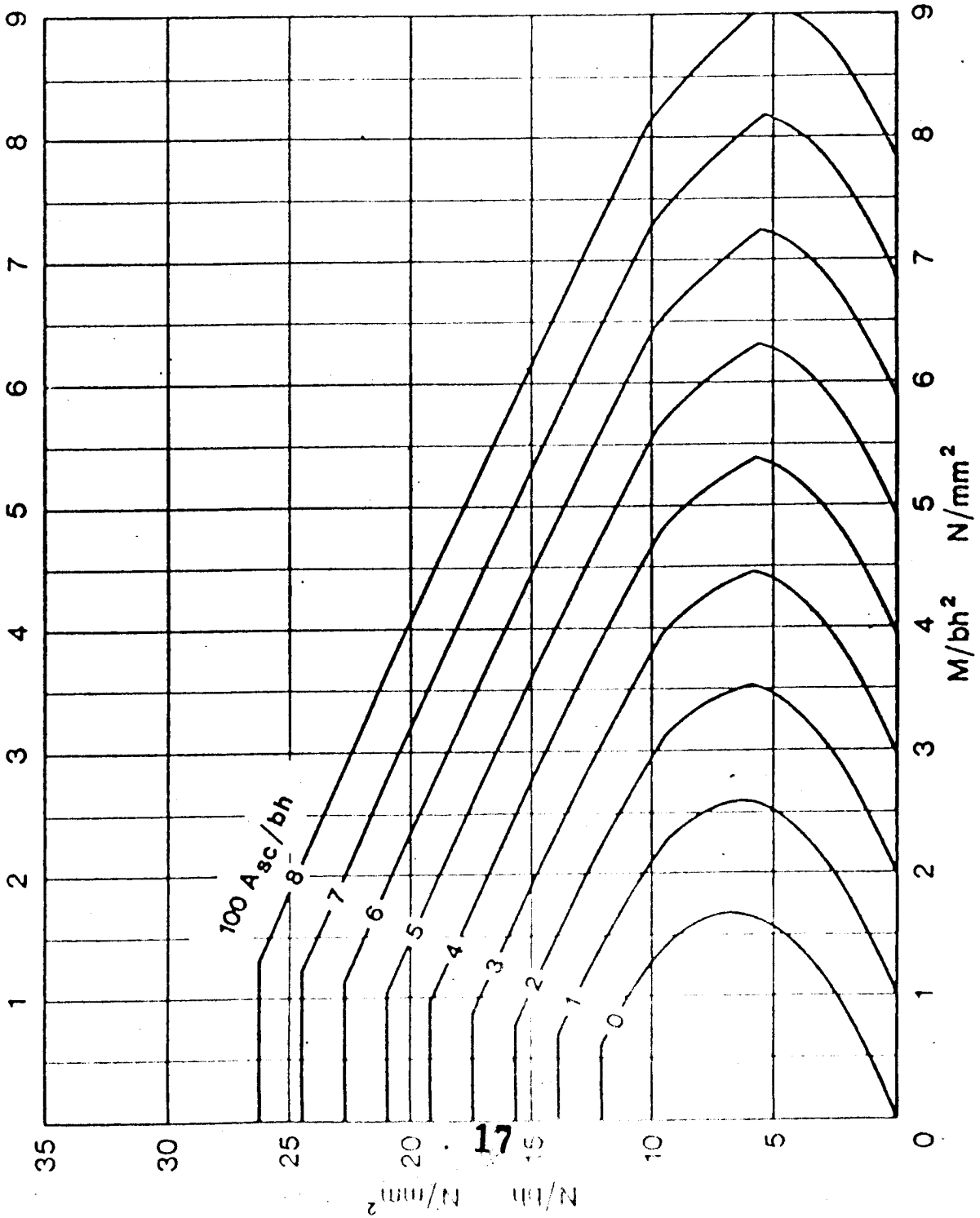
| | |
|----------|------|
| f_{cu} | 30 |
| f_y | 250 |
| d/h | 0.90 |



