

---

**UNIVERSITI SAINS MALAYSIA**

Semester I Examination  
Academic Session 2007/2008

October/November 2007

**EEE 532 – MICROWAVE CIRCUIT DESIGN**

Time : 2 hours

---

**INSTRUCTION TO CANDIDATE:**

Please ensure that this examination paper contains **THIRTEEN (13)** printed pages including Appendices (9 pages) and **SIX (6)** questions before answering.

This question paper has three sections, **Section A**, **Section B** and **Section C**.

Answer **ONE (1)** questions in **Section A**, **Section B** and **Section C**.

**ONE (1)** question from any **Section**. Answer **FOUR (4)** questions.

Use three answer booklets which is provided where the answer for questions in **Section A, B and C** are in difference answer booklets.

Distribution of marks for each question is given accordingly.

All questions must be answered in English.

**Section A: Answer ONE (1) question.**

1. (a) Derive the  $[Z]$  matrix for the following two port network in Figure 1.

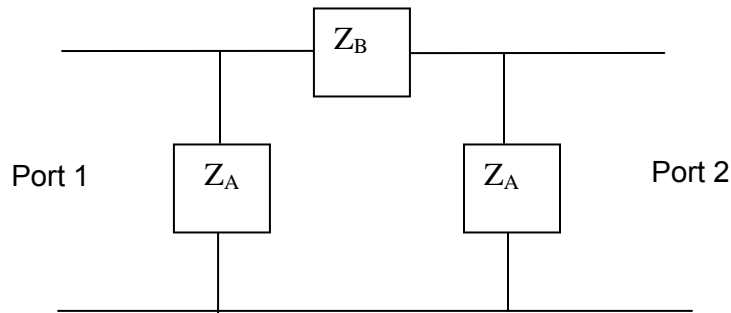


Figure 1.

(15%)

- (b) Consider a lossless two-port network.

- (i) If the network is reciprocal, show that  $|S_{21}|^2 = 1 - |S_{11}|^2$ .
- (ii) If the network is nonreciprocal, show that it is impossible to have unidirectional transmission where  $S_{12} = 0$  and  $S_{21} \neq 0$ .

(10%)

2. Design a Butterworth lowpass filter with a cutoff frequency of 1 GHz at 3dB and attenuation level greater than 20 dB at 2.5 GHz. The filter is design on the printed circuit board with a dielectric constant,  $\epsilon_r = 2.5$  and impedance  $Z_0 = 50 \Omega$ .

(25%)

**Section B: Answer ONE (1) question.**

3. (a) Design a matching sections using a quarter-wave transformer to match a load of  $Z_L = 100 + j50$  ohm to a 50 ohm line at frequency of 1 GHz.

(10 marks)

- (b) If the same load is to be matched with 50 ohm line using a three-sections maximally flat quarter – wave transformer, calculate all the characteristic impedance of the three sections.

(15 marks)

4. Design a 15dB broadband 3 sections maximally flat coupled line coupler using a substrate of  $\epsilon_r=4.5$  and thickness of 1.5 mm with center frequency of 2 GHz. The input of all ports are to be 50 ohm . Given that the voltage expression at port 3 in terms of port 1 is

$$V_3 = 2jV_1 \sin \theta e^{-jN\theta} \left[ C_1 \cos(N-1)\theta + C_2 \cos(N-3)\theta + \dots \frac{1}{2} C_M \right]$$

where N=number of section ,  $M=(N+1)/2$  ,  $C_o = \left| \frac{V_3}{V_1} \right|_{\theta=\pi/2}$

Assume that the coupler is symmetrical such that  $C_1 = C_N$ ,  $C_2 = C_{N-1}$  etc

Using the following formula

$$Z_{oe} = Z_o \sqrt{\frac{1+C}{1-C}}$$

$$Z_{oo} = Z_o \sqrt{\frac{1-C}{1+C}}$$

$$\frac{1}{2}(Z_{oc} - Z_{oo}) = JZ_o$$

and the graph in Appendix 2 calculate the microstripline dimension , s and w of the above coupler.

(25 marks)

...4/-

**Section C: Answer ONE (1) question.**

5. Referring to the ATF 36077 datasheet as in Appendix 3, using the S parameter at 7 GHz. The source impedance is  $Z_S = 40\Omega$  and the load impedance is  $Z_L = 60\Omega$ . Calculate:

- (i) Power Gain. (5 Marks)
- (ii) Available Gain. (5 Marks)
- (iii) Transducer power gain. (5 Marks)
- (iv) Determine the transistor stability. (10 Marks)

6. (a) Referring to Figure 2, explain the operation of the circuit. (10 Marks)

(b) Using the S parameter as in Question 5, design a Low Noise Amplifier operating at 4 GHz having a noise figure of 4 dB. Use single stub matching for the input and quarter wave transformer matching at the output. Use  $C_i$  as your  $\Gamma_S$ . Microwave laminate is Ultralam 2000 having a dielectric constant of 2.45, a thickness of 0.5 mm and copper thickness of 35  $\mu\text{m}$ .