Rectangular columns

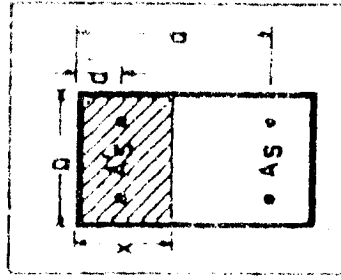


| | |
|----------|------|
| f_{cu} | 30 |
| f_y | 250 |
| d/h | 0.95 |

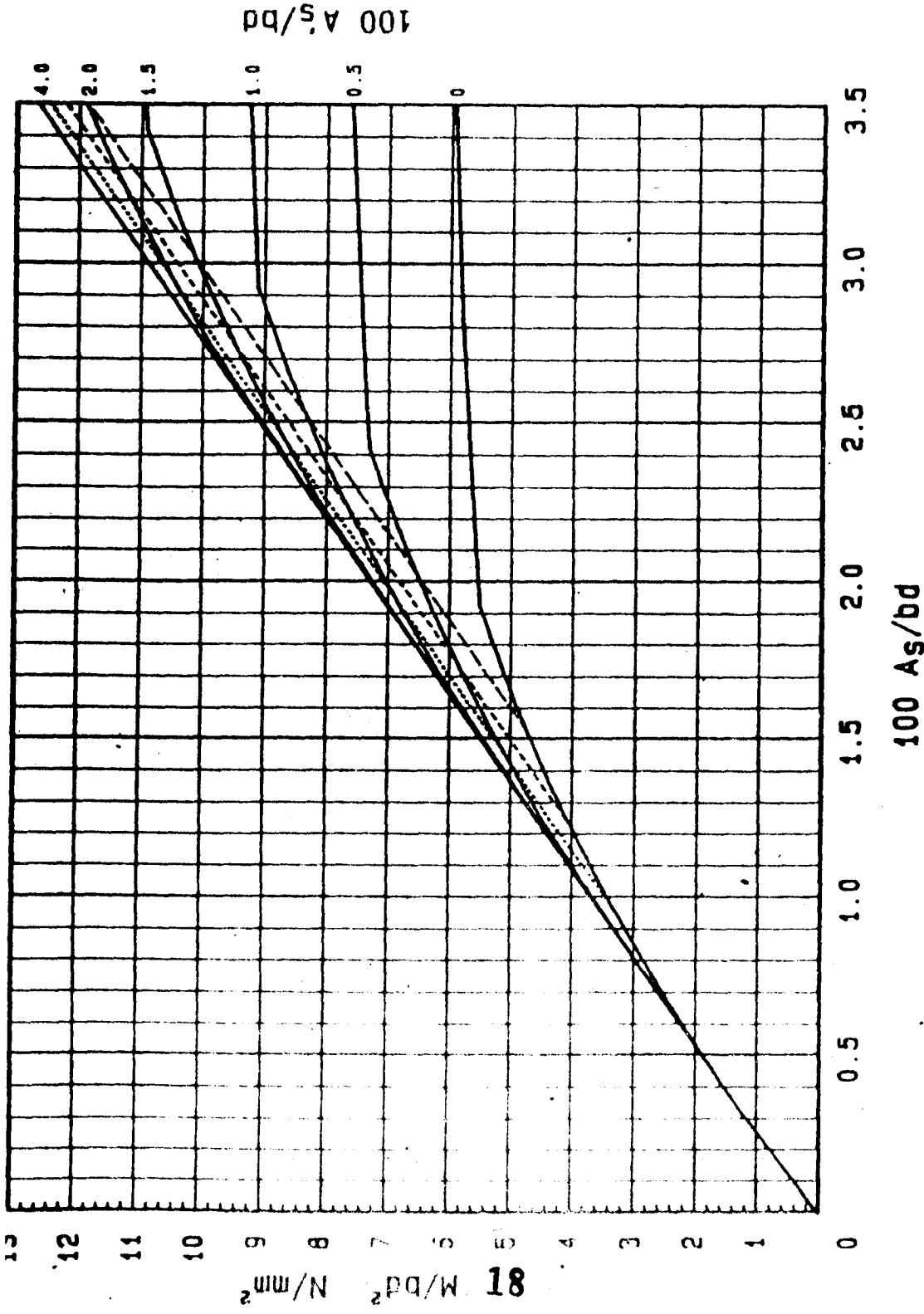


Rectangular columns

- $x/d = 0.3$ (dotted line)
- $x/d = 0.4$ - - - - - (dashed line)
- $x/d = 0.5$ - - - - - (dash-dot line)

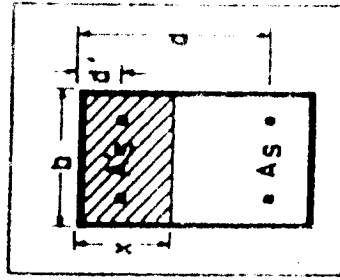


| | |
|----------|------|
| f_{cu} | 30 |
| f_y | 460 |
| d'/d | 0.10 |

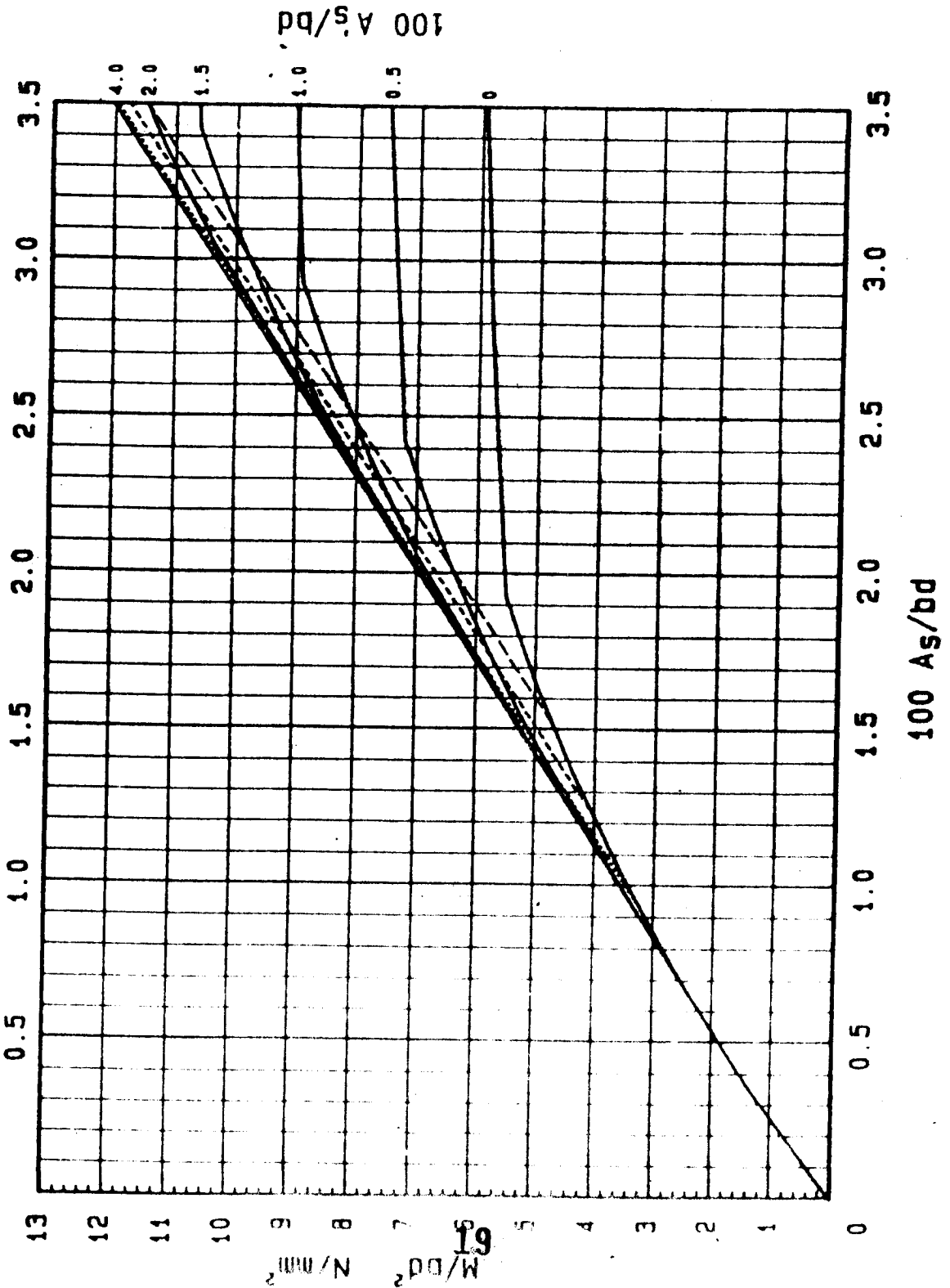


Doubly reinforced beams

- $x/d = 0.3$ (dotted line)
- $x/d = 0.4$ - - - - (dashed line)
- $x/d = 0.5$ - - - - (dash-dot line)