(15 Marks)

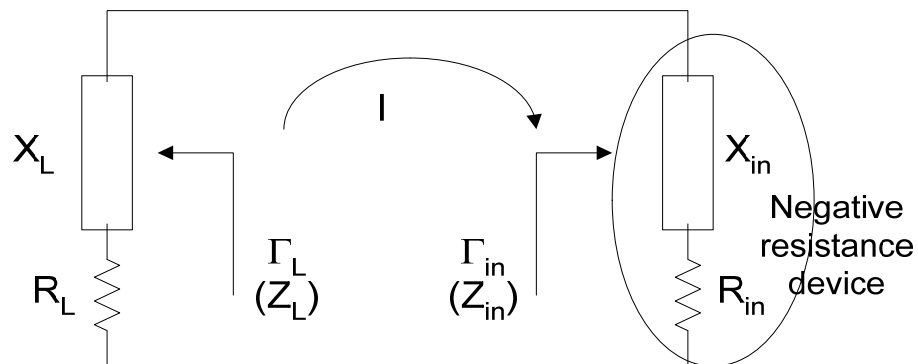


Figure 2

ooo0ooo

**LNA DESIGN**

$$C_i = \frac{\Gamma_{opt}}{(1 + N_i)}$$

$$R_i = \frac{1}{(1 + N_i)} \sqrt{N_i^2 + N_i(1 - |\Gamma_{opt}|^2)}$$

$$N_i = \frac{\left[ (F_r - F_{min}) |1 + \Gamma_{opt}|^2 \right]}{4r_n}$$

$$\Gamma_L = \left( S_{22} + \frac{S_{12} S_{21} \Gamma_{in}}{1 - S_{11} \Gamma_{in}} \right)^*$$

**Important Formulas:****Network parameters****S=parameter**

$$S_{11} = \left. \frac{V_{r1}}{V_{i1}} \right|_{V_{r2}=0} \quad S_{12} = \left. \frac{V_{t2}}{V_{i2}} \right|_{V_{r2}=0} \quad S_{21} = \left. \frac{V_{t1}}{V_{i1}} \right|_{V_{r1}=0} \quad S_{22} = \left. \frac{V_{r2}}{V_{i2}} \right|_{V_{r1}=0}$$

**ABCD parameter**

$$A = \left. \frac{V_1}{V_2} \right|_{I_2=0} \quad B = \left. \frac{V_1}{-I_2} \right|_{V_2=0} \quad C = \left. \frac{I_1}{V_2} \right|_{I_2=0} \quad D = \left. \frac{I_1}{-I_2} \right|_{V_2=0}$$

**Conversion**

$$\begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix} = \frac{1}{Z_o A + B + Z_o^2 C + Z_o D} \begin{bmatrix} Z_o A + B - Z_o^2 C - Z_o D & 2Z_o(AD - BC) \\ 2Z_o & -Z_o A + B - Z_o^2 C + Z_o D \end{bmatrix}$$

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \frac{1}{2S_{21}} \begin{bmatrix} (1 + S_{11})(1 - S_{22}) + S_{12}S_{21} & Z_o((1 + S_{11})(1 + S_{22}) - S_{12}S_{21}) \\ \frac{1}{Z_o}((1 - S_{11})(1 - S_{22}) - S_{12}S_{21}) & (1 - S_{11})(1 + S_{22}) + S_{12}S_{21} \end{bmatrix}$$

**Butterworth lowpass filter**

$$g_k = 2 \sin(2k - 1) \frac{\pi}{2n} \text{ where } k=1, \dots, n$$

$$g_0 = g_{n+1} = 1$$

$$n = \frac{\log_{10}(10^{A/10} - 1)}{2 \log_{10}(\omega / \omega_c)}$$

$$C_k = \frac{g_k}{Z_o \omega_c}$$

$$L_k = \frac{Z_o g_k}{\omega_c}$$

**Bandpass filter**

$$J_{01} = \left( \frac{\pi \Omega}{2g_0 g_1} \right)^{\frac{1}{2}}$$

$$J_{k,k+1} = \left( \frac{\pi \Omega}{2} \right) \frac{1}{\sqrt{g_k \cdot g_{k+1}}} \quad \text{where } k=1, \dots, n$$

$$J_{n,n+1} = \left( \frac{\pi \Omega}{2g_n \cdot g_{n+1}} \right)$$

**Amplifier design****Unilateral**

$$\Gamma_S = \left( \frac{Z_S - Z_O}{Z_S + Z_O} \right) \quad \Gamma_L = \left( \frac{Z_L - Z_O}{Z_L + Z_O} \right)$$

$$\Gamma_{in} = \left( S_{11} + \frac{S_{12}S_{21}\Gamma_L}{1 - S_{22}\Gamma_L} \right) \quad \Gamma_{out} = \left( S_{22} + \frac{S_{12}S_{21}\Gamma_S}{1 - S_{11}\Gamma_S} \right)$$