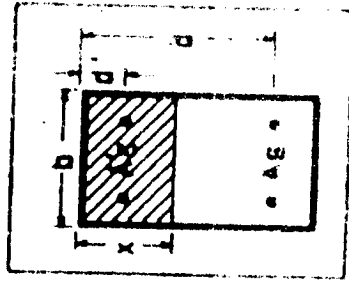


| | |
|----------|------|
| f_{cu} | 30 |
| f_y | 480 |
| d'/d | 0.15 |

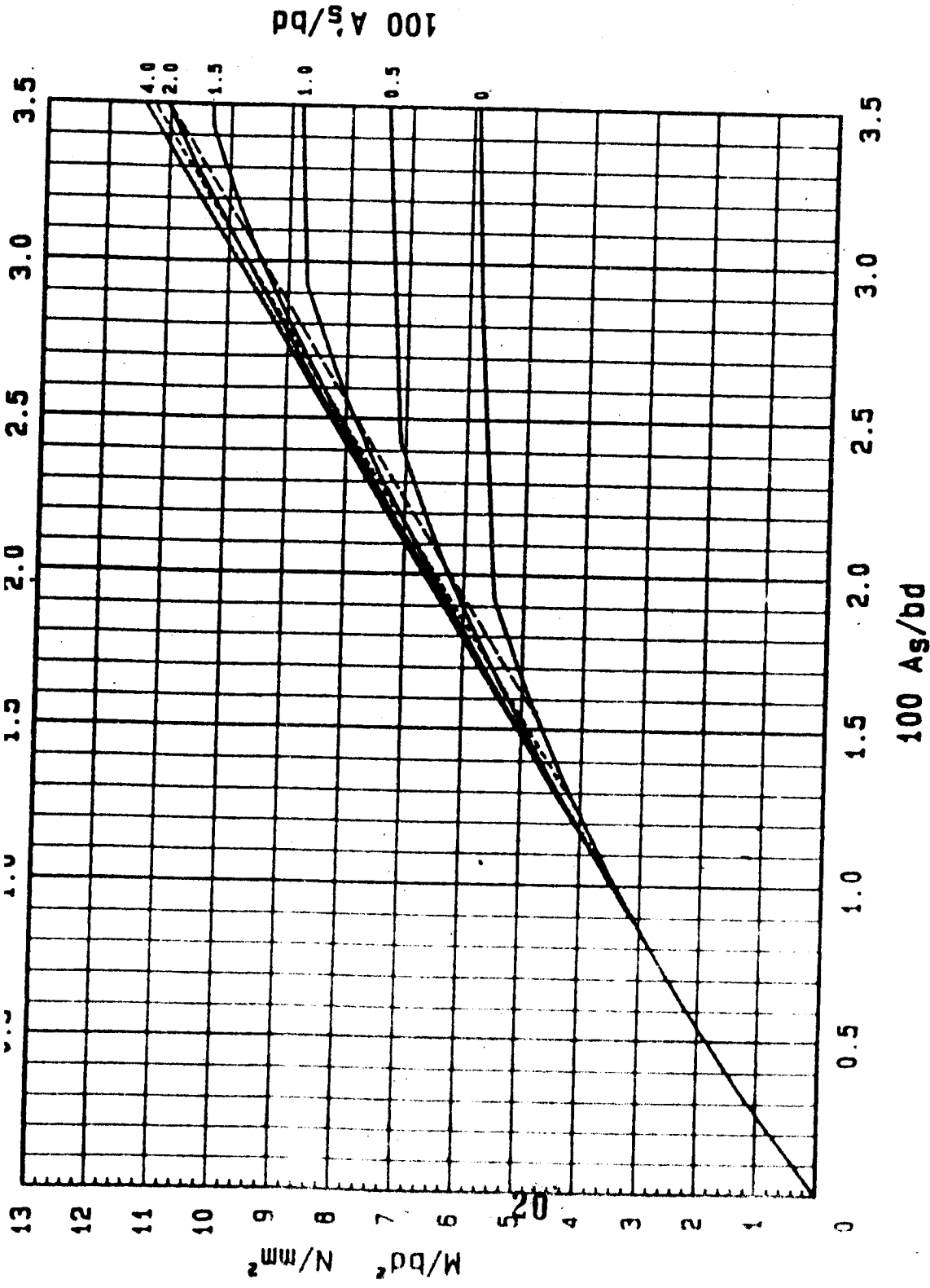


Doubly reinforced beams

- $x/d = 0.3$ (dotted line)
- $x/d = 0.4$ - - - - (dashed line)
- $x/d = 0.5$ - - - - (dash-dot line)



| | |
|----------|------|
| f_{cu} | 30 |
| f_y | 460 |
| d'/d | 0.20 |



Doubly reinforced beams

Table 2. Strength of concrete

| Grade | Characteristic strength f_{cu} | Cube strength at an age of | | | | |
|-------|----------------------------------|----------------------------|-------------------|-------------------|-------------------|-------------------|
| | | 7 days | 2 months | 3 months | 6 months | 1 year |
| | N/mm ² | N/mm ² | N/mm ² | N/mm ² | N/mm ² | N/mm ² |
| 20 | 20.0 | 13.5 | 22 | 23 | 24 | 25 |
| 25 | 25.0 | 16.5 | 27.5 | 29 | 30 | 31 |
| 30 | 30.0 | 20 | 33 | 35 | 36 | 37 |
| 40 | 40.0 | 28 | 44 | 45.5 | 47.5 | 50 |
| 50 | 50.0 | 36 | 54 | 55.5 | 57.5 | 60 |

Design may be based on the characteristic strength or, if appropriate, the strength given in Table 2 for the age of loading.

Table 4. Ultimate bending moments and shear forces

| | At outer support | Near middle of end span | At first interior support | At middle of interior spans | At interior supports |
|--------|------------------|-------------------------|---------------------------|-----------------------------|----------------------|
| Moment | 0 | $\frac{Fl}{11}$ | $-\frac{Fl}{9}$ | $\frac{Fl}{14}$ | $-\frac{Fl}{10}$ |
| Shear | $0.45F$ | — | $0.6F$ | — | $0.55F$ |

In Table 4, l is the effective span and F is the total ultimate load ($1.4G_k + 1.6Q_k$). No redistribution of the moments found from Table 4 should be made.