**Stability:**

$$K = \frac{1 - |S_{11}|^2 - |S_{22}|^2 + |D|^2}{2|S_{12}S_{21}|}$$

$$D = S_{11}S_{22} - S_{12}S_{21}$$

**Power gain:**

$$G = \left( \frac{|S_{21}|^2 (1 - |\Gamma_L|^2)}{(1 - |\Gamma_{in}|^2) |1 - S_{22}\Gamma_L|^2} \right)$$

**Available Power gain:**

$$G_A = \left( \frac{|S_{21}|^2 (1 - |\Gamma_S|^2)}{|1 - S_{11}\Gamma_S|^2 (1 - |\Gamma_{out}|^2)} \right)$$

**Transducer Power Gain:**

$$G_T = \frac{|S_{21}|^2 (1 - |\Gamma_S|^2) (1 - |\Gamma_L|^2)}{|1 - \Gamma_S \Gamma_{in}|^2 |1 - S_{22}\Gamma_L|^2}$$

**Bilateral**

$$\Delta = S_{11}S_{22} - S_{12}S_{21}$$

$$K = \frac{1 - |S_{11}|^2 - |S_{22}|^2 + |\Delta|}{2|S_{12}S_{21}|}$$

$$\Gamma_S = \frac{B_1 \pm \sqrt{B_1^2 - 4|C_1|^2}}{2C_1}$$

$$B_1 = 1 + |S_{11}|^2 - |S_{22}|^2 - |\Delta|^2$$

$$C_1 = S_{11} - \Delta S_{22}^*$$

$$\Gamma_L = \frac{B_2 \pm \sqrt{B_2^2 - 4|C_2|^2}}{2C_2}$$

$$B_2 = 1 + |S_{22}|^2 - |S_{11}|^2 - |\Delta|^2$$

$$C_2 = S_{22} - \Delta S_{11}^*$$

$$\Gamma_{in} = \Gamma_S^* = S_{11} + \frac{S_{12}S_{21}\Gamma_L}{1 - S_{22}\Gamma_L}$$

$$\Gamma_{out} = \Gamma_L^* = S_{22} + \frac{S_{12}S_{21}\Gamma_S}{1 - S_{11}\Gamma_S}$$

$$C_L = \frac{(S_{22} - \Delta S_{11}^*)^*}{|S_{22}|^2 - |\Delta|^2}$$

$$R_L = \left| \frac{S_{12}S_{21}}{|S_{22}|^2 - |\Delta|^2} \right|$$

$$C_S = \frac{(S_{11} - \Delta S_{22}^*)^*}{|S_{11}|^2 - |\Delta|^2}$$

$$R_S = \left| \frac{S_{12}S_{21}}{|S_{11}|^2 - |\Delta|^2} \right|$$

$$G_{T \max} = \frac{1}{1 - |\Gamma_S|^2} |S_{21}|^2 \frac{1 - |\Gamma_L|^2}{|1 - S_{22}\Gamma_L|^2}$$

**Microstrip:**

$$Z_o = \frac{377}{\sqrt{\epsilon_r} \left( \frac{w}{h} + 2 \right)}$$

**Trigonometric Function**

$$\sin \alpha \sin \beta = \frac{1}{2} \cos(\alpha - \beta) - \frac{1}{2} \cos(\alpha + \beta)$$

$$\cos \alpha \cos \beta = \frac{1}{2} \cos(\alpha - \beta) + \frac{1}{2} \cos(\alpha + \beta)$$

$$\sin \alpha \cos \beta = \frac{1}{2} \sin(\alpha + \beta) + \frac{1}{2} \sin(\alpha - \beta)$$

$$\cos \alpha \sin \beta = \frac{1}{2} \sin(\alpha + \beta) - \frac{1}{2} \sin(\alpha - \beta)$$

$$\sin 2\alpha = 2 \sin \alpha \cos \alpha = \frac{2 \tan \alpha}{1 + \tan^2 \alpha}$$

$$\cos 2\alpha = \cos^2 \alpha - \sin^2 \alpha = 2 \cos^2 \alpha - 1 = 1 - 2 \sin^2 \alpha$$

$$\sin 3\alpha = 3 \sin \alpha - 4 \sin^3 \alpha$$

$$\cos 3\alpha = 4 \cos^3 \alpha - 3 \cos \alpha$$

$$\sin 4\alpha = 4 \sin \alpha \cos \alpha - 8 \sin^3 \alpha \cos \alpha$$

$$\cos 4\alpha = 8 \cos^4 \alpha - 8 \cos^2 \alpha + 1$$

$$\sin 5\alpha = 5 \sin \alpha - 20 \sin^3 \alpha + 16 \sin^5 \alpha$$

$$\cos 5\alpha = 16 \cos^5 \alpha - 20 \cos^3 \alpha + 5 \cos \alpha$$

Multisection transformer

Binomial matching transformer

$$\Gamma_n = AC_n^N = \frac{Z_{n+1} - Z_n}{Z_{n+1} + Z_n} \cong \frac{1}{2} \ln \frac{Z_{n+1}}{Z_n}$$

$$A = 2^{-N} \frac{Z_L - Z_o}{Z_L + Z_o} \cong 2^{-N} \ln \frac{Z_L}{Z_o}$$

$$C_n^N = \frac{N!}{(N-n)!n!}$$