Table 8. Basic span/effective depth ratios for rectangular beams

| Support conditions | Ratio |
|--------------------|-------|
| Cantilever | 7 |
| Simply supported | 20 |
| Continuous | 26 |

Table 10. Modification factor for tension reinforcement

| Service stress (f_s) | $\frac{100A_s}{bd}$ | | | | | | | |
|--------------------------|---------------------|------|------|------|------|------|------|-------|
| | 0.25 | 0.50 | 0.75 | 1.00 | 1.50 | 2.00 | 2.50 | > 3.0 |
| N/mm ² | | | | | | | | |
| 145 ($f_y = 250$) | 2.0 | 1.98 | 1.62 | 1.44 | 1.24 | 1.13 | 1.06 | 1.01 |
| 150 | 2.0 | 1.91 | 1.58 | 1.41 | 1.22 | 1.11 | 1.04 | 0.99 |
| 200 | 2.0 | 1.46 | 1.26 | 1.15 | 1.02 | 0.94 | 0.89 | 0.85 |
| 238 ($f_y = 410$) | 1.60 | 1.23 | 1.09 | 1.00 | 0.90 | 0.84 | 0.80 | 0.77 |
| 246 ($f_y = 425$) | 1.55 | 1.20 | 1.06 | 0.98 | 0.88 | 0.83 | 0.79 | 0.76 |
| 250 | 1.52 | 1.18 | 1.05 | 0.97 | 0.87 | 0.82 | 0.78 | 0.75 |
| 267 ($f_y = 460$) | 1.41 | 1.11 | 0.99 | 0.92 | 0.84 | 0.78 | 0.75 | 0.72 |
| 290 ($f_y = 500$) | 1.27 | 1.03 | 0.92 | 0.86 | 0.79 | 0.74 | 0.71 | 0.68 |
| 300 | 1.22 | 0.99 | 0.90 | 0.84 | 0.77 | 0.72 | 0.69 | 0.67 |

Table 11. Modification factor for compression reinforcement

| $\frac{100A_s'}{bd}$ | Factor |
|----------------------|--------|
| 0.25 | 1.07 |
| 0.50 | 1.14 |
| 0.75 | 1.20 |
| 1.0 | 1.25 |
| 1.5 | 1.33 |
| 2.0 | 1.40 |
| > 3.0 | 1.50 |

Intermediate values may be interpolated

Table 12. Bending moment coefficients for slabs spanning in two directions at right angles, simply supported on four sides

| l_x/l_y | 1.0 | 1.1 | 1.2 | 1.3 | 1.4 | 1.5 | 1.75 | 2.0 | 2.5 | 3.0 |
|---------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| α_{xx} | 0.062 | 0.074 | 0.084 | 0.093 | 0.099 | 0.104 | 0.113 | 0.118 | 0.122 | 0.124 |
| α_{yy} | 0.062 | 0.061 | 0.059 | 0.055 | 0.051 | 0.046 | 0.037 | 0.029 | 0.020 | 0.014 |

$$M_{xx} = \alpha_{xx} n l_x^2 \quad (14)$$

$$M_{yy} = \alpha_{yy} n l_y^2 \quad (15)$$

where M_{xx} and M_{yy} are the maximum moments at mid span on strips of unit width and spans l_x and l_y , respectively,

n is the total ultimate load per unit area ($1.6g_k + 1.6q_k$),

l_y is the length of the longer side,

l_x is the length of the shorter side,

α_{xx} and α_{yy} are moment coefficients shown in Table 12.

Floor and Roof Loads

| | kN/m ² |
|-------------------------|-------------------|
| Classrooms | 3.0 |
| Dance halls | 5.0 |
| Flats and houses | 1.5 |
| Garages, passenger cars | 2.5 |
| Gymnasiums | 5.0 |
| Hospital wards | 2.0 |
| Hotel bedrooms | 2.0 |
| Offices for general use | 2.5 |
| Flat roofs, with access | 1.5 |
| Flat roofs, no access | 0.75 |

Sectional Areas per Metre Width for Various Bar Spacings (mm²)

| Bar size (mm) | Spacing of bars | | | | | | | | |
|---------------|-----------------|-------|-------|-------|------|------|------|------|------|
| | 90 | 75 | 100 | 125 | 150 | 175 | 200 | 250 | 300 |
| 6 | 566 | 377 | 283 | 226 | 189 | 162 | 142 | 113 | 94 |
| 8 | 1010 | 671 | 503 | 402 | 335 | 287 | 252 | 201 | 168 |
| 10 | 1570 | 1050 | 785 | 628 | 523 | 449 | 393 | 314 | 262 |
| 12 | 2260 | 1510 | 1130 | 905 | 754 | 646 | 566 | 452 | 377 |
| 16 | 4020 | 2680 | 2010 | 1610 | 1340 | 1150 | 1010 | 804 | 670 |
| 20 | 6280 | 4190 | 3140 | 2510 | 2090 | 1800 | 1570 | 1260 | 1050 |
| 25 | 9820 | 6550 | 4910 | 3930 | 3270 | 2810 | 2450 | 1960 | 1640 |
| 32 | 16100 | 10700 | 8040 | 6430 | 5360 | 4600 | 4020 | 3220 | 2680 |
| 40 | 25100 | 16800 | 12600 | 10100 | 8380 | 7180 | 6280 | 5030 | 4190 |

Bar Area and Perimeters

Sectional Areas of Groups of Bars (mm²)

| Bar size (mm) | Number of bars | | | | | | | | | |
|---------------|----------------|------|------|------|------|------|------|-------|-------|-------|
| | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | |
| 6 | 28.3 | 56.6 | 84.9 | 113 | 142 | 170 | 198 | 226 | 255 | 283 |
| 8 | 50.3 | 101 | 151 | 201 | 252 | 302 | 352 | 402 | 453 | 503 |
| 10 | 78.5 | 157 | 236 | 314 | 393 | 471 | 550 | 628 | 707 | 785 |
| 12 | 113 | 226 | 339 | 452 | 566 | 679 | 792 | 905 | 1020 | 1130 |
| 16 | 201 | 402 | 603 | 804 | 1010 | 1210 | 1410 | 1610 | 1810 | 2010 |
| 20 | 314 | 628 | 943 | 1260 | 1570 | 1890 | 2200 | 2510 | 2830 | 3140 |
| 25 | 491 | 982 | 1470 | 1960 | 2450 | 2950 | 3440 | 3930 | 4420 | 4910 |
| 32 | 804 | 1610 | 2410 | 3220 | 4020 | 4830 | 5630 | 6430 | 7240 | 8040 |
| 40 | 1260 | 2510 | 3770 | 5030 | 6280 | 7540 | 8800 | 10100 | 11300 | 12600 |

Perimeters and Weights of Bars

| Bar size (mm) | 6 | 8 | 10 | 12 | 16 | 20 | 25 | 32 | 40 |
|----------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Perimeter (mm) | 18.85 | 25.1 | 31.4 | 37.7 | 50.3 | 62.8 | 78.5 | 100.5 | 125.6 |
| Weight (kg/m) | 0.222 | 0.395 | 0.616 | 0.888 | 1.579 | 2.466 | 3.824 | 6.313 | 9.864 |

Shear Reinforcement

A_{sv}/b_s for Varying Stirrup Diameter and Spacing

| Stirrup diameter (mm) | Stirrup spacing (mm) | | | | | | | | | |
|-----------------------|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | 85 | 90 | 100 | 125 | 150 | 175 | 200 | 225 | 250 | 275 |
| 8 | 1.183 | 1.118 | 1.006 | 0.805 | 0.671 | 0.575 | 0.503 | 0.447 | 0.402 | 0.366 |
| 10 | 1.847 | 1.744 | 1.57 | 1.256 | 1.047 | 0.897 | 0.785 | 0.698 | 0.628 | 0.571 |
| 12 | 2.659 | 2.511 | 2.26 | 1.808 | 1.507 | 1.291 | 1.13 | 1.004 | 0.904 | 0.822 |
| 16 | 4.729 | 4.467 | 4.02 | 3.216 | 2.68 | 2.297 | 2.01 | 1.787 | 1.608 | 1.462 |